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Improving Flower Pollination Algorithm for Solving 0 –1 Knapsack Problem

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Abstract: Binary knapsack problem has received considerable attention in combinational optimization. Various meta-heuristic algorithms are dedicated to solve this problem in the literature. Recently, a binary flower pollination algorithm (BFPA) was proposed, which has been successfully applied to solve 0-1 knapsack problem. In this paper, two new time-varying transfer functions are proposed to improve the exploration and exploitation capability of the BFPA with the best solution and short computing time. Based on small, medium, and high-dimensional scales of the knapsack problem, the computational results reveal that the proposed time-varying transfer functions not only to find the best possible solutions but also to have less computational time. Compared to the standard transfer functions, the efficiency of the proposed time-varying transfer functions is superior, especially in the high-dimensional scales.

1. Introduction

The process of optimization is searching and finding the optimal solution of a given problem [1, 2]. In general, based on the nature of the search space and decision variables, an optimization problem can be divided into three main classes: continuous, discrete and mixed integer optimization problem [3, 4]. The binary optimization problems are a set classes of the discrete optimization problem in which the decision variable is a set of bits.

The knapsack problem is an optimization problem that can be modelled as a discrete binary optimization problem. The knapsack problem has widely studied in many real world applications, such as project selection, cutting stock problems, scheduling problems, resource allocation, and investment decision making [5-7].

There are several methods that have been developed to solve knapsack problem which can be divided into two types: exact methods, such as branch and bound method and dynamic programming. These methods can give the exact solution, but it is effective for small sized problems. The second type includes approximate methods that can give an approximate solution, but at reasonable times compared to exact methods [8-10].

In recent years, several meta-heuristic methods were proposed for tackling 0-1 knapsack problem, such as monarch butterfly optimization (MBO)[11], bat algorithm (BA)[12,13], particle swarm optimization (PSO)[14-16], monkey algorithm (MA)[17], ant colony optimization (ACO)[18], amoeboid organism algorithm (AOA)[19], and harmony search (HS)[20].

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The flower pollination algorithm is a bio-inspired algorithm that mimics the pollination characteristics of flowers in plants. Flower pollination algorithm is first proposed by Yang [21] for solving single objective optimization problems. In (2014) Yang et al. [22] extended flower pollination algorithm for solving multi objective optimization problems. In (2015) Yang [23] proposed a binary flower pollination algorithm to tackle a feature selection problem. Abdel-Basset et al. [9] proposed a binary version of flower pollination algorithm for solving both small and large scale knapsack problem. Compared with some other algorithms, the flower pollination algorithm can perform better in terms of the global convergence and the convergence speed.

In the binary flower pollination algorithm, a transformation function is used to convert the continuous values generated from the algorithm into binary ones, and, therefore it is able to provide a binary flower pollination algorithm a sufficient amount to balance between exploration and exploitation [24].

In this paper, two efficient time-varying transfer functions are proposed to solve the 0-1 knapsack problem. The proposed transfer functions are based on combining the S-shaped and V-shaped transfer functions with time-varying concept.

The remainder of this paper is organized as follows. Section 2 describes the basic 0 - 1 knapsack problem. Section 3 introduces binary flower pollination algorithm. In Section 4, the proposed timevarying transfer functions are presented. Section 5 presents and discusses the experimental results. In section 6, conclusion is drawn.

2. Knapsack problem

Knapsack problem is a NP-hard combinatorial optimization problem and defined as follows [8, 25]:

Given a set of *n* items, each item *i* has a profit c_i and weight w_i . The objective is to select a subset of the items such that the total profit is maximized without exceeding the knapsack's capacity M. Mathematically, the knapsack problem can be formulated as follows:

$$Max f(x) = \sum_{i=1}^{n} c_i x_i$$
(1)

$$\sum_{i=1}^{n} w_i x_i \le M \tag{2}$$

where

$$x_i = \begin{cases} 1 & \text{if item i is selected} \\ 0 & \text{otherwise} \end{cases}$$

To solve knapsack problem, we select a subset of the items of the binary vector x_i such that the optimal solution satisfies the constraint in Eq. (2) and maximizes the objective function in Eq.(1).

In such a constrained optimization problem, the penalty function is used to handle the constrained knapsack problem. As known, the knapsack problem is a maximization problem that can be converted into minimization by multiplying Eq. (1) by -1. As a result, the penalty function can be written as follow: $Min\phi(x) = -f(x) + \lambda Max(0,h)$ (3)

Where $h = \sum_{i=1}^{n} w_i x_i - M$ and λ represents the penalty coefficient. In this paper λ set to 10¹⁰ for

all tests. The penalty function can be described in Figure 1.

s.t.



Figure 1: Penalty function

A Repair operator is treated the infeasible solutions which violates the constraint in Eq. (2) by converting them into feasible solutions and also improve the feasible solutions. The repair operator algorithm can be applied in two stages. The first stage is to convert the infeasible solution into feasible by taking out the items of the lower c_i / w_i ratio so as the constraint in Eq. (2) is not to exceed the knapsack capacity. The second stage is to improve the feasible solution by adding the items of the high c_i / w_i ratio to the knapsack with the keeping of the constraint.

3. Binary flower pollination algorithm(BFPA)

Yang (2012) proposed a new algorithm for global optimization called flower pollination algorithm [21]. It is a meta-heuristic algorithm that mimics nature, inspired of the pollination process in flowers.

Pollination in flowers can be taken two forms: biotic pollination and abiotic pollination. In the first type, the pollen is transferred by pollination like insects and animals. While the second form based on wind and diffusion in the water.

Pollination can be divided into self-pollination and cross-pollination. Self-pollination is transferring the pollens from one flower to the same flower or different flowers in the same plant. Cross-pollination is transferring the pollens from one flower to another flower of a different plant. A flower and its pollen represented a solution to the optimization problem. In the flower pollination algorithm, four basic rules are used[21, 26, 27]:

- 1. The global pollination includes biotic and cross-pollination, the pollinators move in a way that follows a lévy flight distribution.
- 2. The local pollination includes abiotic and self-pollination.
- 3. Flower constancy can be considered as the reproduction probability that is proportional to the similarity of two flowers involved.
- 4. We use a switch probability $p \in [0,1]$ to switch between global pollination and local pollination.

Rules 1 and 3 can be expressed mathematically as:

$$x_i^{t+1} = x_i^t + \gamma L\left(\lambda\right) \left(x_i^t - g^*\right) \tag{4}$$

where x_i^t is the solution vector or the pollen *i* at iteration *t*, g^* is the current best solution that is found at the current iteration, γ is a scaling factor to control the step size, $L(\lambda)$ is the step size in the lévy flights which is representing the strength of the pollination. Since pollinators move over a long distance with various distance steps, a lévy flight can be used to mimic this behaviour. That is, L > 0 from a lévy distribution as

$$L \sim \frac{\lambda \Gamma(\lambda) \sin\left(\frac{\pi \lambda}{2}\right)}{\pi} \left(\frac{1}{S^{1+\lambda}}\right) (S \gg S_0 > 0)$$
(5)

Yang (2012) proposed $\Gamma(\lambda)$, the standard gamma function, and $\lambda = 1.5$. This distribution is valid for large steps S > 0. In (1994), Mantegna used the Gaussian distribution for generating the step size S by generating two random numbers U and V as follows [26]:

$$S = \frac{U}{|V|^{1/\lambda}} \quad U \sim N(0, \sigma^2), \quad V \sim N(0, 1)(6)$$
$$\sigma^2 = \left(\frac{\Gamma(1+\lambda)}{\lambda \Gamma[(1+\lambda)/2]} * \frac{\sin(\pi\lambda/2)}{2^{\frac{\lambda-1}{2}}}\right)^{1/\lambda} \tag{7}$$

For local pollination, rules 2 and 3 can be expressed as:

$$x_{i}^{t+1} = x_{i}^{t} + k \left(x_{j}^{t} - x_{k}^{t} \right)$$
(8)

where x_j and x_k are the pollens (solution vectors) from different flowers of the same plant. k is the parameter draws from a uniform distribution in [0,1]. To switch between common global pollination to intensive local pollination, we used rule 4. In 2012, Yang suggested that switch probability or proximity probability p = 0.8 for most applications. The flower pollination algorithm can be presented in Figure 2.

Flower	Pollination Algorithm
Begin	
-	Define the objective function max or min $f(x)$, and switch probability $p \in [0,1]$
-	Initialize the population of n random flowers
-	Evaluate each flowers in the population
-	Find the best solution
-	while (stopping criterion)
-	for i=1:n
-	if (r≤p)
-	New solution $=$ global pollination Eq. (4)
-	else
-	New solution = local pollination Eq. (8)
-	end if
-	Evaluate new solution
-	If new solution is better, update the population
-	end for
-	Find current best solution
-	end while

Figure 2: Flower pollination algorithm

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4. The proposed time-varying transfer functions

The knapsack problem can be modeled as a discrete problem in which the solution vector is binary, where 1 corresponds to that an item will be selected in the knapsack and 0 otherwise. In any binary algorithm, where one uses the step vector to calculate the probability of changing positions, the transfer functions significantly impact the balance between exploration and exploitation[24, 28].

In BFPA, the transfer function is used to map a continuous search space to a binary one, and the updating process is designed to switch positions of pollens between 0 and 1 in binary search spaces. In order to build this binary vector, a transfer function in Eq. (9) can be used after Eq. (8), in which the new solution is constrained to only binary values:

$$x_{i}^{t} = \begin{cases} 1 & if \quad T(x) > r \\ 0 & ow \end{cases}$$

$$\tag{9}$$

where $r \in [0,1]$ is a random number, T(x) is the transfer function.

Mirjalili and Lewis [29] introduced eight transfer functions and divided them into two families: S-Shaped transfer functions and V-Shaped transfer functions. These transfer functions are listed in Table 1. The transfer function was tested by Mirjalili and Lewis on 25 benchmark functions. The results show that V-shaped transfer functions are useful for the binary particle swarm optimization, especially V_4 function has merit for solving these functions. Teng et al.[30] has demonstrated the effect of V-shaped transfer function using binary particle swarm optimization on the feature selection problem. The experimental tests reveal that the efficiency of the proposed method.

In optimization algorithm, it is expected that the focus of the early stages of the implementation the algorithm will be on exploration to avoid falling into the local point, but in later stages of implementing the algorithm focuses more on exploitation to improve the quality of the solution[24, 28].

In this paper, two dynamic transfer functions are adapted form Mafarja, Aljarah [28] and Islam, Li [24], and proposed to improve the BFPA with the following considerations [24]:

- 1. In the early stages of the implementation, the transfer function should provide a high probability of flipping all the bits of x_i so that the BFPA can provide a stronger exploration.
- 2. In the intermediate stages of the implementation, the BFPA should start shifting from exploration to exploitation. This can achieved by using a transfer function that can reduce the probability of flipping all the bits of x_i .
- 3. In the final stages of the implementation, the transfer function should provide a low probability of flipping all the bits of x_i , so that the BFPA can provide a stronger exploitation capability.

In our proposed time-varying transfer function (TV), a new control parameter τ is added in the original transfer function. This τ is a time varying variable which starts with large value and gradually decreases over time. Two types of τ are proposed as follow:

$$\tau_1 = \left(1 - \frac{t}{T}\right) \tau_{1,\max} + \frac{t}{T} \tau_{1,\min}$$
(10)

and

$$\tau_2 = \tau_{2,\max} - t \left(\frac{\tau_{2,\max} - \tau_{2,\min}}{T} \right) \tag{11}$$

where τ_{max} and τ_{min} are the minimum and maximum values of the control parameter τ , and T is the maximum iteration of the BFPA. Table 2 lists the two proposed time-varying transfer functions.

	S-Shaped family		V-Shaped family
S1	$T\left(x\right) = \frac{1}{1 + e^{-2x}}$	V1	$T(x) = \left erf\left(\frac{\sqrt{\pi}}{2}x\right) \right $
S2	$T(x) = \frac{1}{1 + e^{-x}}$	V2	$T(x) = \tanh(x) $
S 3	$T\left(x\right) = \frac{1}{1 + e^{-\frac{x}{2}}}$	V 3	$T(x) = \left \frac{x}{\sqrt{1 + x^2}} \right $
S 4	$T\left(x\right) = \frac{1}{1 + e^{-\frac{x}{3}}}$	V4	$T(x) = \left \frac{2}{\pi}\arctan\left(\frac{\pi}{2}x\right)\right $

 Table 1: Families of transfer functions

Table 2: The two proposed time-varying transfer functions.

	Time-varying 1		Time-varying 2
T1S1	$TVS(x) = \frac{1}{1 + e^{\frac{-2x}{\tau_1}}}$	T2S1	$TVS(x) = \frac{1}{1 + e^{\frac{-2x}{\tau_2}}}$
T1S2	$TVS(x) = \frac{1}{1 + e^{\frac{-x}{\tau_1}}}$	T2S2	$TVS\left(x\right) = \frac{1}{1 + e^{\frac{-x}{\tau_2}}}$
T1S3	$TVS(x) = \frac{1}{1 + e^{-\frac{x}{2\tau_1}}}$	T2S3	$TVS(x) = \frac{1}{1 + e^{-\frac{x}{2\tau_2}}}$
T1S4	$TVS(x) = \frac{1}{1 + e^{-\frac{x}{3\tau_1}}}$	T2S4	$TVS(x) = \frac{1}{1 + e^{-\frac{x}{3\tau_2}}}$

Table 3: The two proposed time-varying transfer functions.

T1V1	$TVV(x) = \left erf\left(\frac{\sqrt{\pi}x}{2\tau_1}\right) \right $	T2V1	$TVV(x) = \left erf\left(\frac{\sqrt{\pi}x}{2\tau_2}\right) \right $
T1V2	$TVV(x) = \left \tanh\left(\frac{x}{\tau_1}\right) \right $	T2V2	$TVV(x) = \left \tanh\left(\frac{x}{\tau_2}\right) \right $
Г1V3	$TVV(x) = \left \frac{x / \tau_1}{\sqrt{1 + x^2 / \tau_1}} \right $	[2V3	$TVV(x) = \left \frac{x / \tau_2}{\sqrt{1 + x^2 / \tau_2}} \right $
Г1V4	$TVV(x) = \left \frac{2}{\pi}\arctan\left(\frac{\pi x}{2\tau_1}\right)\right $	Γ 2 V4	$TVV(x) = \left \frac{2}{\pi}\arctan\left(\frac{\pi x}{2\tau_2}\right)\right $

5. Computational results

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5.1. Parameter setting

For the binary flower pollination algorithm, the parameters were setting as follows: the population size =50, $\lambda = 1.5$, p = 0.8. In this paper, we use linear decreasing time varying where $\tau_{\text{max}} = 4$, $\tau_{\text{min}} = 0.1$, and T represents the maximum number of iterations.

5.2 Comparison results

To verify the feasibility and effectiveness of the proposed time-varying transfer functions method for solving 0–1 Knapsack problem, three scales of the knapsack problem are considered: low, medium, and high-dimensional scales. In this paper, all the results are obtained from 50 independent trials. The best solution, the worst solution, the mean and the standard deviation (SD) values, Mean iterations are reported as evaluation criteria. All of the computational experiments were conducted in Matlab 13a on a PC with an Intel Pentium Core i7-7500 processor (2.9 GHz) with 16GB of RAM in the Windows 10 OS.

5.2.1 Low scale 0-1 KP

The performance of the improved algorithm is investigated to solve ten low scale 0-1 KP instances (kp-1 to kp-10), which are taken from [9, 13]. The dimensions in this case are ranging from 4 to 23. The information dimension, capacity, weights and profits for these ten instances are described in Table S1 (Appendix). Table 4 shows the comparison results for all the used different transfer functions for the kp1 and kp10. The rest instances are listed in Table S2 (Appendix).

As observed from the results in Table 4 and Table S2, for the low scale knapsack problems, there is no difference among the results of using the proposed time-varying transfer functions and the standard transfer functions in terms of the best, worse, mean, and SD values. The major difference among the performance of the proposed time-varying transfer functions and the standard transfer functions in not expected because of relatively small numbered items. Contrary, the proposed time-varying transfer functions give optimal results with less number of iterations. The mean iterations of the proposed timevarying transfer functions are obviously better than the standard transfer functions for kp8, kp9, and kp10 where the number of items is higher than the others. Moreover, comparing between the two proposed transfer function, the required iterations to get the optimal solution using Eq. (11) is less than of Eq. (10) for kp8, kp9, and kp10.

