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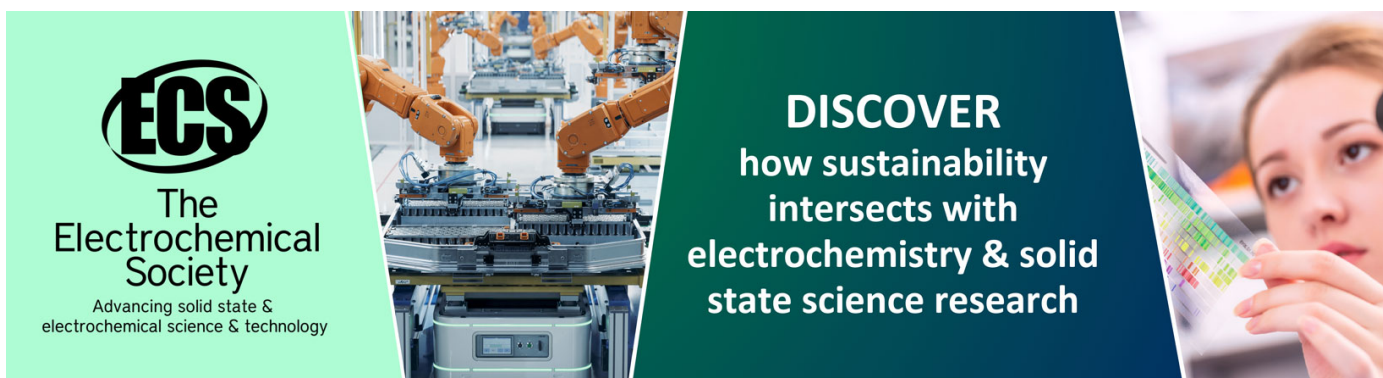
From wide to ultrawide-bandgap semiconductors for high power and high frequency electronic devices

To cite this article: Kelly Woo *et al* 2024 *J. Phys. Mater.* **7** 022003

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RECEIVED
19 May 2023REVISED
7 November 2023ACCEPTED FOR PUBLICATION
8 January 2024PUBLISHED
8 March 2024

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From wide to ultrawide-bandgap semiconductors for high power and high frequency electronic devices

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Keywords: ultrawide-bandgap, power electronics, radio-frequency devices, gallium nitride, aluminum nitride, diamond, gallium oxide

Abstract

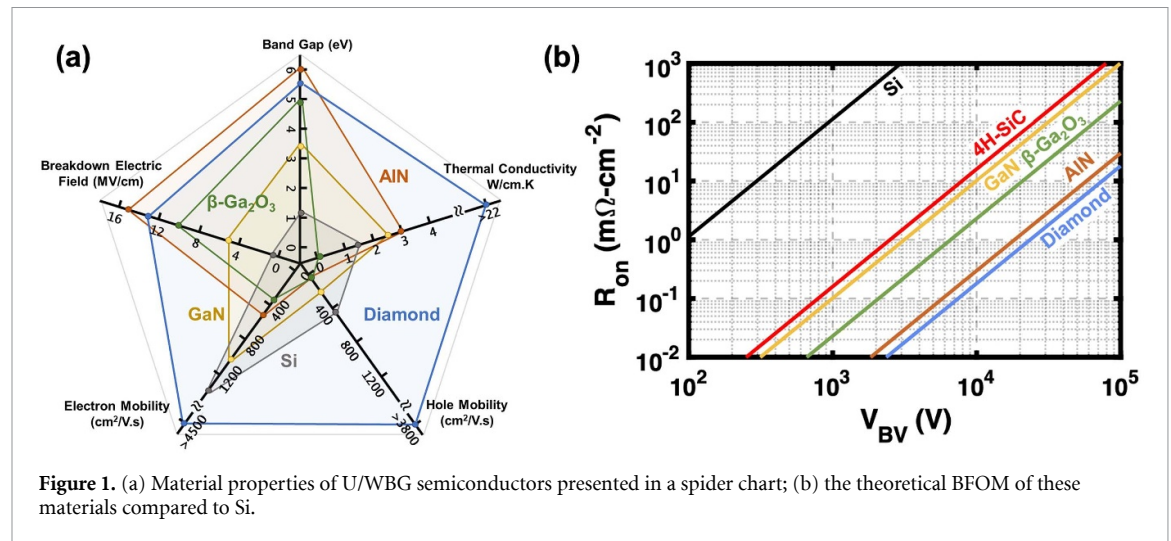
Wide and ultrawide-bandgap (U/WBG) materials have garnered significant attention within the semiconductor device community due to their potential to enhance device performance through their substantial bandgap properties. These exceptional material characteristics can enable more robust and efficient devices, particularly in scenarios involving high power, high frequency, and extreme environmental conditions. Despite the promising outlook, the physics of UWBG materials remains inadequately understood, leading to a notable gap between theoretical predictions and experimental device behavior. To address this knowledge gap and pinpoint areas where further research can have the most significant impact, this review provides an overview of the progress and limitations in U/WBG materials. The review commences by discussing Gallium Nitride, a more mature WBG material that serves as a foundation for establishing fundamental concepts and addressing associated challenges. Subsequently, the focus shifts to the examination of various UWBG materials, including AlGaN/AlN, Diamond, and Ga₂O₃. For each of these materials, the review delves into their unique properties, growth methods, and current state-of-the-art devices, with a primary emphasis on their applications in power and radio-frequency electronics.

1. Introduction

Wide bandgap (WBG) materials, such as Silicon Carbide (SiC) and Gallium Nitride (GaN), have unequivocally demonstrated their versatility across various fields, including optics, power electronics, and radio frequency (RF) technology. This has led to a significant expansion of their applications and a burgeoning market presence. What sets them apart is their exceptional ability to operate effectively in high-temperature and challenging environments. The progress in WBG materials is now driving substantial interest in an emerging class of semiconductors known as ultrawide-bandgap (UWBG) materials, distinguished by even wider bandgaps. Both WBG and UWBG materials exhibit remarkable resistance to electric field breakdown due to their large bandgap, offering a multitude of advantages to electronic devices and systems. These benefits encompass enhanced efficiency, the capability for high-temperature operation, smaller footprints, simplified system designs, and reduced overall system costs. Ultimately, broader positive impacts such as diminished carbon emissions and closure of the digital divide can result from the successful development of these technologies. In terms of specific device applications, today GaN has asserted its dominance in lighting technology, with noteworthy contributions in radar and telecommunication as well. Additionally, GaN has made significant inroads into power electronics. SiC, on the other hand, has excelled in medium to high-power electronics and serves as an excellent substrate for GaN RF technology. Consequently, there exists both a symbiotic and competitive relationship between SiC and GaN, shaping the current landscape of applications and markets. Their collective successes have firmly established WBG materials on the technological map, paving the way for the exploration of UWBG materials.

Table 1. Material properties of GaN and emerging UWBG semiconductors and their Baliga and Johnson figure of merits [3, 4] (references therein).

Material Parameters	GaN	β -Ga ₂ O ₃	Diamond	AlN
Bandgap E_g (eV)	3.4	4.8	5.5	6.0
Critical Field E_{cr} (MV cm ⁻¹)	3–3.5	8–10.3	10–13	15.4
Electron mobility μ_e (cm ² V ⁻¹ s ⁻¹)	1000	180	4500	426
Hole mobility μ_h (cm ² V ⁻¹ s ⁻¹)	24	—	3800	—
Relative permittivity ϵ_r	10.4	10	5.7	9.76
Electron saturation velocity v_{sat} (10 ⁷ cm s ⁻¹)	1.5–2.0	1.1	2.3	1.3
Thermal conductivity K (W m ⁻¹ K ⁻¹)	253	11–27	2290–3450	285–319
Baliga FOM (10 ⁶ V ² Ω ⁻¹ cm ⁻²)	27 900	36 300	554 000	336 000
Johnson FOM (10 ¹² V s ⁻¹)	11	18	29–47	31.9



The significance of semiconductor technology and its sustainability are frequently assessed through its market size. In the power semiconductor sector, the projected global market for Silicon Carbide is \$6 billion, and for Gallium Nitride \$2 billion by the year 2027 [1]. This substantial growth can be predominantly attributed to the expansion of hybrid and electric vehicles and several other key sectors, including, power supplies, military/aerospace applications, as well as renewable energy and smart grids. In the GaN RF market, an annual revenue of \$1.8 billion in 2022 is predicted to increase to \$2.7 billion by 2028 [2]. This significant commercial revenue stems from the utilization of high electron mobility transistors (HEMTs) for power amplifiers in wireless base stations. Furthermore, the increased efficiency and reliability offered by RF-oriented GaN find valuable applications in radar systems within the defense sector.