Instance	Transfer	Rost	Moon	Worst	SD	Mean
Instance	Tunction	Dest	Wieall	worst	3D	nerations
kp-1	S 1	35	35	35	0	1
	S2	35	35	35	0	1
	S 3	35	35	35	0	1
	S 4	35	35	35	0	1
	V1	35	35	35	0	1
	V2	35	35	35	0	1
	V3	35	35	35	0	1
	V4	35	35	35	0	1
	T1S1	35	35	35	0	1
	T1S2	35	35	35	0	1
	T1S3	35	35	35	0	1
	T1S4	35	35	35	0	1

Table 4. Results obtained by the transfer functions for the low scale $0-1$ R	Table 4: Results	obtained by th	e transfer	functions for	the low	scale 0–1 KP
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Journal of Physics: Conference Series		es	1879 (202	21) 022097	doi:10.1088	/1742-6596/1879/2/022097
	771171	25	25	25	0	
		35	35	35	0	1
	T1V2	35	35	35	0	1
	11V3	35	35	35	0	1
		35	35	35	0	1
	1281	35	35	35	0	1
	T2S2	35	35	35	0	1
	T2S3	35	35	35	0	1
	1284	35	35	35	0	1
	12V1	35	35	35	0	1
	T2V2	35	35	35	0	1
	12V3	35	35	35	0	1
1 10	T2V4	35	35	35	0	
kp-10	SI	9767	9767	9767	0	2.28
	S2	9767	9767	9767	0	4.44
	S3	9767	9767	9/6/	0	9.8
	S 4	9767	9767	9767	0	15.64
	V1	9767	9767	9767	0	1.2
	V2	9767	9767	9767	0	1.2
	V3	9767	9767	9767	0	1.24
	V4	9767	9767	9767	0	1.12
	T1S1	9767	9767	9767	0	4.39
	T1S2	9767	9767	9767	0	1.95
	T1S3	9767	9767	9767	0	7.19
	T1S4	9767	9767	9767	0	15.19
	T1V1	9767	9767	9767	0	1.12
	T1V2	9767	9767	9767	0	1.08
	T1V3	9767	9767	9767	0	1.15
	T1V4	9767	9767	9767	0	1
	T2S1	9767	9767	9767	0	2.95
	T2S2	9767	9767	9767	0	2.17
	T2S3	9767	9767	9767	0	8.42
	T2S4	9767	9767	9767	0	12.76
	T2V1	9767	9767	9767	0	1.15
	T2V2	9767	9767	9767	0	1
	T2V3	9767	9767	9767	0	1.04
	T2V4	9767	9767	9767	0	1

5.2.2 Medium scale 0-1 KP

To further evaluate the performance of proposed time-varying transfer functions in medium scale 0-1 Knapsack problem, ten medium size 0-1 KP instances (kp-11 to kp-20) are taken from [9, 13] in which the items are between 30 and 75. The description of these ten instances is described in Table S3 (Appendix). Table 5 summarizes the comparison results for all the used different transfer functions for the kp15 and kp20. The rest instances results are reported in Table S4 (Appendix).

Obviously, it is evident from Table 5 and Table S4 that the proposed time-varying transfer functions obtained the same best, worse, mean, and SD values as the standard transfer functions. From Tables 5 and S4, for the mean iterations, the proposed time-varying transfer functions are superior to the other eight standard transfer functions on kp11 to kp20. This indicates that the proposed time-varying transfer functions is comparatively fast. For example, in kp20, the reduction in mean iteration of T1S2 and T2S2

Ibn Al-Haitham International Conference for Pur	e and Applied Sciences	(IHICPS)	IOP Publishing
Journal of Physics: Conference Series	1879 (2021) 022097	doi:10.1088/1742	-6596/1879/2/022097

functions was 37.61% and 49.81% lower than that of S2, respectively. On the other hand, the reduction in mean iteration of T1V4 and T2V4 functions was 40.08% and 60.32% lower than that of V4, respectively.

Further, it was noted that the v-shaped transfer functions are usually yielded the least iterations compared to S-shaped transfer functions. On the other hand, comparing between the two proposed transfer functions, the required iterations to get an optimal solution using Eq. (11) is less than of Eq. (10) for all the 0-1 Knapsack problems. Additionally, the number of iterations of T2V1, T2V2, T2V3, and T2V4 are obviously small than T1V1, T1V2, T1V3, and T1V4.

	Transfer					Mean
Instance	function	Best	Mean	Worst	SD	iterations
kp-15	S 1	2440	2440	2440	0	9.72
-	S2	2440	2440	2440	0	29.4
	S 3	2440	2440	2440	0	21.64
	S 4	2440	2440	2440	0	15.6
	V1	2440	2440	2440	0	5.56
	V2	2440	2440	2440	0	3.4
	V3	2440	2440	2440	0	2.44
	V4	2440	2440	2440	0	1.8
	T1S1	2440	2440	2440	0	19.84
	T1S2	2440	2440	2440	0	17.04
	T1S3	2440	2440	2440	0	12.12
	T1S4	2440	2440	2440	0	8.48
	T1V1	2440	2440	2440	0	1.08
	T1V2	2440	2440	2440	0	1.16
	T1V3	2440	2440	2440	0	1.16
	T1V4	2440	2440	2440	0	1.12
	T2S1	2440	2440	2440	0	25.16
	T2S2	2440	2440	2440	0	16.8
	T2S3	2440	2440	2440	0	15.56
	T2S4	2440	2440	2440	0	9.92
	T2V1	2440	2440	2440	0	1.04
	T2V2	2440	2440	2440	0	1.04
	T2V3	2440	2440	2440	0	1.04
	T2V4	2440	2440	2440	0	1
kp-20	S 1	3614	3614	3614	0	48.53
-	S 2	3614	3614	3614	0	125.41
	S 3	3614	3614	3614	0	115.36
	S 4	3614	3614	3614	0	137.4
	V1	3614	3614	3614	0	18.54
	V2	3614	3614	3614	0	8.46
	V3	3614	3614	3614	0	6.82
	V4	3614	3614	3614	0	4.89
	T1S1	3614	3614	3614	0	50.18
	T1S2	3614	3614	3614	0	78.24
	T1S3	3614	3614	3614	0	82.13
	T1S4	3614	3614	3614	0	92.74
	T1V1	3614	3614	3614	0	10.21

Table 5: Results obtained by the transfer functions for the medium scale 0-1 KP

Ibn Al-Haitham International Conference for Pure and Applied Sciences (IHICPS)							
Journal of Physics: Conference Series	1	879 (2021)	022097	doi:10.1	088/1742-65	96/1879/2/022097	
T1V2	3614	3614	3614	0	4.18		
T1V3	3614	3614	3614	0	4.53		
T1V4	3614	3614	3614	0	2.93		
T2S1	3614	3614	3614	0	46.65		
T2S2	3614	3614	3614	0	62.94		
T2S3	3614	3614	3614	0	91.6		
T2S4	3614	3614	3614	0	69.34		
T2V1	3614	3614	3614	0	7.26		
T2V2	3614	3614	3614	0	3.62		
T2V3	3614	3614	3614	0	3.98		
T2V4	3614	3614	3614	0	1.94		

5.2.3 High-dimensional scale 0-1 KP

concluded.

To further highlight the benefits of our proposed time-varying transfer functions, three cases have been investigated. The first case handles the uncorrelated problem (kp21 – kp25) where the weights w_i are uncorrelated with the profits c_i . Each w_i and c_i is randomly chosen from 5 to 20 and from 5 to 40, respectively. The second case handles the weakly correlated problem (kp26 – kp30). In this case, the weights w_i and the profits c_i can be expressed as follows: $w_i \in [5, 20]$ and $c_i \in [w_i - 5, w_i + 5]$. The third case handles the strongly correlated problem (kp31 – kp35). In this case, w_i and c_i can be calculated as: $w_i \in [5, 20]$ and $c_i \in [w_i + 5]$. The knapsack capacity for the kp-21-kp35 can be calculated as $M = 0.75 \times \sum_{i=1}^{n} w_i$. The dimension sizes varying from 100 to 2000 items. For all used transfer functions, the maximum iteration is set to 10000. Tables 6 – 8 reports the comparison results for all the used different transfer functions for the kp22, kp25, kp27, kp30, kp32, and kp35. The rest problems are listed in Tables S5 – S7 (Appendix). Based on the obtained results, several points are

- (1) It can be seen that the proposed time-varying transfer functions significantly outperform the standard transfer functions on all evaluation measures including the best, mean, worst, and standard deviations.
- (2) As observed from the results, the proposed time-varying V-shaped transfer functions, T1V1 T2V4, can easily find the optimal values with small SD in all uncorrelated, weakly correlated, and strongly correlated problems.
- (3) It is obvious that there is an improvement for searching the global optimal solution when using T2V1, T2V2, T2V3, and T2V4 compared to T1V1, T1V2, T1V3, and T1V4. This leads to the performance dominance of T2V1, T2V2, T2V3, and T2V4 against those performed on the T1V1, T1V2, T1V3, and T1V4.
- (4) The mean iteration values of time-varying V-shaped transfer functions, T1V1 T2V4, are obviously superior to S1, S2, S3, S4, V1, V2, V3, and V4 for all high-dimensional scale problems. The performance of T2V1, T2V2, T2V3, and T2V4 is better than that of T1V1, T1V2, T1V3, and T1V4.
- (5) Compared to the proposed time-varying V-shaped transfer functions, T2V4 is significantly improving the performance metrics with lower SD and mean iterations.

Table 6: Comparison results of uncorrelated high-dimensional scale 0–1 KP

Instance	Dimension	Transfer function	Best	Mean	Worst	SD	Mean iterations
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Ibn Al-Haitham International Conference for I			Pure and Ap	plied Sciences	(IHICPS) IOP Publishing			
Journal of Physics	Journal of Physics: Conference Series		1879 (2	1879 (2021) 022097		doi:10.1088/1742-6596/1879/2/0		
kp-22	500	S 1	10340	10338	10335	2.739	1038	
-		S2	10338	10302.2	10225	25.46	2394	
		S 3	10338	10306.6	10225	26.923	2187	
		S 4	10338	10311	10225	20.01	2541	
		V1	10345	10345	10345	0	185	
		V2	10345	10345	10345	0	103	
		V3	10345	10345	10345	0	161	
		V4	10345	10345	10345	0	94	
		T1S1	10345	10345	10345	0	1074	
		T1S2	10343	10333.4	10319	13.145	1851	
		T1S3	10343	10328.6	10319	13.145	2018	
		T1S4	10343	10323.8	10319	10.733	1932	
		T1V1	10345	10345	10345	0	110	
		T1V2	10345	10345	10345	0	95	
		T1V3	10345	10345	10345	0	104	
		T1V4	10345	10345	10345	0	73	
		T2S1	10345	10345	10345	0	1022	
		T2S2	10343	10325	10319	10.392	1915	
		T2S3	10343	10327.2	10319	9.96	1893	
		T2S4	10343	10328.4	10319	9.044	1801	
		T2V1	10345	10345	10345	0	100	
		T2V2	10345	10345	10345	0	94	
		T2V3	10345	10345	10345	0	99	
		T2V4	10345	10345	10345	0	69	
kp-25	2000	S 1	40612	40598.2	40589	12.674	6285	
		S 2	40610	40554.8	40525	33.945	8136	
		S 3	40610	40549	40525	37.259	7985	
		S 4	40610	40544.9	40525	38.157	7612	
		V1	40615	40611.8	40610	15.375	3485	
		V2	40615	40612.4	40610	14.281	2952	
		V3	40615	40611.2	40610	16.158	3624	
		V4	40615	40612.8	40610	14.825	2531	
		T1S1	40616	40610.6	40595	9.521	4258	
		T1S2	40614	40599.5	40590	20.98	6395	
		T1S3	40614	40611.8	40590	19.353	5927	
		T1S4	40614	40610.2	40590	21.97	6042	
		T1V1	40616	40614.6	40611	8.34	2493	
		T1V2	40616	40615	40611	7.921	2051	
		T1V3	40616	40614.2	40611	8.95	2964	
		T1V4	40616	40615.2	40611	6.56	1950	
		T2S1	40616	40611.2	40595	8.536	4381	
		T2S2	40614	40610.6	40590	19.561	6134	
		T2S3	40614	40611.4	40590	17.562	5630	
		T2S4	40614	40610.8	40590	20.315	6729	
		T2V1	40616	40614	40611	7.65	2654	
		T2V2	40616	40614.8	40611	6.98	1983	
		T2V3	40616	40614.6	40611	6.551	2452	
		T2V4	40616	40615.4	40611	5.439	1875	

 Table 7: Comparison results of weakly correlated high-dimensional scale 0–1 KP

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Journal	of Physics:	Conference	Series
Journar	01 1 11 9 51 6 5.	Conterence	Derres

1879 (2021) 022097 doi:10.1088/1742-6596/1879/2/022097

Instance	Dimension	Transfer Be	Best	t Mean	Worst	SD	Mean
mstunee	Dimension	function	function Dest		worst	50	iterations
kp-27	500	S 1	5197	5185.2	5175	8.624	1002
		S2	5190	5186.2	5184	9.943	1980
		S 3	5190	5185.4	5184	8.67	1542
		S 4	5190	5185.6	5184	8.24	1834
		V1	5197	5193.4	5190	4.96	162
		V2	5197	5193	5190	5.63	90
		V3	5197	5194.2	5190	5.176	166
		V4	5197	5194.6	5190	4.641	75
		T1S1	5197	5197	5197	0	995
		T1S2	5197	5194.8	5194	2.67	1091
		T1S3	5197	5195.4	5194	1.954	1124
		T1S4	5197	5194.2	5194	1.37	1387
		T1V1	5197	5197	5197	0	123
		T1V2	5197	5197	5197	0	84
		T1V3	5197	5197	5197	0	98
		T1V4	5197	5197	5197	0	61
		T2S1	5197	5197	5197	0	981
		T2S2	5197	5195	5194	1.095	1192
		T2S3	5197	5194.8	5194	2.04	1184
		T2S4	5197	5194.4	5194	1.93	1207
		T2V1	5197	5197	5197	0	111
		T2V2	5197	5197	5197	Ő	88
		T2V3	5197	5197	5197	Ő	93
		T2V4	5197	5197	5197	Õ	56
kp-30	2000	S1	21044	21036.5	21018	20.652	6018
		S2	21025	21005.2	20890	44.67	9820
		<u>S</u> 3	21025	21004.8	20890	46.391	9453
		S 4	21025	21005.1	20890	45.752	9572
		V1	21068	21057	21033	17.297	3091
		V2	21068	21057.4	21033	18.632	2735
		V3	21068	21056.8	21033	15.348	3120
		V4	21068	21057.8	21033	14.982	2493
		T1S1	21081	21079.2	21070	12.358	5304
		T1S2	21078	21074	21062	27.291	7659
		T1S3	21078	21073	21062	28.9	7362
		T1S4	21078	21074.6	21062	25.367	7710
		T1V1	21081	21079	21075	9.452	2514
		T1V2	21081	21079.2	21075	8.651	2183
		T1V3	21081	21078	21075	10.12	2907
		T1V4	21081	21079.2	21075	8.654	2061
		T2S1	21081	21079	21070	11.92	5297
		T2S2	21078	21074.8	21062	29.381	7640
		T2S3	21078	21075	21062	25.648	7193
		T2S4	21078	21074	21062	28.31	7684
		T2V1	21081	21078	21075	11.51	2761
		T2V2	21081	21079	21075	8.372	2031
		T2V3	21081	21078.6	21075	9.62	2897
		T2V4	21081	21079.4	21075	8.05	2005

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Journal of Physics: Conference Series	1879 (2021) 022097	doi:10.1088/1742	-6596/1879/2/022097