UWBG materials, like AlGaIn/AlN, diamond, and β -Ga₂O₃, have similar applications to those of WBG materials; however, with significantly larger bandgaps than 3 eV, they promise to offer even higher performance metrics. The electronic properties of GaN and UWBG materials are listed in table 1 and illustrated in figure 1. A simple method to quantify a device's suitability for power applications (specifically low frequency unipolar power switching) is by the Baliga figure of merit (BFOM): $V_{br}^2/R_{on,sp}$ or $\frac{1}{4}\epsilon\mu E_{cr}^3$, where V_{br} is the breakdown voltage, $R_{on,sp}$ is the specific on-resistance, ϵ is the dielectric constant, μ is the carrier mobility, and E_{cr} is the critical electric field. A higher value indicates that a device can sustain high blocking voltages while incurring minimal on-state losses, which can be visualized in figure 1(b). Thus, the critical electric field, which typically scales with the bandgap has a large influence on the BFOM. For high frequency power applications, the Johnson figure of merit (JFOM) is used: $v_{sat}E_{cr}/2\pi$, where v_{sat} is the saturation velocity. According to both FOMs, UWBG materials provide significant improvement in comparison to GaN which itself greatly surpasses Si in high power and frequency device performance.

In this comprehensive review article, our primary focus is on the exploration of electronic device technology led by GaN as a well-established technology, along with emerging technologies such as AlGaIn/AlN, Diamond, and β -Ga₂O₃. Our discussion will revolve around various aspects of these materials of interest, including their material properties, growth techniques, devices, and applications, providing an ample overview of their significance in the field of electronic device technology. While we recognize the significance of Silicon Carbide, it is not included in this article, and we would like to direct interested readers to some outstanding recent reviews on this subject [5, 6].

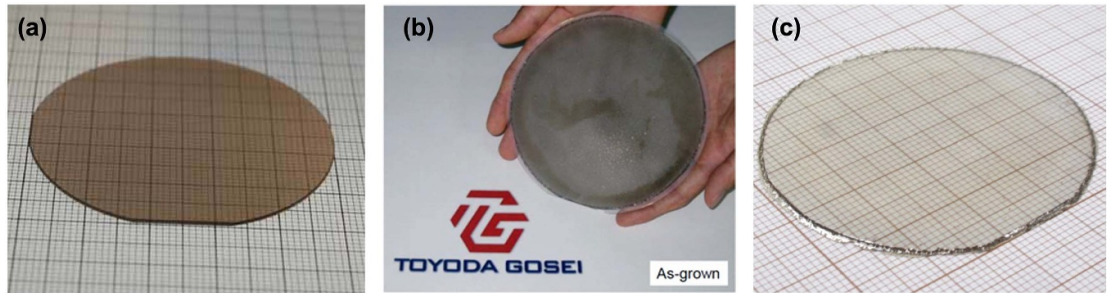


Figure 2. (a) Image of 2 inch. c-plane ammonothermal-GaN substrate (manufactured at AMMONO company) [20]; (b) 6 inch GaN crystal grown on MOCVD-GaN seeds using Na-flux method [21]; (c) 2 inch HVPE-GaN wafer with a thickness of $500\ \mu\text{m}$ and an etch pit density of $5 \times 10^4\ \text{cm}^{-2}$ [22].