Instance I	Dimension	Transfer	Doct	Moon	Worst	SD	Mean
Instance	Dimension	function	Dest	Mean Wors		20	iterations
kp-32	500	S 1	6783	6783	6783	0	978
•		S 2	6779	6775.6	6768	5.681	1862
		S 3	6779	6776	6768	6.16	1734
		S 4	6779	6775	6768	5.935	1815
		V1	6783	6781.5	6779	3.94	138
		V2	6783	6782	6779	4.67	105
		V3	6783	6781.9	6779	4.914	133
		V4	6783	6782.4	6779	3.952	100
		T1S1	6783	6783	6783	0	1086
		T1S2	6783	6780	6776	3.68	1273
		T1S3	6783	6780.2	6776	2.942	1360
		T1S4	6783	6780.9	6776	4.37	1109
		T1V1	6783	6783	6783	0	97
		T1V2	6783	6783	6783	0	57
		T1V3	6783	6783	6783	0	96
		T1V4	6783	6783	6783	0	50
		T2S1	6783	6783	6783	0	1050
		T2S2	6783	6781.2	6776	4.518	1241
		T2S3	6783	6780.8	6776	5.63	1293
		T2S4	6783	6782	6776	4.09	1113
		T2V1	6783	6783	6783	0	101
		T2V2	6783	6783	6783	0	55
		T2V3	6783	6783	6783	0	90
		T2V4	6783	6783	6783	0	51
kp-35	2000	S 1	27285	27279.6	27246	15.162	5506
		S 2	27292	27276	27230	30.37	6931
		S 3	27292	27277.2	27230	35.61	6654
		S 4	27292	27276.1	27230	29.49	6837
		V1	27356	27349	27344	10.34	2741
		V2	27356	27350	27344	12.57	2652
		V3	27356	27349.8	27344	11.31	2903
		V4	27356	27351	27344	11.94	2511
		T1S1	27362	27359	27350	9.58	6347
		T1S2	27362	27358	27349	16.54	5028
		T1S3	27362	27357	27349	18.36	5391
		T1S4	27362	27357.6	27349	15.29	5727
		T1V1	27362	27360	27358	3.67	1890
		T1V2	27362	27361	27358	2.94	1682
		T1V3	27362	27360.2	27358	3.05	1954
		T1V4	27362	27361.6	27358	3.58	1509
		T2S1	27362	27358.2	27350	10.17	3583
		T2S2	27362	27357.6	27349	14.89	5126
		T2S3	27362	27358	27349	16.52	6084
		T2S4	27362	27357	27349	17.13	5737
		T2V1	27362	27361	27358	2.34	1903
		T2V2	27362	27360.9	27358	3.61	1530
		T2V3	27362	27361.4	27358	2.57	1827

Table 8: Comparison results of strongly correlated high-dimensional scale 0–1 KP

Ibn Al-Haitham International Conference for Pure	and Applied Sciences	(IHICPS)	IOP Publishing
Journal of Physics: Conference Series	1879 (2021) 022097	doi:10.1088/1742-6	596/1879/2/022097

T2V4 27362 27361.8 27358 2.09 1493

6. Conclusion

In this paper, two time-varying transfer functions are proposed to improve the exploration and exploitation capability of the binary flower pollination algorithm in solving the 0-1 KP problem efficiently. The experimental results show that the introduction of time-varying parameter in the transfer function can improve the performance of BFPA in solving small, medium, and high-dimensional scales 0-1 KP problems. Additionally, the experimental results show that proposed time-varying V-shaped transfer functions outperform the other S-shaped transfer functions in terms of the best, worse, mean, SD values, and the mean iterations.

Appendix

Instance	dimension	capacity M	weights W	profits C
kp-1	4	20	w=[6597]	c=[9 11 13 15]
kp-2	4	11	w=[2 4 6 7]	$c = [6 \ 10 \ 12 \ 13]$
kp-3	5	80	w=[15 20 17 8 31]	c=[33 24 36 37 12]
kp-4	7	50	w=[31 10 20 19 4 3 6]	c=[70 20 39 37 7 5 10]
1-m <i>5</i>	10	260	w=[95 4 60 32 23 72 80 62 65	c=[55 10 47 5 4 50 8 61 85
кр-5	10	209	46]	87]
kp-6	10	60	w=[30 25 20 18 17 11 5 2 1 1]	c=[20 18 17 15 15 10 5 3 1 1]
_			w=[56.358531 80.874050	c=[0.125126 19.330424
			47.987304 89.596240	58.500931 35.029145
		275	74.660482 85.894345	82.284005 17.410810
Irm 7	15		51.353496 1.498459	71.050142 30.399487
кр-7	15	5/5	36.445204 16.589862	9.140294 14.731285
			44.569231 0.466933	98.852504 11.908322
			37.788018 57.118442	0.891140 53.166295
			60.716575]	60.176397]
			w=[84 83 43 4 44 6 82 92 25 83	c=[91 72 90 46 55 8 35 75 61
kp-8	20	879	56 18 58 14 48 70 96 32 68	15 77 40 63 75 29 75 17
_			92]	78 40 44]
			w=[92 4 43 83 84 68 92 82 6 44	· [44 46 00 72 01 40 75 25 9
kp-9	20	878	32 18 56 83 25 96 70 48 14	$C = [44 \ 46 \ 90 \ 72 \ 91 \ 40 \ 75 \ 55 \ 8 \ 54 \ 78 \ 40 \ 77 \ 15 \ (1 \ 17 \ 75)$
			58]	54 /8 40 // 15 61 1/ /5]
			w=[983 982 981 980 979 978	c=[981 980 979 978 977 976
	22	10000	488 976 972 486 486 972	487 974 970 485 485 970
kp-10	23	10000	972 485 485 969 966 483	970 484 484 976 974 482
-			964 963 961 958 959]	962 961 959 958 857]

Table S1: The description of the low scale 0-1 KP instances

	Transfer					Mean
Instance	function	Best	Mean	Worst	SD	iterations
	S 1	23	23	23	0	1
	S2	23	23	23	0	1
less Q	S 3	23	23	23	0	1
кр-2	S4	23	23	23	0	1
	V1	23	23	23	0	1
	V2	23	23	23	0	1

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Journal of Physics:	Journal of Physics: Conference Series		1879 (2021) 022097	doi:10.1	5/1879/2/022097	
	V3	23	23	23	0	1
	V4	23	23	23	0	1
	T1S1	23	23	23	0	1
	T1S2	23	23	23	0	1
	T1S3	23	23	23	0	1
	T1S4	23	23	23	0	1
	T1V1	23	23	23	0	1
	T1V2	23	23	23	0	1
	T1V3	23	23	23	0	1
	T1V4	23	23	23	0	1
	T2S1	23	23	23	0	1
	T2S2	23	23	23	0	1
	T2S3	23	23	23	0	1
	T2S4	23	23	23	0	1
	T2V1	23	23	23	0	1
	T2V2	23	23	23	0	1
	T2V3	23	23	23	0	1
	T2V4	23	23	23	Ő	1
	S1	130	130	130	0	1
	S1 S2	130	130	130	Ő	1
	S2 S3	130	130	130	0	1
	53 54	130	130	130	0	1
	V1	130	130	130	0	1
	V1 V2	130	130	130	0	1
	V2 V3	130	130	130	0	1
	V J V A	130	130	130	0	1
	V4 T1S1	130	130	130	0	1
	T151 T152	120	130	120	0	1
	T152	120	130	120	0	1
	1155 T184	120	130	130	0	1
kp-3	1154 T1V1	120	130	130	0	1
-		130	130	130	0	1
	11V2	130	130	130	0	1
	11V3	130	130	130	0	1
		130	130	130	0	1
	1281	130	130	130	0	1
	1282	130	130	130	0	l
	T2S3	130	130	130	0	l
	1284	130	130	130	0	l
	T2V1	130	130	130	0	1
	T2V2	130	130	130	0	1
	T2V3	130	130	130	0	1
	T2V4	130	130	130	0	1
	S 1	107	107	107	0	1
	S2	107	107	107	0	1.08
	S 3	107	107	107	0	1.04
kn-4	S4	107	107	107	0	1.04
vЪ_д	V1	107	107	107	0	1
	V2	107	107	107	0	1
	V3	107	107	107	0	1
	V4	107	107	107	0	1

Ibn Al-Haitham International Conference for Pure and Applied Sciences (IHICPS) IOP						
Journal of Physics: Conference Series			1879 (2021) 022097	doi:10.1088/1742-6596/1879/2/022		
-						
	T1S1	107	107	107	0	1
	T1S2	107	107	107	0	1
	T1S2	107	107	107	0	1
	T1S4	107	107	107	Ő	1
	TIV1	107	107	107	Ő	1
	T1V2	107	107	107	0	1
	T1V3	107	107	107	0	1
	T1V4	107	107	107	Ő	1
	T2S1	107	107	107	0	1
	T2S2	107	107	107	Ő	1
	T2S3	107	107	107	Ő	1
	T2S4	107	107	107	Ő	1
	T2V1	107	107	107	0	1
	T2V2	107	107	107	0 0	1
	T2V3	107	107	107	0	1
	T2V4	107	107	107	Ő	1
	S1	295	295	295	0	1.12
	S2	295	295	295	0	1.92
	S3	295	295	295	0 0	1.32
	S4	295	295	295	0	1.16
	V1	295	295	295	0 0	1.16
	V2	295	295	295	0	1.04
	V3	295	295	295	0 0	1.04
	V4	295	295	295	0	1.04
	T1S1	295	295	295	0 0	1
	T1S2	295	295	295	0	1
	T1S3	295	295	295	0 0	1
	T1S4	295	295	295	0	1
kp-5	T1V1	295	295	295	0	1
	T1V2	295	295	295	0	1
	T1V3	295	295	295	0	1
	T1V4	295	295	295	0	1
	T2S1	295	295	295	0	1
	T2S2	295	295	295	0	1
	T2S3	295	295	295	0	1
	T2S4	295	295	295	0	1
	T2V1	295	295	295	0	1
	T2V2	295	295	295	0	1
	T2V3	295	295	295	0	1
	T2V4	295	295	295	0	1
	S 1	52	52	52	0	1
	S2	52	52	52	0	1
	S 3	52	52	52	0	1
	S 4	52	52	52	0	1
1 6	V1	52	52	52	0	1
кр-б	V2	52	52	52	0	1
	V3	52	52	52	0	1
	V4	52	52	52	0	1
	T1S1	52	52	52	0	1
	T1S2	52	52	52	0	1

Ibn Al-Haitham Inte	ernational Conferer	ice for Pure	e and Applied Science	s (IHICPS)		IOP Publishing
Journal of Physics:	Conference Series		1879 (2021) 022097	doi:10.1	088/1742-659	6/1879/2/022097
	T1S3	52	52	52	0	1
	T1S4	52	52	52	0	1
	T1V1	52	52	52	0	1
	T1V2	52	52	52	0	1
	T1V3	52	52	52	0	1
	T1V4	52	52	52	0	1
	T2S1	52	52	52	0	1
	T2S2	52	52	52	0	1
	T2S3	52	52	52	0	1
	T2S4	52	52	52	0	1
	T2V1	52	52	52	Ō	1
	T2V2	52	52	52	Ő	1
	T2V3	52	52	52	Ő	1
	T2V4	52	52 52	52 52	Ő	1
	S1	481.07	481.069	481.07	0 0	1
	\$2 51	481.07	481.069	481.07	0	1
	S2 S3	481.07	481.069	401.07	0	1
	55 \$4	481.07	481.002	481.07	0	1
	54 V1	401.07	481.009	401.07	0	1
	V1 V2	401.07	481.009	401.07	0	1
	V2 V2	401.07	481.009	401.07	0	1
	V S V A	401.07	481.009	401.07	0	1
	V4 T1C1	481.07	481.009	481.07	0	1
	1151 T152	481.07	481.009	481.07	0	1
	1152 T152	481.07	481.069	481.07	0	1
	T153	481.07	481.069	481.07	0	1
kp-7	1184	481.07	481.069	481.07	0	1
1	TIVI	481.07	481.069	481.07	0	1
	T1V2	481.07	481.069	481.07	0	1
	TIV3	481.07	481.069	481.07	0	1
	TIV4	481.07	481.069	481.07	0	1
	T2S1	481.07	481.069	481.07	0	1
	T2S2	481.07	481.069	481.07	0	1
	T2S3	481.07	481.069	481.07	0	1
	T2S4	481.07	481.069	481.07	0	1
	T2V1	481.07	481.069	481.07	0	1
	T2V2	481.07	481.069	481.07	0	1
	T2V3	481.07	481.069	481.07	0	1
	T2V4	481.07	481.069	481.07	0	1
	S 1	1025	1025	1025	0	1.36
	S2	1025	1025	1025	0	1.68
	S 3	1025	1025	1025	0	1.24
	S4	1025	1025	1025	0	1.68
	V1	1025	1025	1025	0	1.68
In Q	V2	1025	1025	1025	0	1.56
кр-о	V3	1025	1025	1025	0	1.52
	V4	1025	1025	1025	0	1.28
	T1S1	1025	1025	1025	0	1.95
	T1S2	1025	1025	1025	0	1.22
	T1S3	1025	1025	1025	0	1.15
	T1S4	1025	1025	1025	0	1.56

Ibn Al-Haitham Int	ernational Conferenc	Pure and Applied Sciences (IHICPS)			IOP Publishing	
Journal of Physics:	Conference Series		1879 (2021) 022097		088/1742-659	6/1879/2/022097
	T1V1	1025	1025	1025	0	1.49
	T1V2	1025	1025	1025	0	1.23
	T1V3	1025	1025	1025	0	1.07
	T1V4	1025	1025	1025	0	1.04
	T2S1	1025	1025	1025	0	2.14
	T2S2	1025	1025	1025	0	1.02
	T2S3	1025	1025	1025	0	1.04
	T2S4	1025	1025	1025	0	1.32
	T2V1	1025	1025	1025	0	1.59
	T2V2	1025	1025	1025	0	1.14
	T2V3	1025	1025	1025	0	1.04
	T2V4	1025	1025	1025	0	1
	S1	1024	1024	1024	0	1.6
	S2	1024	1024	1024	0	1.72
	S 3	1024	1024	1024	0	1.16
	S 4	1024	1024	1024	0	1.92
	V1	1024	1024	1024	0	1.92
	V2	1024	1024	1024	0	2
	V3	1024	1024	1024	0	2.04
	V4	1024	1024	1024	0	1.48
	T1S1	1024	1024	1024	0	2.5
	T1S2	1024	1024	1024	0	1.04
	T1S3	1024	1024	1024	0	1.04
lm 0	T1S4	1024	1024	1024	0	1.21
кр-9	T1V1	1024	1024	1024	0	1.07
	T1V2	1024	1024	1024	0	1.94
	T1V3	1024	1024	1024	0	1.83
	T1V4	1024	1024	1024	0	1.08
	T2S1	1024	1024	1024	0	1.91
	T2S2	1024	1024	1024	0	1.29
	T2S3	1024	1024	1024	0	1.12
	T2S4	1024	1024	1024	0	1.67
	T2V1	1024	1024	1024	0	1.54
	T2V2	1024	1024	1024	0	1.44
	T2V3	1024	1024	1024	0	1.75
	T2V4	1024	1024	1024	0	1

Table S3: Medium	size 0-1	KP test	problems
------------------	----------	---------	----------

Instance	dimension	capacity M	weights W	profits C
kp-11	30	577	w=[46 17 35 1 26 17 17 48 38 17 32 21 29 48 31 8 42 37 6 9 15 22 27 14 42 40 14 31 6 34]	c=[57 64 50 6 52 6 85 60 70 65 63 96 18 48 85 50 77 18 70 92 17 43 5 23 67 88 35 3 91 48]
kp-12	35	655	w=[7 4 36 47 6 33 8 35 32 3 40 50 22 18 3 12 30 31 13 33 4 48 5 17 33 26 27 19 39 15 33 47 17 41 40]	c=[35 67 30 69 40 40 21 73 82 93 52 20 61 20 42 86 43 93 38 70 59 11 42 93 6 39 25 23 36 93 51 81 36 46 96]

Ibn Al-Hai	tham Intern	ational Conf	erence for Pure and Applied Sciences (IHI	CPS) IOP Publishing
Journal of	Physics: Co	nference Ser	ies 1879 (2021) 022097 doi	:10.1088/1742-6596/1879/2/022097
kp-13	40	819	w=[28 23 35 38 20 29 11 48 26 14 12 48 35 36 33 39 30 26 44 20 13 15 46 36 43 19 32 2 47 24 26 39 17 32 17 16 33 22 6 12]	c=[13 16 42 69 66 68 1 13 77 85 75 95 92 23 51 79 53 62 56 74 7 50 23 34 56 75 42 51 13 22 30 45 25 27 90 59 94 62 26 111
kp-14	45	907	w=[18 12 38 12 23 13 18 46 1 7 20 43 11 47 49 19 50 7 39 29 32 25 12 8 32 41 34 24 48 30 12 35 17 38 50 14 47 35 5 13 47 24 45 39 1]	c=[98 70 66 33 2 58 4 27 20 45 77 63 32 30 8 18 73 9 92 43 8 58 84 35 78 71 60 38 40 43 43 22 50 4 57 5 88 87 34 98 96 99 16 1 25]
kp-15	50	882	w=[15 40 22 28 50 35 49 5 45 3 7 32 19 16 40 16 31 24 15 42 29 4 14 9 29 11 25 37 48 39 5 47 49 31 48 17 46 1 25 8 16 9 30 33 18 3 3 3 4 1]	c=[78 69 87 59 63 12 22 4 45 33 29 50 19 94 95 60 1 91 69 8 100 32 81 47 59 48 56 18 59 16 45 54 47 84 100 98 75 20 4 19 58 63 37 64 90 26 29 13 53 83]
kp-16	55	1050	w=[27 15 46 5 40 9 36 12 11 11 49 20 32 3 12 44 24 1 24 42 44 16 12 42 22 26 10 8 46 50 20 42 48 45 43 35 9 12 22 2 14 50 16 29 31 46 20 35 11 4 32 35 15 29 16]	c=[98 74 76 4 12 27 90 98 100 35 30 19 75 72 19 44 5 66 79 87 79 44 35 6 82 11 1 28 95 68 39 86 68 61 44 97 83 2 15 49 59 30 44 40 14 96 37 84 5 43 8 32 95 86 18]
kp-17	60	1006	w=[7 13 47 33 38 41 3 21 37 7 32 13 42 42 23 20 49 1 20 25 31 4 8 33 11 6 3 9 26 44 39 7 4 34 25 25 16 17 46 23 38 10 5 11 28 34 47 3 9 22 17 5 41 20 33 29 1 33 16 14]	c=[81 37 70 64 97 21 60 9 55 85 5 33 71 87 51 100 43 27 48 17 16 27 76 61 97 78 58 46 29 76 10 11 74 36 59 30 72 37 72 100 9 47 10 73 92 9 52 56 69 30 61 20 66 70 46 16 43 60 33 84]
kp-18	65	1319	$ w = [47\ 27\ 24\ 27\ 17\ 17\ 50\ 24\ 38\ 34 \\ 40\ 14\ 15\ 36\ 10\ 42\ 9\ 48\ 37\ 7\ 43 \\ 47\ 29\ 20\ 23\ 36\ 14\ 2\ 48\ 50\ 39 \\ 50\ 25\ 7\ 24\ 38\ 34\ 44\ 38\ 31\ 14 \\ 17\ 42\ 20\ 5\ 44\ 22\ 9\ 1\ 33\ 19\ 19 \\ 23\ 26\ 16\ 24\ 1\ 9\ 16\ 38\ 30\ 36\ 41 \\ 43\ 6] $	$c=[47\ 63\ 81\ 57\ 3\ 80\ 28\ 83\ 69\\ 61\ 39\ 7\ 100\ 67\ 23\ 10\ 25\ 91\\ 22\ 48\ 91\ 20\ 45\ 62\ 60\ 67\ 27\\ 43\ 80\ 94\ 47\ 31\ 44\ 31\ 28\ 14\\ 17\ 50\ 9\ 93\ 15\ 17\ 72\ 68\ 36\\ 10\ 1\ 38\ 79\ 45\ 10\ 81\ 66\ 46\\ 54\ 53\ 63\ 65\ 20\ 81\ 20\ 42\ 24\\ 28\ 1]$
kp-19	70	1426	w=[4 16 16 2 9 44 33 43 14 45 11 49 21 12 41 19 26 38 42 20 5 14 40 47 29 47 30 50 39 10 26 33 44 31 50 7 15 24 7 12 10 34 17 40 28 12 35 3 29 50 19 28 47 13 42 9 44 14 43 41 10 49 13 39 41 25 46 6 7 43]	$ \begin{array}{c} c = \begin{bmatrix} 66 & 76 & 71 & 61 & 4 & 20 & 34 & 65 & 22 & 8 \\ 99 & 21 & 99 & 62 & 25 & 52 & 72 & 26 & 12 \\ 55 & 22 & 32 & 98 & 31 & 95 & 42 & 2 & 32 \\ 16 & 100 & 46 & 55 & 27 & 89 & 11 & 83 \\ 43 & 93 & 53 & 88 & 36 & 41 & 60 & 92 & 14 \\ 5 & 41 & 60 & 92 & 30 & 55 & 79 & 33 & 10 \\ 45 & 3 & 68 & 12 & 20 & 54 & 63 & 38 & 61 \\ 85 & 71 & 40 & 58 & 25 & 73 & 351 \\ \end{array} $
kp-20	75	1433	w=[24 45 15 40 9 37 13 5 43 35 48 50 27 46 24 45 2 7 38 20 20 31 2 20 3 35 27 4 21 22 33 11 5 24 37 31 46 13 12 12 41 36 44 36 34 22 29 50 48 17 8 21 28 2	c=[2 73 82 12 49 35 78 29 83 18 87 93 20 6 55 1 83 91 71 25 59 94 90 61 80 84 57 1 26 44 44 88 7 34 18 25 73 29 24 14 23 82 38 67 94 43 (1 07 27 67 22 80 20 20 01

61 97 37 67 32 89 30 30 91

Ibn Al-Haitham International Conference	IOP Publishing		
Journal of Physics: Conference Series	1879 (2021) 022097	doi:10.1088/1742-659	6/1879/2/022097
2	44 45 25 11 37 35 24 9 40 4	5 8 50 21 3 18	31 97 79 68 85

4 45 25 11 37 35 24 9 40 45 8	50 21 3 18 31 97 79 68 85
47 1 22 1 12 36 35 14 17 5]	43 71 49 83 44 86 1 100 28
	4 16]

	Transfer					Mean
Instance	function	Best	Mean	Worst	SD	iterations
	S1	1437	1437	1437	0	2.48
	S2	1437	1437	1437	0	7.8
	S 3	1437	1437	1437	0	6.96
	S 4	1437	1437	1437	0	4.92
	V1	1437	1437	1437	0	1.84
	V2	1437	1437	1437	0	2.04
	V3	1437	1437	1437	0	1.24
	V 4	1437	1437	1437	0	1.12
kp-11	T1S1	1437	1437	1437	0	5.7
ľ	T1S2	1437	1437	1437	0	3.56
	T1S3	1437	1437	1437	0	5.81
	T1S4	1437	1437	1437	0	4.17
	T1V1	1437	1437	1437	0	1.14
	T1V2	1437	1437	1437	0	1.94
	T1V3	1437	1437	1437	0	1.08
	T1V4	1437	1437	1437	0	1.04
	T2S1	1437	1437	1437	0	3.87
	T2S2	1437	1437	1437	0	3.92
	T2S3	1437	1437	1437	0	4.91
	T2S4	1437	1437	1437	0	2.55
	T2V1	1437	1437	1437	0	1.04
	T2V2	1437	1437	1437	0	1.37
	T2V3	1437	1437	1437	0	1
	T2V4	1437	1437	1437	0	1
	S1	1689	1689	1689	0	3.8
	S2	1689	1689	1689	0	7.96
	S 3	1689	1689	1689	0	4.88
	S 4	1689	1689	1689	0	3.76
	V1	1689	1689	1689	0	2.2
	V2	1689	1689	1689	0	1.92
kp-12	V3	1689	1689	1689	0	1.68
_	V4	1689	1689	1689	0	1.36
	T1S1	1689	1689	1689	0	4.24
	T1S2	1689	1689	1689	0	3.6
	T1S3	1689	1689	1689	0	3.48
	T1S4	1689	1689	1689	0	3.8
	T1V1	1689	1689	1689	0	1.04

Table S4: Results obtained by the transfer functions for the medium scale 0-1 KP

Ibn Al-Haitham Interna	tional Conference	e for Pure	and Applied Sci	ences (IHICPS)	IOP Publishing
Journal of Physics: Cor	nference Series		1879 (2021) 022	2097 doi:10.	1088/1742-0	6596/1879/2/022097
	T1V2	1689	1689	1689	0	1.16
	T1V3	1689	1689	1689	0	1.04
	T1V4	1689	1689	1689	0	1.04
	T2S1	1689	1689	1689	0	4.88
	T2S2	1689	1689	1689	0	3.8
	T2S3	1689	1689	1689	0	4.64
	T2S4	1689	1689	1689	0	3.16
	T2V1	1689	1689	1689	0	1.24
	T2V2	1689	1689	1689	0	1
	T2V3	1689	1689	1689	0	1.08
	T2V4	1689	1689	1689	0	1
	S 1	1821	1821	1821	0	8.28
	S2	1821	1821	1821	0	37.8
	S 3	1821	1821	1821	0	22.2
	S4	1821	1821	1821	0	17.92
	V1	1821	1821	1821	0	4.56
	V2	1821	1821	1821	0	3.72
	V3	1821	1821	1821	0	2.68
	V4	1821	1821	1821	0	1.96
	T1S1	1821	1821	1821	0	11.56
	T1S2	1821	1821	1821	0	22.41
	T1S3	1821	1821	1821	0	16.63
1 10	T1S4	1821	1821	1821	0	12.65
kp-13	T1V1	1821	1821	1821	0	3.47
	T1V2	1821	1821	1821	0	2.34
	T1V3	1821	1821	1821	0	1.94
	T1V4	1821	1821	1821	0	1.04
	T2S1	1821	1821	1821	0	9 53
	T2S1	1821	1821	1821	Ő	193
	T2S2	1821	1821	1821	0	18.66
	T2S3	1821	1821	1821	0	10.06
	T2V1	1821	1821	1821	0	1.9/
	T2V1 T2V2	1821	1821	1821	0	1.74
	12V2 T2V2	1021	1821	1821	0	1.15
	12V3	1021	1021	1021	0	1.55
	<u>12V4</u> S1	2022	2022	2033	0	3.28
	S1 S2	2033	2033	2033	0	3.28
	S2 S3	2033	2033	2033	0	22
	S4	2033	2033	2033	0	22.88
	V1	2033	2033	2033	0	3 52
kn-14	V2	2033	2033	2033	0	2.32
~r · ·	V3	2033	2033	2033	Ő	2.08
	V4	2033	2033	2033	0	1.48
	T1S1	2033	2033	2033	0	5.19
	T1S2	2033	2033	2033	0	14.55
	T1S3	2033	2033	2033	0	20.12