2. Gallium nitride (GaN)

2.1. Material properties

The electron mobility in bulk GaN at room temperature is dependent on the doping, where it can reach $1000\ \text{cm}^2\ (\text{V}\cdot\text{s})^{-1}$ at low doping concentrations of $10^{15}\text{--}10^{16}\ \text{cm}^{-3}$ and decreases to $200\text{--}600\ \text{cm}^2\ (\text{V}\cdot\text{s})^{-1}$ in the doping range of $10^{17}\text{--}10^{18}\ \text{cm}^{-3}$. The hole mobility is much lower, typically less than $100\ \text{cm}^2\ (\text{V}\cdot\text{s})^{-1}$, and drops to around $10\text{--}30\ \text{cm}^2\ (\text{V}\cdot\text{s})^{-1}$ in the doping range of $10^{17}\text{--}10^{18}\ \text{cm}^{-3}$. A detailed mobility model for GaN describing the doping and temperature dependence is well documented [7]. On the other hand, the electron mobility in the two-dimensional electron gas (2DEG) formed at the AlGaIn/GaN interface can reach up to $2000\ \text{cm}^2\ (\text{V}\cdot\text{s})^{-1}$ at room temperature [8], motivating the development of GaN-based HEMTs. For high-field transport, the highest electron saturation velocity in GaN was reported to be $2\text{--}2.5 \times 10^7\ \text{cm s}^{-1}$ [9, 10], while the hole saturation velocity was limited to $0.7 \times 10^7\ \text{cm s}^{-1}$ [11, 12].

The intrinsic breakdown in a material is caused by avalanche initiated by the impact ionization at high electric fields. A critical field of $3\text{--}3.5\ \text{MV cm}^{-1}$ is estimated for GaN by the empirical formula in terms of its 3.4 eV bandgap [4]. In recent years, avalanche has been routinely achieved in GaN PN structures with proper doping profiles and efficient field management designs due to the availability of higher-quality native GaN substrates. Several photo-multiplication-based methods have been utilized in experiments to extract the impact ionization coefficients for electrons and holes in GaN [13–15]. Based on these coefficients, a physics-based model describing the critical field regarding doping concentration in GaN has been proposed [16].

For high power and frequency devices, the thermal properties of the materials become increasingly important as self-heating becomes a larger issue. The thermal conductivity (TC) of a material dictates how efficiently it can dissipate heat. For GaN, the TC is moderately high, around $170\text{--}220\ \text{W (m}\cdot\text{K)}^{-1}$ [17, 18], and was reported to be sensitive to the doping concentration and dislocation density.

2.2. Growth and doping

2.2.1. Bulk substrate growth

The past few decades have witnessed the rapid development of GaN-based electronic devices from experimental prototypes to successful commercialization. The scalability and quality of native GaN substrates play a critical role in reducing the manufacturing costs of GaN to further boost its commercial appeal, however, they still require more research efforts within the nitride community. The decomposition pressure at the melting point for GaN is around 6 GPa [19], leading to intrinsic difficulties in adopting the traditional melt growth method for bulk GaN substrates. Numerous research efforts in developing new crystal growth technology for GaN have been made, mainly consisting of three growth methods: ammonothermal growth, sodium-flux (Na-flux) growth, and hydride vapor phase epitaxy (HVPE). Figure 2 shows the images of the bulk GaN substrates grown by each of these methods.

The ammonothermal method begins by solubilizing polycrystalline (PC) GaN feedstock in supercritical ammonia under high pressure ($100\text{--}500\ \text{MPa}$) [23, 24]. Then, the dissolved materials are transported to the recrystallization region along a temperature gradient and growth on the seeding crystals occurs at temperatures of $500\ ^\circ\text{C}\text{--}600\ ^\circ\text{C}$ [23, 25, 26]. 2 inch GaN bulk substrates with a dislocation density down to $5 \times 10^3\ \text{cm}^{-2}$ were successfully demonstrated with the ammonothermal growth method [20]. The method's primary limitation is its relatively slow growth rate of around a few micrometers per hour.

Na-flux growth also belongs to the category of solution growth approaches but produces a more favorable growth condition by using sodium flux. The typical temperature and pressure during growth are

around 750 °C–900 °C and 5 MPa [27–30], respectively. Today, this method can produce a 6 inch crystallographically flat GaN wafer with high structural quality [31], and the typical dislocation density of the Na-flux method is around 10^4 – 10^6 cm⁻² [32].

Finally, the knowledge of HVPE growth of GaN was appropriated from the growth of GaAs and InP. In this method, chloride gas reacts with a gallium source and forms a gaseous phase in the source zone (800 °C–900 °C). The product is then transported to the nitrogen source in the deposition zone (1000 °C–1100 °C) for further reaction and crystallized as GaN [22, 33]. The most significant advantages of HVPE growth include the atmospheric pressure condition and a high growth rate on the order of several hundreds of micrometers per hour [34]. However, the size and thickness of the wafer are limited by the bowing of the crystallographic planes due to the lattice mismatch between GaN and the seeding materials.

2.2.2. Epitaxial layer growth

Several epitaxial growth methods have been developed for GaN thin-film growth on either native or nonnative substrates, including HVPE [35–38], molecular beam epitaxy (MBE) [39–42], and metalorganic chemical vapor deposition (MOCVD) [43–45]. When growing on nonnative substrates, a low-temperature AlN buffer layer is usually adopted to improve the surface morphology and increase the crystal quality by mitigating the lattice mismatch between GaN and foreign substrates [46]. Homoepitaxial growth on native GaN substrates does not require such a buffer layer. MBE growth provides precise control of the impurity and thickness of the film during the growth; however, it usually requires a high-vacuum atmosphere. MOCVD is considered to be the leading technique for the growth of III–V-nitride materials for mass production [47]. The use of high-purity chemical sources, characteristic of this method, yields a high degree of composition control and uniformity, high growth rates, and large-scale manufacturing potential.

2.2.3. Doping

Si is the most commonly used dopant element for donors in GaN by substituting the Ga sites [48]. The Si doping concentration can be well controlled by adjusting the flow rate of the gaseous source, for example, SiH₄ or Si₂H₆, over the range from 10^{16} to 10^{19} cm⁻³ without forming cracks and surface pits during growth [49, 50]. It was demonstrated that Si offered shallow donor states (around 10–20 meV) in GaN [51, 52], giving rise to a nearly complete ionization ratio at room temperatures. Furthermore, nitrogen vacancies in GaN can also provide unintentional n-type doping in GaN [53, 54].

P-type doping in GaN was also successfully achieved by using Mg as acceptors, which led to the invention of the blue LED utilizing a GaN PN junction. However, Mg-doped GaN tends to be electrically insulating if grown in the presence of hydrogen. The role of H atoms in passivating the Mg acceptors in GaN was elucidated as the H atoms were found to form neutral Mg–H complexes [55, 56]. The Mg–H bonds can be broken by low-energy electron beam irradiation or a high temperature thermal anneal above 700 °C [55, 57], which gives free holes in GaN. Due to the relatively high activation energy of Mg (130–180 meV reported) in GaN [58–60], the ionization ratio of Mg acceptors is typically less than 10%. Achieving a high hole concentration and high p-type conductivity with Mg remains critical for the GaN community.

Given the material properties and growth techniques summarized in the previous sections, we will discuss a few fundamental device structures and their applications to elucidate the importance of GaN in power and radio-frequency electronics.