Journal of Physics: Conference Series 1879 (2021) 02207 doi:10.1088/1742-6596/1879/2/022097 TIV3 2033 2033 0 1.9.49 TIV1 2003 20033 0 1.42 TIV2 2003 20033 0 1.42 TIV3 2003 20033 0 1.42 TIV4 2003 20033 0 1.94 T2S1 2003 20033 0 3.92 T2S2 2003 20033 0 1.94 T2V1 2003 20033 0 1.04 T2V2 2003 20033 0 1.04 T2V2 2003 20033 0 1.04 T2V2 2003 2033 0 1.04 T2V2 2033 2033 0 1.04 T2V2 2033 2033 0 1.04 T2V2 2033 2033 0 1.04 T2V4 2033 2033 0 1	Ibn A	Al-Haitham Interna	ational Conferenc	e for Pure	r Pure and Applied Sciences (IHICPS)			<u>IOP</u> Publishing	
$k_{p-16} = \begin{array}{ccccccccccccccccccccccccccccccccccc$	Journ	nal of Physics: Con	nference Series		1879 (2021) 022	2097 doi:10.	1088/1742-6	596/1879/2/022097	
TiS4 2033 2033 2033 0 19.49 TiV1 2033 2033 2033 0 1.42 TiV2 2033 2033 2033 0 1.42 TiV2 2033 2033 0 1.19 TiV4 2033 2033 0 3.92 T2S2 2033 2033 0 3.92 T2S2 2033 2033 0 1.94 T2V1 2033 2033 0 1.95 T2S2 2033 2033 0 1.14 T2V2 2033 2033 0 1.14 T2V2 2033 2033 0 1.04 S1 2651 2651 26									
TIS4 2033 2033 2033 0 19.49 TIV1 2033 2033 0 1.42 TIV2 2033 2033 0 1.42 TIV3 2033 2033 0 1.42 TIV3 2033 2033 0 1.04 TSE 2033 2033 0 1.04 TZS2 2033 2033 0 1.295 T2S2 2033 2033 0 1.788 T2V1 2033 2033 0 1.04 T2V2 2033 2033 0 1.04 T2V2 2033 2033 0 1.04 T2V3 2033 2033 0 1.04 T2V4 2033 2033 0 1.04 T2V2 2033 2033 0 1.04 T2V3 2033 2033 0 1.04 V3 2651 2651 0 1.56 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>									
trivi 2033 2033 2033 0 1.42 TiV2 2033 2033 2033 0 1.42 TiV3 2033 2033 0 1.19 TiV4 2033 2033 0 1.42 T2S1 2033 2033 0 3.92 T2S2 2033 2033 0 12.95 T2S3 2033 2033 0 1.494 T2V1 2033 2033 0 1.08 T2V2 2033 2033 0 1.04 T2V4 2033 2033 0 1.04 V2 2651 2651 2651 0 423.53 S4 2651 2651			T1S4	2033	2033	2033	0	19.49	
kp-16 T1V2 2033 2033 2033 0 1.42 T1V3 2033 2033 2033 0 1.04 T2S1 2033 2033 2033 0 1.04 T2S2 2033 2033 2033 0 1.295 T2S3 2033 2033 0 1.494 T2V1 2033 2033 0 1.494 T2V2 2033 2033 0 1.08 T2V2 2033 2033 0 1.04 T2V2 2033 2033 0 1.04 T2V4 2033 2033 0 1.04 T2V4 2033 2033 0 1.04 S2 2651 2651 2651 0 13.56 S2 2651 2651 2651 0 3.23 360.6 V1 2651 2651 2651 0 9.12 3.23 360.6 V1			T1V1	2033	2033	2033	0	1.42	
kp-16 T1V3 2033 2033 2033 0 1.19 T1V4 2033 2033 2033 0 3.92 T2S1 2033 2033 2033 0 1.295 T2S2 2033 2033 2033 0 1.7.88 T2S4 2033 2033 2033 0 1.4.94 T2V1 2033 2033 2033 0 1.04 T2V2 2033 2033 2033 0 1.04 T2V3 2033 2033 0 1.04 1.22 T2V4 2033 2033 0 1.04 1.356 V1 2651 2651 2651 0 1.356 V2 2651 2651 2651 <td></td> <td></td> <td>T1V2</td> <td>2033</td> <td>2033</td> <td>2033</td> <td>0</td> <td>1.42</td>			T1V2	2033	2033	2033	0	1.42	
TIV4 2033 2033 2033 0 1.04 T2S1 2033 2033 2033 0 12.95 T2S2 2033 2033 2033 0 17.88 T2S4 2033 2033 0 14.94 T2V1 2033 2033 0 1.04 T2V2 2033 2033 0 1.04 T2V3 2033 2033 0 1.04 T2V4 2033 2033 0 1.04 S3 2651 2651 0 13.56 S2 2651 2651 2651 0 13.56 V2 2651 2651 2651 0 3.2 T18 2651 2651 2651 0 3.2 T18 </td <td></td> <td></td> <td>T1V3</td> <td>2033</td> <td>2033</td> <td>2033</td> <td>0</td> <td>1.19</td>			T1V3	2033	2033	2033	0	1.19	
T2S1 2033 2033 2033 0 3.92 T2S2 2033 2033 2033 0 12.95 T2S4 2033 2033 2033 0 17.88 T2S4 2033 2033 2033 0 1.494 T2V1 2033 2033 0 1.12 T2V2 2033 2033 0 1.04 T2V4 2033 2033 0 1.04 S2 2651 2651 0 1.04 S3 2651 2651 2651 0 1.356 S4 2651 2651 2651 0 3.2 V1 2651 2651 2651 0 3.2 <t< td=""><td></td><td></td><td>T1V4</td><td>2033</td><td>2033</td><td>2033</td><td>0</td><td>1.04</td></t<>			T1V4	2033	2033	2033	0	1.04	
T2S2 2033 2033 2033 0 12.95 T2S3 2033 2033 2033 0 17.88 T2V1 2033 2033 2033 0 14.94 T2V1 2033 2033 0 1.08 T2V2 2033 2033 0 1.04 T2V4 2033 2033 0 1.04 S1 2651 2651 0 13.56 S2 2651 2651 2651 0 3.23 V1 2651 265			T2S1	2033	2033	2033	0	3.92	
T2S3 2033 2033 2033 0 17.88 T2V1 2033 2033 0 1.4.94 T2V1 2033 2033 0 1.08 T2V2 2033 2033 0 1.04 T2V3 2033 2033 0 1.04 T2V4 2033 2033 0 1.04 S1 2651 2651 0 1.356 S2 2651 2651 2651 0 11.36 V1 2651 2651 2651 0 3.2 T1S1 2651 2651 2651 0 3.2 T1S2 2651 2651 2651 0 3.2 T1S3 2651<			T2S2	2033	2033	2033	0	12.95	
$ kp-16 $ $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			T2S3	2033	2033	2033	0	17.88	
$kp-16 = \begin{bmatrix} T2V1 & 2033 & 2033 & 2033 & 0 & 1.08 \\ T2V2 & 2033 & 2033 & 2033 & 0 & 1.04 \\ T2V4 & 2033 & 2033 & 2033 & 0 & 1.04 \\ T2V4 & 2033 & 2033 & 2033 & 0 & 1.04 \\ \hline T2V4 & 2033 & 2033 & 2033 & 0 & 1.04 \\ \hline S1 & 2651 & 2651 & 2651 & 0 & 13.56 \\ \hline S2 & 2651 & 2650.2 & 2647 & 1.69 & 524.3 \\ \hline S3 & 2651 & 2650.2 & 2643 & 2.53 & 360.6 \\ \hline V1 & 2651 & 2651 & 2651 & 0 & 11.36 \\ \hline V2 & 2651 & 2651 & 2651 & 0 & 9.12 \\ \hline V3 & 2651 & 2651 & 2651 & 0 & 9.12 \\ \hline V3 & 2651 & 2651 & 2651 & 0 & 3.2 \\ \hline T1S1 & 2651 & 2651 & 2651 & 0 & 3.47.16 \\ \hline T1S2 & 2651 & 2651 & 2651 & 0 & 20.82 \\ \hline T1S2 & 2651 & 2651 & 2651 & 0 & 347.16 \\ \hline T1S2 & 2651 & 2651 & 2651 & 0 & 348 \\ \hline T1V2 & 2651 & 2651 & 2651 & 0 & 318 \\ \hline T1V2 & 2651 & 2651 & 2651 & 0 & 3.92 \\ \hline T1V3 & 2651 & 2651 & 2651 & 0 & 3.92 \\ \hline T1V4 & 2651 & 2651 & 2651 & 0 & 3.92 \\ \hline T1V4 & 2651 & 2651 & 2651 & 0 & 3.92 \\ \hline T1V4 & 2651 & 2651 & 2651 & 0 & 3.92 \\ \hline T1V4 & 2651 & 2651 & 2651 & 0 & 3.92 \\ \hline T2S4 & 2651 & 2651 & 2651 & 0 & 3.28.5 \\ \hline T2S2 & 2651 & 2651 & 2651 & 0 & 4.52 \\ \hline T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ \hline T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ \hline T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ \hline T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ \hline T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ \hline T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ \hline T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ \hline T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ \hline T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ \hline T2V4 & 2651 & 2651 & 2651 & 0 & 1.08 \\ \hline S2 & 2917 & 2917 & 2917 & 0 & 81.88 \\ \hline S3 & 2917 & 2917 & 2917 & 0 & 43.84 \\ \hline S4 & 2917 & 2917 & 2917 & 0 & 2.88 \\ \hline V3 & 2917 & 2917 & 2917 & 0 & 2.88 \\ \hline V3 & 2917 & 2917 & 2917 & 0 & 1.8 \\ \hline T1S1 & 2917 & 2917 & 0 & 1.8 \\ \hline T1S2 & 2917 & 2917 & 2917 & 0 & 1.8 \\ \hline T1S1 & 2917 & 2917 & 2917 & 0 & 8.5 \\ \hline T1S2 & 2917 & 2917 & 2917 & 0 & 8.5 \\ \hline T1S2 & 2917 & 2917 & 2917 & 0 & 50.73 \\ \hline \end{array}$			T2S4	2033	2033	2033	0	14.94	
$ kp-16 = \begin{bmatrix} T2V2 & 2033 & 2033 & 2033 & 0 & 1.12 \\ T2V3 & 2033 & 2033 & 2033 & 0 & 1.04 \\ T2V4 & 2033 & 2033 & 2033 & 0 & 1.04 \\ \hline T2V4 & 2033 & 2051 & 2651 & 0 & 13.56 \\ \hline S2 & 2651 & 2650.2 & 2647 & 1.69 & 524.3 \\ \hline S3 & 2651 & 2650.2 & 2643 & 2.53 & 360.6 \\ \hline V1 & 2651 & 2651 & 2651 & 0 & 423.53 \\ \hline V1 & 2651 & 2651 & 2651 & 0 & 9.12 \\ \hline V2 & 2651 & 2651 & 2651 & 0 & 9.12 \\ \hline V3 & 2651 & 2651 & 2651 & 0 & 3.2 \\ \hline T1S2 & 2651 & 2651 & 2651 & 0 & 3.2 \\ \hline T1S2 & 2651 & 2651 & 2651 & 0 & 3.47.16 \\ \hline T1S3 & 2651 & 2651 & 2651 & 0 & 347.16 \\ \hline T1S3 & 2651 & 2651 & 2651 & 0 & 347.16 \\ \hline T1S4 & 2651 & 2651 & 2651 & 0 & 348 \\ \hline T1V2 & 2651 & 2651 & 2651 & 0 & 3.92 \\ \hline T1V2 & 2651 & 2651 & 2651 & 0 & 3.92 \\ \hline T1V3 & 2651 & 2651 & 2651 & 0 & 3.92 \\ \hline T1V3 & 2651 & 2651 & 2651 & 0 & 3.92 \\ \hline T1V3 & 2651 & 2651 & 2651 & 0 & 3.92 \\ \hline T1V4 & 2651 & 2651 & 2651 & 0 & 3.92 \\ \hline T2S4 & 2651 & 2651 & 2651 & 0 & 328.5 \\ \hline T2V4 & 2651 & 2651 & 2651 & 0 & 328.5 \\ \hline T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ \hline T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ \hline T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ \hline T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ \hline T2V4 & 2651 & 2651 & 2651 & 0 & 3.98 \\ \hline Re -17 & \hline S1 & 2917 & 2917 & 0 & 81.88 \\ \hline S3 & 2917 & 2917 & 2917 & 0 & 43.84 \\ \hline S4 & 2917 & 2917 & 2917 & 0 & 43.84 \\ \hline S4 & 2917 & 2917 & 2917 & 0 & 2.88 \\ \hline V1 & 2917 & 2917 & 2917 & 0 & 2.88 \\ \hline V3 & 2917 & 2917 & 2917 & 0 & 1.8 \\ \hline T1S2 & 2917 & 2917 & 2917 & 0 & 1.8 \\ \hline T1S1 & 2917 & 2917 & 2917 & 0 & 8.5 \\ \hline T1S2 & 2917 & 2917 & 2917 & 0 & 8.5 \\ \hline T1S2 & 2917 & 2917 & 2917 & 0 & 8.5 \\ \hline T1S2 & 2917 & 2917 & 2917 & 0 & 8.5 \\ \hline T1S2 & 2917 & 2917 & 2917 & 0 & 8.5 \\ \hline T1S2 & 2917 & 2917 & 2917 & 0 & 8.5 \\ \hline T1S2 & 2917 & 2917 & 2917 & 0 & 8.5 \\ \hline T1S2 & 2917 & 2917 & 2917 & 0 & 8.5 \\ \hline T1S2 & 2917 & 2917 & 2917 & 0 & 8.5 \\ \hline T1S2 & 2917 & 2917 & 2917 & 0 & 8.5 \\ \hline T1S2 & 2917 & 2917 & 2917 & 0 & 5.073 \\ \hline \end{array}$			T2V1	2033	2033	2033	0	1.08	
$ kp-16 = \begin{bmatrix} 12V3 & 2033 & 2033 & 2033 & 0 & 1.04 \\ 12V4 & 2033 & 2033 & 2033 & 0 & 1.04 \\ S1 & 2651 & 2650 & 2631 & 0 & 13.56 \\ S2 & 2651 & 2650 & 2647 & 1.69 & 524.3 \\ S3 & 2651 & 2650 & 2643 & 2.53 & 360.6 \\ V1 & 2651 & 2651 & 2651 & 0 & 11.36 \\ V2 & 2651 & 2651 & 2651 & 0 & 11.36 \\ V2 & 2651 & 2651 & 2651 & 0 & 5.04 \\ V4 & 2651 & 2651 & 2651 & 0 & 3.2 \\ T1S1 & 2651 & 2651 & 2651 & 0 & 3.2 \\ T1S2 & 2651 & 2651 & 2651 & 0 & 347.16 \\ T1S3 & 2651 & 2651 & 2651 & 0 & 318 \\ T1V2 & 2651 & 2651 & 2651 & 0 & 318 \\ T1V2 & 2651 & 2651 & 2651 & 0 & 318 \\ T1V2 & 2651 & 2651 & 2651 & 0 & 3.92 \\ T1V2 & 2651 & 2651 & 2651 & 0 & 3.92 \\ T1V2 & 2651 & 2651 & 2651 & 0 & 3.92 \\ T1V2 & 2651 & 2651 & 2651 & 0 & 1.93 \\ T1V2 & 2651 & 2651 & 2651 & 0 & 1.93 \\ T1V2 & 2651 & 2651 & 2651 & 0 & 1.93 \\ T2S2 & 2651 & 2651 & 2651 & 0 & 1.93 \\ T2S2 & 2651 & 2651 & 2651 & 0 & 328.5 \\ T2S3 & 2651 & 2651 & 2651 & 0 & 328.5 \\ T2S4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 3.94 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 3.94 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 3.94 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 3.94 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 3.94 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 3.94 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V3 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 3.52 \\ V2 & 2917 & 2917 & 2917 & 0 & 43.84 \\ S4 & 2917 & 2917 & 2917 & 0 & 43.84 \\ S4 & 2917 & 2917 & 2917 & 0 & 43.84 \\ S4 & 2917 & 2917 & 2917 & 0 & 2.88 \\ V3 & 2917 & 2917 & 2917 & 0 & 2.88 \\ V3 & 2917 & 2917 & 2917 & 0 & 1.8 \\ T1S1 & 2917 & 2917 & 2917 & 0 & 1.8 \\ T1S1 & 2917 & 2917 & 2917 & 0 & 1.8 \\ T1S1 & 2917 & 2917 & 2917 & 0 & 50.73 \\ \end{bmatrix}$			T2V2	2033	2033	2033	0	1.12	
$ \frac{12}{kp-16} + \frac{12}{kp-17} + 1$			T2V3	2033	2033	2033	0	1.04	
$k_{p-16} = \begin{bmatrix} S1 & 2651 & 2651 & 2651 & 0 & 13.56 \\ S2 & 2651 & 2650.2 & 2647 & 1.69 & 524.3 \\ S3 & 2651 & 2650.2 & 2643 & 2.53 & 360.6 \\ V1 & 2651 & 2651 & 2651 & 0 & 11.36 \\ V2 & 2651 & 2651 & 2651 & 0 & 9.12 \\ V3 & 2651 & 2651 & 2651 & 0 & 5.04 \\ V4 & 2651 & 2651 & 2651 & 0 & 3.2 \\ T1S2 & 2651 & 2651 & 2651 & 0 & 347.16 \\ T1S2 & 2651 & 2651 & 2651 & 0 & 347.16 \\ T1S3 & 2651 & 2651 & 2651 & 0 & 347.16 \\ T1S3 & 2651 & 2651 & 2651 & 0 & 318 \\ T1V2 & 2651 & 2651 & 2651 & 0 & 3.92 \\ T1V2 & 2651 & 2651 & 2651 & 0 & 3.92 \\ T1V2 & 2651 & 2651 & 2651 & 0 & 3.92 \\ T1V2 & 2651 & 2651 & 2651 & 0 & 3.92 \\ T1V4 & 2651 & 2651 & 2651 & 0 & 1.9 \\ T2S1 & 2651 & 2651 & 2651 & 0 & 1.9 \\ T2S1 & 2651 & 2651 & 2651 & 0 & 1.9 \\ T2S3 & 2651 & 2651 & 2651 & 0 & 328.5 \\ T2V1 & 2651 & 2651 & 2651 & 0 & 328.5 \\ T2V1 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V1 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V2 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V1 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V2 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ S2 & 2917 & 2917 & 2917 & 0 & 42.88 \\ S3 & 2917 & 2917 & 2917 & 0 & 42.88 \\ V3 & 2917 & 2917 & 2917 & 0 & 42.88 \\ V3 & 2917 & 2917 & 2917 & 0 & 4.88 \\ V3 & 2917 & 2917 & 2917 & 0 & 4.88 \\ V3 & 2917 & 2917 & 2917 & 0 & 4.88 \\ V3 & 2917 & 2917 & 2917 & 0 & 4.88 \\ V3 & 2917 & 2917 & 2917 & 0 & 4.88 \\ V3 & 2917 & 2917 & 2917 & 0 & 4.58 \\ V3 & 2917 & 2917 & 2917 & 0 & 4.58 \\ V3 & 2917 & 2917 & 2917 & 0 & 50.73 \\ \end{array}$	_		T2V4	2033	2033	2033	0	1.04	
$kp-16 = \begin{cases} 82 & 2651 & 2650.2 & 2647 & 1.69 & 524.3 \\ 83 & 2651 & 2651 & 2651 & 0 & 423.53 \\ 84 & 2651 & 2650.2 & 2643 & 2.53 & 360.6 \\ 11.36 & 122 & 2651 & 2651 & 0 & 11.36 \\ 122 & 2651 & 2651 & 2651 & 0 & 9.12 \\ 123 & 2651 & 2651 & 2651 & 0 & 5.04 \\ 124 & 2651 & 2651 & 2651 & 0 & 3.2 \\ 1181 & 2651 & 2651 & 2651 & 0 & 3.2 \\ 1182 & 2651 & 2651 & 2651 & 0 & 347.16 \\ 1183 & 2651 & 2651 & 2651 & 0 & 347.16 \\ 1184 & 2651 & 2651 & 2651 & 0 & 318 \\ 1112 & 2651 & 2651 & 2651 & 0 & 3.92 \\ 1112 & 2651 & 2651 & 2651 & 0 & 3.92 \\ 1112 & 2651 & 2651 & 2651 & 0 & 3.92 \\ 1112 & 2651 & 2651 & 2651 & 0 & 3.92 \\ 1112 & 2651 & 2651 & 2651 & 0 & 3.92 \\ 1112 & 2651 & 2651 & 2651 & 0 & 3.92 \\ 1112 & 2651 & 2651 & 2651 & 0 & 3.92 \\ 1112 & 2651 & 2651 & 2651 & 0 & 3.92 \\ 1123 & 2651 & 2651 & 2651 & 0 & 3.92 \\ 1124 & 2651 & 2651 & 2651 & 0 & 3.92 \\ 1124 & 2651 & 2651 & 2651 & 0 & 3.92 \\ 1124 & 2651 & 2651 & 2651 & 0 & 3.92 \\ 1124 & 2651 & 2651 & 2651 & 0 & 3.92 \\ 1124 & 2651 & 2651 & 2651 & 0 & 3.92 \\ 1124 & 2651 & 2651 & 2651 & 0 & 3.92 \\ 124 & 2651 & 2651 & 2651 & 0 & 3.92 \\ 124 & 2651 & 2651 & 2651 & 0 & 4.52 \\ 124 & 2651 & 2651 & 2651 & 0 & 4.52 \\ 124 & 2651 & 2651 & 2651 & 0 & 4.52 \\ 124 & 2651 & 2651 & 2651 & 0 & 4.52 \\ 124 & 2651 & 2651 & 2651 & 0 & 4.52 \\ 124 & 2651 & 2651 & 2651 & 0 & 4.52 \\ 124 & 2651 & 2651 & 2651 & 0 & 4.52 \\ 124 & 2917 & 2917 & 2917 & 0 & 81.88 \\ 83 & 2917 & 2917 & 2917 & 0 & 4.288 \\ 83 & 2917 & 2917 & 2917 & 0 & 4.288 \\ 83 & 2917 & 2917 & 2917 & 0 & 4.288 \\ 83 & 2917 & 2917 & 2917 & 0 & 4.288 \\ 83 & 2917 & 2917 & 2917 & 0 & 4.288 \\ 83 & 2917 & 2917 & 2917 & 0 & 4.288 \\ 83 & 2917 & 2917 & 2917 & 0 & 4.288 \\ 83 & 2917 & 2917 & 2917 & 0 & 4.288 \\ 83 & 2917 & 2917 & 2917 & 0 & 4.288 \\ 85 & 2917 & 2917 & 2917 & 0 & 4.288 \\ 85 & 2917 & 2917 & 2917 & 0 & 4.288 \\ 85 & 2917 & 2917 & 2917 & 0 & 4.288 \\ 85 & 2917 & 2917 & 2917 & 0 & 4.52 \\ 1152 & 2917 & 2917 & 2917 & 0 & 5.73 \\ 1152 & 2917 & 2917 & 2917 & 0 & 5.73 \\ 1152 & 2917 & 2917 & 2917 & 0 & 5.73 \\ 1152 & 2917 & 2917 & 2917 & 0 & 5.73 \\ 1152 & 2917 & 2917 & $			S 1	2651	2651	2651	0	13.56	
$k_{p-16} = \frac{83}{12} 2651 2651 2651 2651 0 423.53 360.6 V1 2651 2651 2651 0 11.36 V1 2651 2651 2651 0 9.12 V3 2651 2651 2651 0 5.04 V4 2651 2651 2651 0 3.2 T1S1 2651 2651 2651 0 347.16 T1S2 2651 2651 2651 0 347.16 T1V2 2651 2651 2651 0 349.4 T1V2 2651 2651 2651 0 3.92 T1V4 2651 2651 2651 0 3.92 T1V4 2651 2651 2651 0 3.92 T1V4 2651 2651 2651 0 1.9 T2S1 2651 2651 0 328.5 T2S3 2651 2651 2651 0 328.5 T2S3 2651 2651 0 0 7.15 T2V2 2651 2651 2651 0 328.5 T2S3 2651 2651 0 4.52 T2V3 2651 2651 0 0 1.08 S2 2917 2917 0 43.84 S4 2917 2917 0 43.84 V3 2917 2917 0 42.88 V3 2917 2917 0 1.8 T1S1 2917 2917 0 1.8 T1S1 2917 2917 0 1.8 T1S1 2917 2917 0 5.73$			S2	2651	2650.2	2647	1.69	524.3	
$kp-16 = \frac{84}{1284} = \frac{2651}{2651} = \frac{2650.2}{2651} = \frac{2643}{2651} = \frac{2.53}{0} = \frac{360.6}{9.12}$ $\frac{V1}{2651} = \frac{2651}{2651} = \frac{2651}{0} = 0 = \frac{9.12}{9.12}$ $\frac{V2}{V3} = \frac{2651}{2651} = \frac{2651}{2651} = 0 = \frac{3.2}{9.2}$ $\frac{V4}{V4} = \frac{2651}{2651} = \frac{2651}{2651} = 0 = \frac{3.2}{9.2}$ $\frac{T151}{T152} = \frac{2651}{2651} = \frac{2651}{2651} = 0 = \frac{3.2}{9.2}$ $\frac{T152}{T152} = \frac{2651}{2651} = \frac{2651}{2651} = 0 = \frac{3.4}{9.16}$ $\frac{Kp-16}{T153} = \frac{2651}{2651} = \frac{2651}{2651} = \frac{2651}{0} = 0 = \frac{3.94}{11}$ $\frac{Kp-16}{T152} = \frac{2651}{2651} = \frac{2651}{2651} = \frac{2651}{0} = 0 = \frac{3.92}{11}$ $\frac{T1V2}{2651} = \frac{2651}{2651} = \frac{2651}{2651} = 0 = \frac{3.92}{11}$ $\frac{T1V4}{2651} = \frac{2651}{2651} = \frac{2651}{0} = 0 = \frac{3.92}{11}$ $\frac{T1V4}{2651} = \frac{2651}{2651} = \frac{2651}{0} = 0 = \frac{3.92}{11}$ $\frac{T281}{2651} = \frac{2651}{2651} = \frac{2651}{0} = 0 = \frac{3.28.5}{12}$ $\frac{T284}{2651} = \frac{2651}{2651} = \frac{2651}{0} = 0 = \frac{3.28.5}{12}$ $\frac{T2V4}{2651} = \frac{2651}{2651} = \frac{2651}{0} = 0 = \frac{4.52}{12}$ $\frac{T2V4}{2651} = \frac{2651}{2651} = \frac{2651}{0} = 0 = \frac{4.52}{12}$ $\frac{S1}{2917} = \frac{2917}{2917} = \frac{2917}{0} = \frac{42.88}{1.88}$ $\frac{S3}{3} = \frac{2917}{2917} = \frac{2917}{0} = 0 = \frac{4.58}{1.88}$ $\frac{S4}{3} = \frac{2917}{2917} = \frac{2917}{0} = 0 = \frac{4.58}{1.88}$ $\frac{S4}{3} = \frac{2917}{2917} = \frac{2917}{0} = 0 = \frac{4.58}{1.88}$ $\frac{S1}{3} = \frac{2917}{2917} = \frac{2917}{0} = \frac{2.16}{1.8}$ $\frac{V1}{V1} = \frac{2917}{2917} = \frac{2917}{0} = 0 = \frac{4.58}{1.88}$ $\frac{S1}{V3} = \frac{2917}{2917} = \frac{2917}{0} = 0 = \frac{4.58}{1.88}$ $\frac{S1}{V3} = \frac{2917}{2917} = \frac{2917}{0} = 0 = \frac{4.58}{1.88}$ $\frac{S1}{V3} = \frac{2917}{2917} = \frac{2917}{0} = 0 = \frac{4.58}{1.88}$ $\frac{S1}{V3} = \frac{2917}{2917} = \frac{2917}{0} = \frac{2.16}{1.8}$ $\frac{V1}{V1} = \frac{2917}{2917} = \frac{2917}{0} = 0 = \frac{4.58}{1.88}$ $\frac{S1}{V3} = \frac{2917}{2917} = \frac{2917}{0} = 0 = \frac{4.58}{1.88}$ $\frac{S1}{V3} = \frac{2917}{2917} = \frac{2917}{0} = 0 = \frac{4.58}{1.88}$ $\frac{S1}{V3} = \frac{2917}{2917} = \frac{2917}{0} = 0 = \frac{4.58}{1.88}$ $\frac{S1}{V3} = \frac{2917}{2917} = \frac{2917}{0} = 0 = \frac{5.5}{1.85}$ $\frac{S1}{V3} = \frac{2917}{2917} = \frac{2917}{0} = 0 = \frac{5.5}{1.85}$ $\frac{S1}{V3} = \frac{2917}{2917} = \frac{2917}{0} = \frac{2917}{0} = \frac$			S 3	2651	2651	2651	0	423.53	