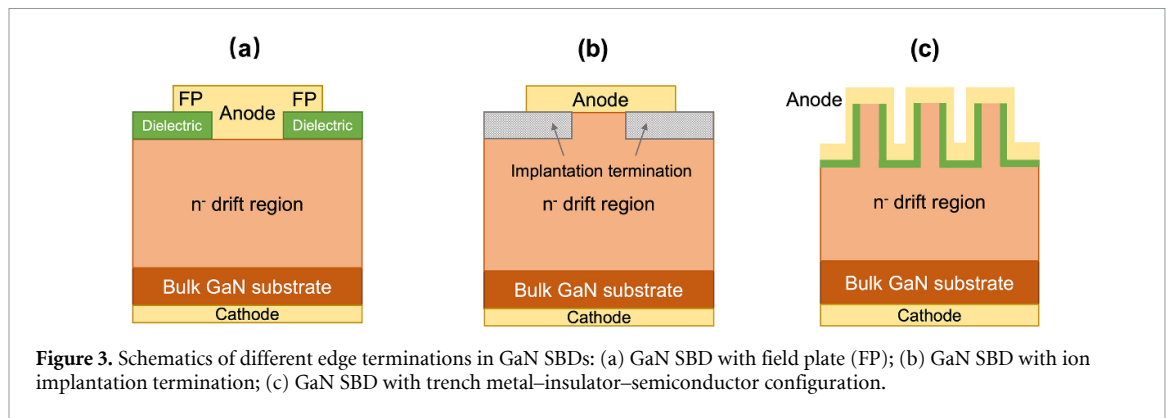
2.3. GaN devices and applications

2.3.1. High power devices

2.3.1.1. Schottky barrier diodes (SBDs)

The SBD is one of the basic rectifiers used in power electronics. Due to its majority carrier transport mechanism, it has the advantage of low turn-on voltage, fast switching, and thus low switching losses. However, the thermionic field emission transport at the metal–semiconductor interface leads to a rapid increase of leakage current at high surface electric fields, limiting the breakdown performance of GaN SBDs. Thus, from a device engineering perspective, efficient edge termination designs are needed to relax the field concentration at the anode edge to improve the breakdown.

Almost all reported GaN SBDs are based on an n-type drift region due to the excellent controllability of n-type GaN growth. Nickle (Ni) is one of the most commonly used contact metals for GaN. GaN SBDs can be simply fabricated by depositing a Schottky contact after the epitaxial growth of the drift region. In this configuration, the field concentration at the anode edge leads to a premature breakdown. The field plate structure (figure 3(a)) is an effective method to mitigate the peak electric field at the edge of the anode, thus enhancing the breakdown voltage [61, 62]. A GaN SBD over 1 kV was reported in 2010 by using a field plate on SiN_x layers for edge termination. Furthermore, growth optimization yielded a structure with a high bulk electron mobility of 930 cm² (V·s)⁻¹, which contributed to a low specific on-resistance of 0.71 mΩ·cm² [61].



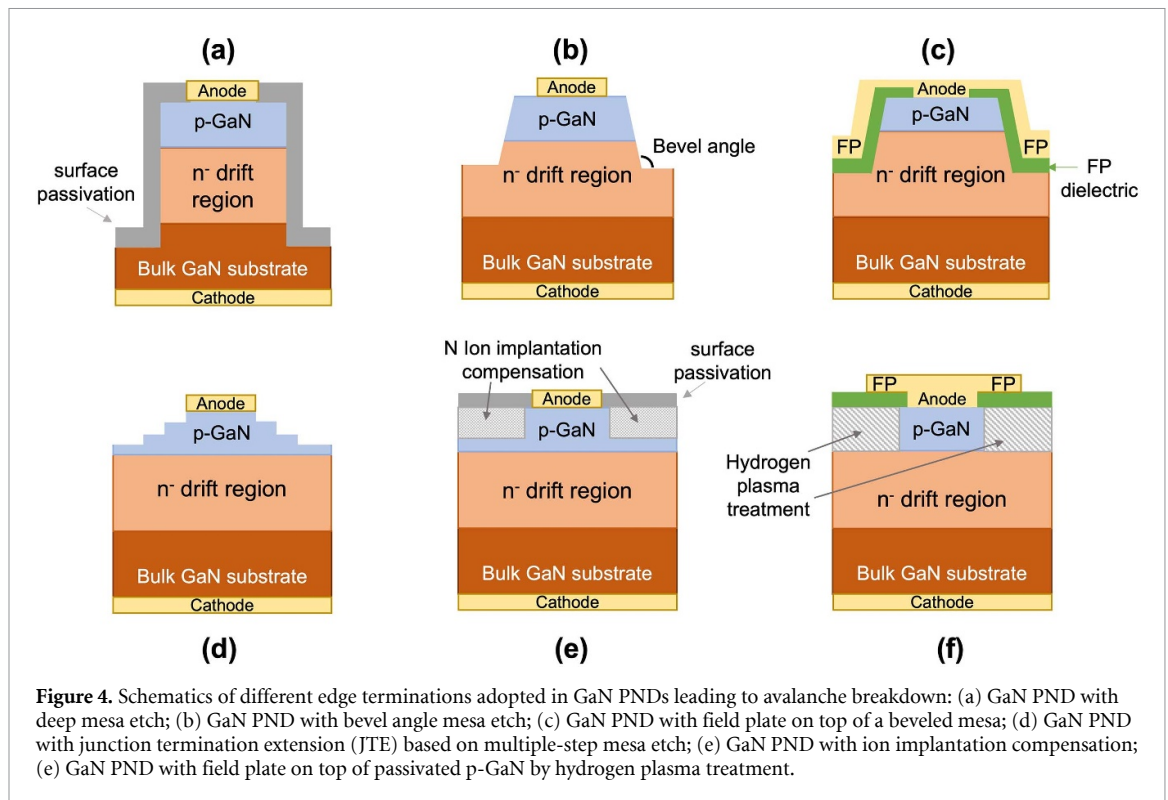
As shown in figure 3(b), the implantation of several species, such as Argon (Ar) and Fluorine (F), was reported to successfully convert n-type GaN to a highly-resistive region [63–66]. This high-resistivity region helps spread the potential along the surface, resulting in a mitigated electric field at the edge and reduced leakage current. Utilizing this technique, a 1.7 kV GaN SBD with Ar implantation termination has been achieved [64], and F implantation also showed a boost of breakdown voltage from 155 V to 775 V in GaN SBDs [67]. Similarly, plasma nitridation can increase the energy barrier height at the edge by compensating the nitrogen vacancies [68], offering a superior breakdown voltage of 995 V compared to 335 V without nitridation termination [69].