$kp-16 = V_1 = 2651 = 2651 = 2651 = 0 = 11.36 = V_2 = 2651 = 2651 = 2651 = 0 = 9.12 = V_3 = 2651 = 2651 = 2651 = 0 = 5.04 = V_4 = 2651 = 2651 = 2651 = 0 = 3.2 = 71.81 = 2651 = 2651 = 2651 = 0 = 347.16 = 71.82 = 2651 = 2651 = 2651 = 0 = 347.16 = 71.83 = 2651 = 2651 = 2651 = 0 = 31.8 = 71.1V_1 = 2651 = 2651 = 2651 = 0 = 3.92 = 71.1V_2 = 2651 = 2651 = 2651 = 0 = 3.92 = 71.1V_2 = 2651 = 2651 = 2651 = 0 = 3.92 = 71.1V_2 = 2651 = 2651 = 2651 = 0 = 3.92 = 71.1V_2 = 2651 = 2651 = 2651 = 0 = 3.92 = 71.1V_2 = 2651 = 2651 = 2651 = 0 = 3.92 = 71.1V_2 = 2651 = 2651 = 2651 = 0 = 3.92 = 71.1V_2 = 2651 = 2651 = 2651 = 0 = 3.92 = 71.1V_2 = 2651 = 2651 = 2651 = 0 = 3.92 = 71.1V_2 = 2651 = 2651 = 2651 = 0 = 3.92 = 72.1V_2 = 2651 = 2651 = 2651 = 0 = 328.5 = 72.84 = 2651 = 2651 = 2651 = 0 = 328.5 = 72.84 = 2651 = 2651 = 2651 = 0 = 7.15 = 72.1V_2 = 2651 = 2651 = 2651 = 0 = 7.15 = 72.1V_2 = 2651 = 2651 = 2651 = 0 = 1.08 = 72.1V_2 = 2651 = 2651 = 2651 = 0 = 1.08 = 51 = 2917 = 2917 = 2917 = 0 = 43.44 = 54 = 2917 = 2917 = 2917 = 0 = 43.44 = 54 = 2917 = 2917 = 2917 = 0 = 3.52 = 72.1V_2 = 2917 = 2917 = 2917 = 0 = 3.51 = 72.1V_2 = 2917 = 2917 = 2917 = 0 = 3.51 = 72.1V_2 = 2$			S4	2651	2650.2	2643	2.53	360.6	
$kp-16 = \begin{array}{c ccccccccccccccccccccccccccccccccccc$			V1	2651	2651	2651	0	11.36	
$k_{p-16} = \frac{V3}{V4} = \frac{2651}{2651} = \frac{2651}{2651} = \frac{2651}{2651} = 0 = \frac{5.04}{3.2}$ $rus = \frac{V4}{T181} = \frac{2651}{2651} = \frac{2651}{2651} = \frac{2651}{2651} = 0 = \frac{3.2}{20.82}$ $rus = \frac{7182}{T182} = \frac{2651}{2651} = \frac{2651}{2651} = \frac{2651}{2651} = 0 = \frac{318}{20.82}$ $rus = \frac{7184}{T184} = \frac{2651}{2651} = \frac{2651}{2651} = 0 = \frac{318}{2651}$ $rus = \frac{2651}{T184} = \frac{2651}{2651} = \frac{2651}{2651} = 0 = \frac{318}{2651}$ $rus = \frac{2651}{T184} = \frac{2651}{2651} = \frac{2651}{2651} = 0 = \frac{318}{2651}$ $rus = \frac{2651}{T184} = \frac{2651}{2651} = \frac{2651}{2651} = 0 = \frac{318}{2651}$ $rus = \frac{2651}{T184} = \frac{2651}{2651} = \frac{2651}{2651} = 0 = \frac{328.5}{2651}$ $rus = \frac{2651}{T284} = \frac{2651}{2651} = \frac{2651}{2651} = 0 = \frac{23.96}{7284}$ $rus = \frac{2651}{2651} = \frac{2651}{2651} = \frac{2651}{2651} = 0 = \frac{23.96}{7284}$ $rus = \frac{2651}{2651} = \frac{2651}{2651} = \frac{2651}{2651} = 0 = \frac{29.4}{252}$ $rus = \frac{2917}{2917} = \frac{2917}{2917} = \frac{2917}{2917} = 0 = \frac{3.88}{3.5}$ $rus = \frac{83}{2917} = \frac{2917}{2917} = \frac{2917}{2917} = 0 = \frac{2.88}{3.5}$ $rus = \frac{2917}{2917} = \frac{2917}{2917} = \frac{2917}{2917} = 0 = \frac{3.85}{3.5}$ $rus = \frac{2917}{2917} = \frac{2917}{2917} = \frac{2917}{2917} = 0 = \frac{3.85}{3.5}$ $rus = \frac{2917}{2917} = \frac{2917}{2917} = \frac{2917}{2917} = 0 = \frac{3.85}{3.5}$			V2	2651	2651	2651	0	9.12	
$kp-16 = \begin{cases} V4 & 2651 & 2651 & 2651 & 0 & 3.2 \\ T1S1 & 2651 & 2651 & 2651 & 0 & 20.82 \\ T1S2 & 2651 & 2651 & 2651 & 0 & 347.16 \\ T1S3 & 2651 & 2651 & 2651 & 0 & 318 \\ T1V1 & 2651 & 2651 & 2651 & 0 & 8.94 \\ T1V2 & 2651 & 2651 & 2651 & 0 & 6.78 \\ T1V3 & 2651 & 2651 & 2651 & 0 & 3.92 \\ T1V4 & 2651 & 2651 & 2651 & 0 & 1.9 \\ T2S1 & 2651 & 2651 & 2651 & 0 & 15.34 \\ T2S2 & 2651 & 2651 & 2651 & 0 & 328.5 \\ T2S4 & 2651 & 2651 & 2651 & 0 & 328.5 \\ T2V1 & 2651 & 2651 & 2651 & 0 & 6.95 \\ T2V1 & 2651 & 2651 & 2651 & 0 & 6.95 \\ T2V1 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V2 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V3 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ Y3 & 2917 & 2917 & 2917 & 0 & 81.88 \\ S3 & 2917 & 2917 & 2917 & 0 & 43.44 \\ S4 & 2917 & 2917 & 2917 & 0 & 43.44 \\ S4 & 2917 & 2917 & 2917 & 0 & 43.84 \\ V1 & 2917 & 2917 & 2917 & 0 & 2.86 \\ V3 & 2917 & 2917 & 2917 & 0 & 1.8 \\ T1S1 & 2917 & 2917 & 2917 & 0 & 8.5 \\ T1S2 & 2917 & 2917 & 2917 & 0 & 8.5 \\ T1S2 & 2917 & 2917 & 2917 & 0 & 8.5 \\ T1S2 & 2917 & 2917 & 2917 & 0 & 50.73 \\ \end{array}$			V3	2651	2651	2651	0	5.04	
$k_{p-16} = \begin{bmatrix} T1S1 & 2651 & 2651 & 2651 & 0 & 20.82 \\ T1S2 & 2651 & 2651 & 2651 & 0 & 347.16 \\ T1S3 & 2651 & 2651 & 2651 & 0 & 318 \\ T1V1 & 2651 & 2651 & 2651 & 0 & 8.94 \\ T1V2 & 2651 & 2651 & 2651 & 0 & 6.78 \\ T1V3 & 2651 & 2651 & 2651 & 0 & 1.9 \\ T2S1 & 2651 & 2651 & 2651 & 0 & 1.9 \\ T2S2 & 2651 & 2651 & 2651 & 0 & 328.5 \\ T2S3 & 2651 & 2651 & 2651 & 0 & 328.5 \\ T2S4 & 2651 & 2651 & 2651 & 0 & 328.5 \\ T2V1 & 2651 & 2651 & 2651 & 0 & 6.95 \\ T2V1 & 2651 & 2651 & 2651 & 0 & 6.95 \\ T2V1 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V2 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V3 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 1.08 \\ S1 & 2917 & 2917 & 2917 & 0 & 81.88 \\ S3 & 2917 & 2917 & 2917 & 0 & 43.44 \\ S4 & 2917 & 2917 & 2917 & 0 & 43.44 \\ S4 & 2917 & 2917 & 2917 & 0 & 2.88 \\ V1 & 2917 & 2917 & 2917 & 0 & 1.8 \\ T1S1 & 2917 & 2917 & 2917 & 0 & 8.5 \\ T1S2 & 2917 & 2917 & 2917 & 0 & 8.5 \\ T1S2 & 2917 & 2917 & 2917 & 0 & 8.5 \\ T1S2 & 2917 & 2917 & 2917 & 0 & 50.73 \\ \end{bmatrix}$			V4	2651	2651	2651	0	3.2	
$k_{p-16} = \begin{bmatrix} T1S2 & 2651 & 2651 & 2651 & 0 & 347.16 \\ T1S3 & 2651 & 2651 & 2651 & 0 & 279.31 \\ T1S4 & 2651 & 2651 & 2651 & 0 & 8.94 \\ T1V2 & 2651 & 2651 & 2651 & 0 & 6.78 \\ T1V3 & 2651 & 2651 & 2651 & 0 & 3.92 \\ T1V4 & 2651 & 2651 & 2651 & 0 & 1.9 \\ T2S1 & 2651 & 2651 & 2651 & 0 & 15.34 \\ T2S2 & 2651 & 2651 & 2651 & 0 & 328.5 \\ T2S3 & 2651 & 2651 & 2651 & 0 & 223.96 \\ T2S4 & 2651 & 2651 & 2651 & 0 & 6.95 \\ T2V1 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V2 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V3 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 1.08 \\ \hline \\ k_{p-17} & k_{1} & 2917 & 2917 & 2917 & 0 & 81.88 \\ S3 & 2917 & 2917 & 2917 & 0 & 43.44 \\ S4 & 2917 & 2917 & 2917 & 0 & 43.44 \\ S4 & 2917 & 2917 & 2917 & 0 & 2.88 \\ V3 & 2917 & 2917 & 2917 & 0 & 2.88 \\ V3 & 2917 & 2917 & 2917 & 0 & 1.8 \\ T1S1 & 2917 & 2917 & 2917 & 0 & 1.8 \\ T1S1 & 2917 & 2917 & 2917 & 0 & 8.5 \\ T1S2 & 2917 & 2917 & 2917 & 0 & 8.5 \\ T1S2 & 2917 & 2917 & 2917 & 0 & 8.5 \\ T1S2 & 2917 & 2917 & 2917 & 0 & 8.5 \\ T1S2 & 2917 & 2917 & 2917 & 0 & 8.5 \\ T1S2 & 2917 & 2917 & 2917 & 0 & 8.5 \\ T1S2 & 2917 & 2917 & 2917 & 0 & 8.5 \\ T1S2 & 2917 & 2917 & 2917 & 0 & 8.5 \\ T1S2 & 2917 & 2917 & 2917 & 0 & 8.5 \\ T1S2 & 2917 & 2917 & 2917 & 0 & 50.73 \\ \hline \end{cases}$			T1S1	2651	2651	2651	0	20.82	
$kp-16 = \frac{T1S3}{T1S4} = \frac{2651}{2651} = \frac{2651}{2651} = \frac{2651}{2651} = \frac{0}{318} = \frac{279.31}{318} = \frac{1177}{1171} = \frac{2651}{2651} = \frac{2651}{2651} = \frac{2651}{2651} = \frac{0}{0} = \frac{318}{318} = \frac{1177}{1172} = \frac{2651}{2651} = \frac{2651}{2651} = \frac{2651}{0} = \frac{0}{0} = \frac{0}{392} = \frac{1177}{1174} = \frac{2651}{2651} = \frac{2651}{2651} = \frac{2651}{0} = \frac{0}{15.34} = \frac{128}{1282} = \frac{2651}{2651} = \frac{2651}{2651} = \frac{2651}{0} = \frac{0}{223.96} = \frac{128}{1284} = \frac{2651}{2651} = \frac{2651}{2651} = \frac{2651}{0} = \frac{0}{223.96} = \frac{128}{1284} = \frac{2651}{2651} = \frac{2651}{2651} = \frac{2651}{0} = \frac{0}{223.96} = \frac{128}{1284} = \frac{2651}{2651} = \frac{2651}{2651} = \frac{2651}{0} = \frac{0}{23.96} = \frac{128}{1284} = \frac{2651}{2651} = \frac{2651}{2651} = \frac{2651}{0} = \frac{0}{2.94} = \frac{127}{1274} = \frac{2651}{2651} = \frac{2651}{2651} = \frac{2651}{0} = \frac{0}{1.08} = \frac{128}{12917} = \frac{2917}{2917} = \frac{2917}{0} = \frac{0}{43.44} = \frac{128}{84} = \frac{2917}{2917} = \frac{2917}{2917} = \frac{2917}{0} = \frac{288}{13} = \frac{118}{2917} = \frac{2917}{2917} = \frac{2917}{0} = \frac{2.88}{13} = \frac{118}{2917} = \frac{2917}{2917} = \frac{2917}{0} = \frac{0}{1.8} = \frac{118}{1181} = \frac{2917}{2917} = \frac{2917}{0} = \frac{0}{1.8} = \frac{118}{1182} = \frac{2917}{2917} = \frac{2917}{2917} = \frac{0}{0} = \frac{50.73}{15} = \frac{118}{1182} = \frac{2917}{2917} = \frac{2917}{2917} = \frac{2917}{0} = \frac{0}{50.73} = \frac{118}{1182} = \frac{2917}{2917} = \frac{2917}{2917} = \frac{2917}{0} = \frac{50.73}{15} = \frac{118}{1182} = \frac{2917}{2917} = \frac{2917}{2917} = \frac{2917}{0} = \frac{50.73}{15} = \frac{118}{1182} = \frac{2917}{2917} = \frac{2917}{2917} = \frac{2917}{0} = \frac{50.73}{15} = \frac{118}{1182} = \frac{2917}{2917} = \frac{2917}{2917} = \frac{2917}{0} = \frac{50.73}{15} = \frac{118}{1182} = \frac{2917}{2917} = \frac{2917}{2917} = \frac{2917}{0} = \frac{50.73}{15} = \frac{118}{118} = \frac{2917}{2917} = \frac{2917}{2917} = \frac{2917}{0} = \frac{118}{118} = \frac{118}{1182} = \frac{2917}{2917} = \frac{2917}{2917} = \frac{2917}{0} = \frac{118}{118} = 11$			T1S2	2651	2651	2651	0	347.16	
$kp-16 = \begin{cases} T1S4 & 2651 & 2651 & 2651 & 0 & 318 \\ T1V1 & 2651 & 2651 & 2651 & 0 & 8.94 \\ T1V2 & 2651 & 2651 & 2651 & 0 & 6.78 \\ T1V3 & 2651 & 2651 & 2651 & 0 & 3.92 \\ T1V4 & 2651 & 2651 & 2651 & 0 & 1.9 \\ T2S1 & 2651 & 2651 & 2651 & 0 & 15.34 \\ T2S2 & 2651 & 2651 & 2651 & 0 & 328.5 \\ T2S3 & 2651 & 2651 & 2651 & 0 & 223.96 \\ T2S4 & 2651 & 2651 & 2651 & 0 & 6.95 \\ T2V1 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V2 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V3 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 4.52 \\ Rentric 1 & 2917 & 2917 & 0 & 6.08 \\ S1 & 2917 & 2917 & 2917 & 0 & 81.88 \\ S3 & 2917 & 2917 & 2917 & 0 & 43.44 \\ S4 & 2917 & 2917 & 2917 & 0 & 43.44 \\ S4 & 2917 & 2917 & 2917 & 0 & 3.52 \\ V2 & 2917 & 2917 & 2917 & 0 & 2.88 \\ V3 & 2917 & 2917 & 2917 & 0 & 1.8 \\ T1S1 & 2917 & 2917 & 2917 & 0 & 8.5 \\ T1S2 & 2917 & 2917 & 2917 & 0 & 8.5 \\ T1S2 & 2917 & 2917 & 2917 & 0 & 8.5 \\ T1S2 & 2917 & 2917 & 2917 & 0 & 8.5 \\ T1S2 & 2917 & 2917 & 2917 & 0 & 50.73 \\ \end{cases}$			T1S3	2651	2651	2651	0	279.31	
Kp-10 T1V1 2651 2651 2651 0 8.94 T1V2 2651 2651 2651 0 6.78 T1V3 2651 2651 2651 0 3.92 T1V4 2651 2651 2651 0 1.9 T2S1 2651 2651 2651 0 328.5 T2S2 2651 2651 2651 0 328.5 T2S3 2651 2651 2651 0 328.5 T2S4 2651 2651 2651 0 223.96 T2V1 2651 2651 2651 0 7.15 T2V2 2651 2651 2651 0 4.52 T2V3 2651 2651 2651 0 1.08 S1 2917 2917 2917 0 81.88 S3 2917 2917 2917 0 43.44 S4 2917 2917 0		kn 16	T1S4	2651	2651	2651	0	318	
$kp-17 \begin{array}{ c c c c c c c c c c c c c c c c c c c$		кр-10	T1V1	2651	2651	2651	0	8.94	
$k_{p-17} = \begin{bmatrix} T1V3 & 2651 & 2651 & 2651 & 0 & 3.92 \\ T1V4 & 2651 & 2651 & 2651 & 0 & 1.9 \\ T2S1 & 2651 & 2651 & 2651 & 0 & 328.5 \\ T2S2 & 2651 & 2651 & 2651 & 0 & 223.96 \\ T2S4 & 2651 & 2651 & 2651 & 0 & 6.95 \\ T2V1 & 2651 & 2651 & 2651 & 0 & 7.15 \\ T2V2 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V3 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 1.08 \\ S1 & 2917 & 2917 & 2917 & 0 & 6.08 \\ S2 & 2917 & 2917 & 2917 & 0 & 6.08 \\ S3 & 2917 & 2917 & 2917 & 0 & 43.44 \\ S4 & 2917 & 2917 & 2917 & 0 & 43.44 \\ S4 & 2917 & 2917 & 2917 & 0 & 3.52 \\ V2 & 2917 & 2917 & 2917 & 0 & 3.52 \\ V2 & 2917 & 2917 & 2917 & 0 & 2.88 \\ V3 & 2917 & 2917 & 2917 & 0 & 2.88 \\ V3 & 2917 & 2917 & 2917 & 0 & 1.8 \\ T1S1 & 2917 & 2917 & 2917 & 0 & 1.8 \\ T1S1 & 2917 & 2917 & 2917 & 0 & 8.5 \\ T1S2 & 2917 & 2917 & 2917 & 0 & 8.5 \\ T1S2 & 2917 & 2917 & 2917 & 0 & 50.73 \\ \end{bmatrix}$			T1V2	2651	2651	2651	0	6.78	
$kp-17 = \begin{cases} T1V4 & 2651 & 2651 & 2651 & 0 & 1.9 \\ T2S1 & 2651 & 2651 & 2651 & 0 & 15.34 \\ T2S2 & 2651 & 2651 & 2651 & 0 & 328.5 \\ T2S3 & 2651 & 2651 & 2651 & 0 & 223.96 \\ T2S4 & 2651 & 2651 & 2651 & 0 & 6.95 \\ T2V1 & 2651 & 2651 & 2651 & 0 & 7.15 \\ T2V2 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V3 & 2651 & 2651 & 2651 & 0 & 2.94 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 1.08 \\ S1 & 2917 & 2917 & 2917 & 0 & 6.08 \\ S2 & 2917 & 2917 & 2917 & 0 & 6.08 \\ S3 & 2917 & 2917 & 2917 & 0 & 43.44 \\ S4 & 2917 & 2917 & 2917 & 0 & 3.52 \\ V2 & 2917 & 2917 & 2917 & 0 & 3.52 \\ V3 & 2917 & 2917 & 2917 & 0 & 2.88 \\ V3 & 2917 & 2917 & 2917 & 0 & 2.88 \\ V3 & 2917 & 2917 & 2917 & 0 & 1.8 \\ T1S1 & 2917 & 2917 & 2917 & 0 & 1.8 \\ T1S1 & 2917 & 2917 & 2917 & 0 & 8.5 \\ T1S2 & 2917 & 2917 & 2917 & 0 & 8.5 \\ T1S2 & 2917 & 2917 & 2917 & 0 & 50.73 \\ \end{cases}$			T1V3	2651	2651	2651	0	3.92	
$kp-17 \begin{array}{c ccccccccccccccccccccccccccccccccccc$			T1V4	2651	2651	2651	0	1.9	
$kp-17 \begin{array}{c ccccccccccccccccccccccccccccccccccc$			T2S1	2651	2651	2651	0	15.34	
$kp-17 = \begin{cases} T2S3 & 2651 & 2651 & 2651 & 0 & 223.96 \\ T2S4 & 2651 & 2651 & 2651 & 0 & 6.95 \\ T2V1 & 2651 & 2651 & 2651 & 0 & 7.15 \\ T2V2 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V3 & 2651 & 2651 & 2651 & 0 & 1.08 \\ \hline T2V4 & 2651 & 2651 & 2651 & 0 & 1.08 \\ \hline S1 & 2917 & 2917 & 2917 & 0 & 6.08 \\ S2 & 2917 & 2917 & 2917 & 0 & 81.88 \\ \hline S3 & 2917 & 2917 & 2917 & 0 & 43.44 \\ \hline S4 & 2917 & 2917 & 2917 & 0 & 42.88 \\ \hline V1 & 2917 & 2917 & 2917 & 0 & 3.52 \\ \hline V2 & 2917 & 2917 & 2917 & 0 & 2.88 \\ \hline V3 & 2917 & 2917 & 2917 & 0 & 2.88 \\ \hline V3 & 2917 & 2917 & 2917 & 0 & 1.8 \\ \hline T1S1 & 2917 & 2917 & 2917 & 0 & 1.8 \\ \hline T1S2 & 2917 & 2917 & 2917 & 0 & 8.5 \\ \hline T1S2 & 2917 & 2917 & 2917 & 0 & 50.73 \\ \end{cases}$			T2S2	2651	2651	2651	0	328.5	
$kp-17 = \begin{cases} T2S4 & 2651 & 2651 & 2651 & 0 & 6.95 \\ T2V1 & 2651 & 2651 & 2651 & 0 & 7.15 \\ T2V2 & 2651 & 2651 & 2651 & 0 & 4.52 \\ T2V3 & 2651 & 2651 & 2651 & 0 & 2.94 \\ T2V4 & 2651 & 2651 & 2651 & 0 & 1.08 \\ \hline S1 & 2917 & 2917 & 2917 & 0 & 6.08 \\ S2 & 2917 & 2917 & 2917 & 0 & 81.88 \\ S3 & 2917 & 2917 & 2917 & 0 & 43.44 \\ S4 & 2917 & 2917 & 2917 & 0 & 43.44 \\ S4 & 2917 & 2917 & 2917 & 0 & 42.88 \\ \hline V1 & 2917 & 2917 & 2917 & 0 & 3.52 \\ \hline V2 & 2917 & 2917 & 2917 & 0 & 2.88 \\ \hline V3 & 2917 & 2917 & 2917 & 0 & 2.16 \\ \hline V4 & 2917 & 2917 & 2917 & 0 & 1.8 \\ \hline T1S1 & 2917 & 2917 & 2917 & 0 & 8.5 \\ \hline T1S2 & 2917 & 2917 & 2917 & 0 & 50.73 \\ \end{cases}$			T2S3	2651	2651	2651	0	223.96	
$\begin{tabular}{ c c c c c c c c c c c c c c c c c c c$			T2S4	2651	2651	2651	0	6.95	
$\frac{1}{1} \frac{1}{1} \frac{1}$			T2V1	2651	2651	2651	0	7.15	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			T2V2	2651	2651	2651	0	4.52	
$\frac{1}{1} + \frac{1}{1} + \frac{1}$			T2V3	2651	2651	2651	0	2.94	
	_		T2V4	2651	2651	2651	0	1.08	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			S 1	2917	2917	2917	0	6.08	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			S2	2917	2917	2917	0	81.88	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			S 3	2917	2917	2917	0	43.44	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			S4	2917	2917	2917	0	42.88	
kp-17 V2 2917 2917 2917 0 2.88 V3 2917 2917 2917 0 2.16 V4 2917 2917 2917 0 1.8 T1S1 2917 2917 2917 0 8.5 T1S2 2917 2917 2917 0 50.73		1	V1	2917	2917	2917	0	3.52	
V329172917291702.16V429172917291701.8T1S129172917291708.5T1S2291729172917050.73		кр-1 /	V2	2917	2917	2917	0	2.88	
V429172917291701.8T1S129172917291708.5T1S2291729172917050.73			V3	2917	2917	2917	0	2.16	
T1S129172917291708.5T1S2291729172917050.73			V4	2917	2917	2917	0	1.8	
T1S2 2917 2917 2917 0 50.73			T1S1	2917	2917	2917	0	8.5	
			T1S2	2917	2917	2917	0	50.73	

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	T1S3	2917	2917	2917	0	40.95	
	T1S4	2917	2917	2917	0	39.27	
	T1V1	2917	2917	2917	0	1.93	
	T1V2	2917	2917	2917	0	1.96	
	T1V3	2917	2917	2917	0	1.04	
	T1V4	2917	2917	2917	0	1	
	T2S1	2917	2917	2917	0	6 94	
	T2S2	2917	2917	2917	0	48 33	
	T252	2017	2917	2917	0	35.97	
	T2S3	2017	2917	2017	0	31.94	
	T2N1	2917	2917	2917	0	1 26	
		2917	2917	2917	0	1.20	
	12V2	2917	2917	2917	0	1.75	
	12V3	2917	2917	2917	0	1.23	
. <u></u>	12V4	2917	2917	2917	0	1	
	51	2818	2818	2818	0	24.28	
	52 53	2010	2817.1	2017	0.32	978.5	
	S4	2818	2817.1	2817	0.32	905.5	
	V1	2818	2818	2818	0.52	94.76	
	V2	2818	2818	2818	0	39.6	
	V3	2818	2818	2818	0	30.36	
	V4	2818	2818	2818	0	18.52	
	T1S1	2818	2818	2818	0	30.65	
	T1S2	2818	2818	2818	0	766.3	
	T1S3	2818	2818	2818	0	598.5	
kn-18	T1S4	2818	2818	2818	0	832.9	
кр 10	T1V1	2818	2818	2818	0	71.2	
	T1V2	2818	2818	2818	0	23.9	
	T1V3	2818	2818	2818	0	19.43	
		2818	2818	2818	0	8.69	
	1251 T282	2010	2818	2010	0	27.83	
	T2S2	2818	2818	2818	0	691.6	
	T2S3	2818	2818	2818	0	536.4	
	T2V1	2818	2818	2818	0	74.9	
	T2V2	2818	2818	2818	0	21.95	
	T2V3	2818	2818	2818	0	15.35	
	T2V4	2818	2818	2818	0	6.94	
	S 1	3223	3223	3223	0	95.68	
	S2	3223	3221.2	3221	0.632	985.5	
	S 3	3223	3221.2	3221	0.632	589.5	
	S 4	3223	3221.2	3221	0.632	765.3	
kp-19	V1	3223	3223	3223	0	13.1	
r -	V2	3223	3223	3223	0	9.43	
	V3	3223	3223	3223	0	7.93	
	V4	3223	3223	3223	Õ	4 1	
	T1C1	3223	3223	3223	0	120.6	

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Journal of Physics: Conference Series		1879 (2021) 022	2097 doi:10.	1088/1742-0	6596/1879/2/022097
T1S2	3223	3223	3223	0	645.35
T1S3	3223	3223	3223	0	428.6
T1S4	3223	3223	3223	0	594.82
T1V1	3223	3223	3223	0	9.72
T1V2	3223	3223	3223	0	9.18
T1V3	3223	3223	3223	0	4.38
T1V4	3223	3223	3223	0	2.14
T2S1	3223	3223	3223	0	89.5
T2S2	3223	3223	3223	0	583.8
T2S3	3223	3223	3223	0	357.91
T2S4	3223	3223	3223	0	455.91
T2V1	3223	3223	3223	0	8.16
T2V2	3223	3223	3223	0	6.28
T2V3	3223	3223	3223	0	6.13
T2V4	3223	3223	3223	0	1.91

Table S5: Comparison results of uncorrelated large size 0–1 KP

Instance	Dimension	Transfer function	Best	Mean	Worst	SD	Mean iterations
kp-21	100	S1	2060	2060	2060	0	142
I		S2	2060	2038.4	2023	19.756	350
		S 3	2060	2036.8	2023	17.387	353
		S 4	2060	2043	2023	18.886	351
		V1	2060	2060	2060	0	95
		V2	2060	2060	2060	0	88
		V3	2060	2060	2060	0	90
		V4	2060	2060	2060	0	76
		T1S1	2060	2060	2060	0	169
		T1S2	2060	2049	2045	6.519	153
		T1S3	2060	2049.8	2045	6.14	215
		T1S4	2060	2048.4	2045	7.092	201
		T1V1	2060	2060	2060	0	57
		T1V2	2060	2060	2060	0	45
		T1V3	2060	2060	2060	0	62
		T1V4	2060	2060	2060	0	39
		T2S1	2060	2060	2060	0	185
		T2S2	2060	2049.6	2048	6.542	162
		T2S3	2060	2049	2048	6.633	224
		T2S4	2060	2049.6	2048	5.941	240
		T2V1	2060	2060	2060	0	61
		T2V2	2060	2060	2060	0	42
		T2V3	2060	2060	2060	0	59
		T2V4	2060	2060	2060	0	34
		S 1	20348	20339.6	20334	7.668	2859
kn 23	1000	S2	20340	20327.2	20308	17.527	4781
кр-23	1000	S 3	20340	20329.4	20308	15.027	4618
		S 4	20340	20326.8	20308	17.181	4237

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		V1	20350	20347.6	20346	2.19	531
		V2	20350	20348	20346	2	498
		V3	20350	20348.4	20346	2.19	562
		V4	20350	20349.2	20346	1.789	415
		T1S1	20350	20344.8	20342	3.899	2094
		T1S2	20349	20338.8	20332	9.311	3586
		T1S3	20349	20339.4	20332	8.848	3428
		T1S4	20349	20338.8	20332	7.12	4057
		T1V1	20350	20348.8	20348	1.095	463
		T1V2	20350	20349.4	20348	0.894	401
		T1V3	20350	20348.8	20348	0.837	443
		T1V4	20350	20349.4	20348	0.894	381
		T2S1	20350	20346	20342	3.742	2099
		T2S2	20349	20342.2	20332	9.3	3308
		T2S3	20349	20343.6	20332	7.8	3258
		T2S4	20349	20340.2	20332	8.526	3974
		T2V1	20350	20349.2	20348	1.095	492
		T2V2	20350	20349.2	20348	0.837	391
		T2V3	20350	20349	20348	1	412
		T2V4	20350	20349.6	20348	0.894	328
		S 1	31255	31247.8	31241	6.686	4289
		S 2	31250	31224.2	31198	26.04	6722
		S 3	31250	31222	31198	23.63	5983
		S 4	31250	31224	31198	25.76	5347
		V1	31257	31249.8	31245	5.215	1025
		V2	31257	31250.8	31245	4.49	992
		V3	31257	31250.4	31245	4.67	1349
		V4	31257	31252.2	31245	4.38	903
		T1S1	31257	31254.6	31253	2.19	2951
		T1S2	31256	31237.6	31228	13.45	4228
		T1S3	31256	31235.4	31228	14.69	3984
1 24	1500	T1S4	31256	31236.4	31228	15.646	4129
кр-24	1500	T1V1	31257	31255.8	31255	1.095	751
		T1V2	31257	31256	31255	1	694
		T1V3	31257	31256.2	31255	0.837	789
		T1V4	31257	31256.4	31255	0.821	562
		T2S1	31257	31255	31253	2	2493
		T2S2	31256	31237.4	31228	12.605	4059
		T2S3	31256	31238.6	31228	12.954	4286
		T2S4	31256	31238.4	31228	11.06	4178
		T_2V_1	31257	31255.8	31255	0.837	842
		T2V2	31257	31256	31255	0.707	697
		T2V3	31257	31255.6	31255	0 894	981
		T2V4	31257	31256.4	31255	0.821	509
			01201	01-0000	0.00	0.021	

 Table S6: Comparison results of weakly correlated large size 0–1 KP

Instance	Dimension	Transfer function	Best	Mean	Worst	SD	Mean iterations
kp-26	100	<u>S</u> 1	1016	1016	1016	0	120

Ibn Al-Haitham International Conference for Pure and Applied Sciences (IHICPS) IO							IOP Publishing	
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,			(,				
			60	1016	007.2	090	11 070	225
			52 52	1010	997.2	989	11.278	325
			53	1016	994.2	989	9.952	298
			S4	1016	998	989	10.677	337
			VI	1016	1016	1016	0	86
			V2	1016	1016	1016	0	79
			V3	1016	1016	1016	0	83
			V4	1016	1016	1016	0	62
			T1S1	1016	1016	1016	0	157
			T1S2	1016	1004	999	7.661	129
			T1S3	1016	1007	999	6.166	194
			T1S4	1016	1009.4	999	7.057	173
			T1V1	1016	1016	1016	0	65
			T1V2	1016	1016	1016	0	49
			T1V3	1016	1016	1016	0	64
			T1V4	1016	1016	1016	0	30
			T2S1	1016	1016	1016	0	160
			T2S2	1016	1009.6	1008	3.578	122
			T2S3	1016	1012	1008	4	188
			T2S4	1016	1011.2	1008	3.347	169
			T2V1	1016	1016	1016	0	64
			T2V2	1016	1016	1016	0	39
			T2V3	1016	1016	1016	0	61
			T2V4	1016	1016	1016	0	31
			S 1	10352	10345.4	10340	9.631	2156
			S 2	10351	10348.2	10338	13.964	3924
			S 3	10351	10347.8	10338	14.57	3615
			S 4	10351	10348	10338	13.238	4025
			V1	10356	10353.6	10350	5.613	492
			V2	10356	10354	10350	4.679	385
			V3	10356	10353.8	10350	5.348	477
			V4	10356	10354.4	10350	4 069	336
			T1S1	10357	10354.2	10352	2.15	2294
			T1S1 T1S2	10357	10352.1	10344	7 281	2960
			T152	10357	10351.6	10344	6 8 2 3	2/00
			T155	10357	10351.0	10344	6.134	3512
	kp-28	1000	1134 T1V1	10357	10351.4	10344	0.134	JJ12 419
			11V1 T1V2	10257	10333.1	10354	2.50	410
			11V2	10357	10356	10354	1.068	304
			T1V3	10357	10355.4	10354	2.06	393
			11V4	10357	10356.2	10354	0.985	300
			T2S1	10357	10354	10352	2.01	2341
			T2S2	10357	10351.8	10344	7.328	3001
			T2S3	10357	10351.2	10344	7.054	2923
			T2S4	10357	10532	10344	6.832	3194
			T2V1	10357	10355.4	10354	2.456	407
			T2V2	10357	10356.1	10354	1.37	318
			T2V3	10357	10356	10354	1.254	371
			T2V4	10357	10356.2	10354	0.895	303
			S 1	15446	15441.6	15432	7.627	4091
	kp-29	1500	S2	15400	15383.4	15365	21.975	5906
	_		S 3	15400	15384	15365	19.713	5213

Ibn Al-Haitham International Conference for	IOP Publishing				
Journal of Physics: Conference Series	1879 (2	2021) 022097	doi:10.1088/1742-659		96/1879/2/022097
S4	15400	15383.6	15365	20.668	5194
V1	15496	15486	15454	10.634	1395
V2	15496	15486.4	15454	9.248	1082
V3	15496	15486.2	15454	11.573	1267
V4	15496	15486.8	15454	8.275	990
T1S1	15507	15491	15470	5.382	3924
T1S2	15507	15495.6	15460	13.627	4615
T1S3	15507	15494.8	15460	14.351	4208
T1S4	15507	15495	15460	12.01	4792
T1V1	15507	15502	15490	5.617	971
T1V2	15507	15503.2	15490	4.319	898
T1V3	15507	15502.6	15490	4.065	919
T1V4	15507	15503.2	15490	4.319	805
T2S1	15507	15491.6	15454	5.915	3902
T2S2	15507	15494.2	15460	12.951	4593
T2S3	15507	15494	15460	13.986	4321
T2S4	15507	15495.4	15460	13.035	4435
T2V1	15507	15502.6	15490	4.972	850
T2V2	15507	15503	15490	3.658	777
T2V3	15507	15502	15490	5.349	882
T2V4	15507	15503.4	15490	4.568	692

Table S7: Comparison results of strongly correlated large size 0–1 KP

Instance	Dimension	Transfer	Best	Mean	Worst	SD	Mean
mstance	Dimension	function		wiedh	worst	50	iterations
		S 1	1332	1332	1332	0	95
		S2	1332	1332	1332	0	184
		S 3	1332	1332	1332	0	176
		S 4	1332	1332	1332	0	190
		V1	1332	1332	1332	0	54
		V2	1332	1332	1332	0	31
		V3	1332	1332	1332	0	50
		V4	1332	1332	1332	0	29
		T1S1	1332	1332	1332	0	109
		T1S2	1332	1332	1332	0	123
		T1S3	1332	1332	1332	0	125
lun 21	100	T1S4	1332	1332	1332	0	120
кр-31		T1V1	1332	1332	1332	0	40
		T1V2	1332	1332	1332	0	25
		T1V3	1332	1332	1332	0	33
		T1V4	1332	1332	1332	0	19
		T2S1	1332	1332	1332	0	137
		T2S2	1332	1332	1332	0	114
		T2S3	1332	1332	1332	0	122
		T2S4	1332	1332	1332	0	108
		T2V1	1332	1332	1332	0	47
		T2V2	1332	1332	1332	0	27
		T2V3	1332	1332	1332	0	30
		T2V4	1332	1332	1332	0	25
kp-33	1000	S 1	13410	13405.2	13395	7.391	1945

Ibn Al-Haitham International Conference for Pure and Applied Scienc						s (IHICPS) IOP Publishing			
Journal of Physics: Conference Series			1879 (2	2021) 022097	doi:10.1088/1742-6596/1879/2/022097				
			\$2	13390	13386	13370	18 62	3026	
			S2 S3	13390	13385.9	13370	19.28	2915	
			S4	13390	13386.4	13370	17.54	3108	
			V1	13448	13441	13436	12.68	1154	
			V2	13448	13442	13436	10.25	1093	
			V3	13448	13441.6	13436	11.39	1251	
			V4	13448	13442.4	13436	10.09	1001	
			T1S1	13454	13449	13440	9.52	2397	
			T1S2	13454	13448.5	13440	10.27	2108	
			T1S3	13454	13448	13440	9.35	2293	
			T1S4	13454	13447.2	13440	11.24	2604	
			T1V1	13454	13454	13454	0	938	
			T1V2	13454	13454	13454	0	756	
			T1V3	13454	13454	13454	0	849	
			T1V4	13454	13454	13454	0	720	
			T2S1	13454	13447	13440	10.14	2253	
			T2S2	13454	13448	13440	8.37	2204	
			T2S3	13454	13447.8	13440	9.63	2157	
			T2S4	13454	13448.2	13440	8.921	2384	
			T2V1	13454	13454	13454	0	961	
			T2V2	13454	13454	13454	0	770	
			T2V3	13454	13454	13454	0	902	
_			T2V4	13454	13454	13454	0	738	
			S 1	20295	20284	20252	10.692	3157	
			S2	20289	20277.2	20246	25.34	5089	
			S 3	20289	20276	20246	27.137	4975	
			S 4	20289	20276.8	20246	26.821	5013	
			V1	20310	20306	20302	9.38	1085	
			V2	20310	20306.8	20302	8.937	1020	
			V3	20310	20306.4	20302	9.036	1017	
			V4	20310	20307	20302	10.02	1003	
			T1S1	20314	20312	20300	6.35	3681	
			T1S2	20314	20310	20296	16.93	3054	
			T1S3	20314	20310.6	20296	18.37	3376	
	kn 31	1500	T1S4	20314	20311	20296	20.589	3128	
	кр-54	1500	T1V1	20314	20314	20314	0	984	
			T1V2	20314	20314	20314	0	793	
			T1V3	20314	20314	20314	0	980	
			T1V4	20314	20314	20314	0	751	
			T2S1	20314	20312.6	20300	5.83	3507	
			T2S2	20314	20311	20296	19.34	3182	
			T2S3	20314	20310.6	20296	15.61	3259	
			T2S4	20314	20310.4	20296	13.29	3204	
			T2V1	20314	20314	20314	0	901	
			T2V2	20314	20314	20314	0	800	
			T2V3	20314	20314	20314	0	826	
_			T2V4	20314	20314	20314	0	748	

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