Trench metal–insulator–semiconductor barrier Schottky diodes (TMBS) have been proposed to effectively modulate the surface electric field at the Schottky contact to achieve a more uniform field distribution [70–72]. A representative TMBS structure is shown in figure 3(c). However, the peak field at the trench corner may also lead to field crowding and premature failure in the dielectrics. Thus, Zhang *et al* reported a novel TMBS structure with Ar implantation beneath the trench oxide, which mitigated this issue [73]. This method effectively enhanced the breakdown voltage from 500 V to 700 V after implantation treatment without degrading the forward characteristics.

2.3.1.2. PN junction diodes (PNDs)

GaN PNDs show lower leakage current and better thermal stability compared to GaN SBD diodes, despite their relatively high turn-on voltage. In contrast to SBDs, the peak electric field in PNDs appears near the junction instead of at the metal contacts as in GaN SBDs. Thus, the peak electric field can be buried inside the bulk, which prevents premature breakdown and improves the feasibility of achieving avalanche in vertical GaN PN diodes. Thanks to the increasing availability of native bulk GaN substrates with low dislocation density, the avalanche phenomenon has been more routinely reported in GaN PN structures. While avalanche is recognized as a performance benchmark in power devices, the off-state leakage current is another important metric in determining the power loss. The relationship between dislocation density and leakage current under the prerequisite of avalanche has been experimentally examined [74]. It was suggested that Poole–Frenkel effects dominated when the dislocation density was in the range of 10^4 cm^{-2} and variable-range-hopping mechanisms dominated when a higher dislocation density (10^6 cm^{-2}) was present in the device.

In GaN PND fabrication, mesa etches are the most versatile edge termination method used. Several edge terminations based on mesa etch are shown in figures 4(a)–(d). The deep mesa etch of the entire drift region creates a uniform electric field distribution, almost the same as in a 1D ideal planar structure [75]. Combined with a sidewall passivation layer, a deep mesa-etched diode was able to produce an 880 V avalanche in a GaN PN diode. A small-angle bevel mesa was also reported to effectively modulate the electric field near the PN junction [76, 77]. However, the bevel design is very sensitive to the ratio of the doping concentration and the bevel degree [78]. Field plating on a beveled mesa further mitigates the peak electric field near the junction, showing great potential in high-voltage kV-class GaN PND with avalanche capability [79, 80]. A 3.48 kV breakdown voltage and low specific on-resistance of $0.95 \text{ m}\Omega\cdot\text{cm}^2$ have been achieved using field plating in a GaN PN structure [80]. Recently, a junction termination extension (JTE) based on multiple-step mesa etched was successfully demonstrated in vertical GaN PN diode, resulting in an avalanche breakdown voltage of over 6 kV in GaN [81, 82]. Mg implantation into the sidewall after a mesa etch demonstrated a 1.5 kV avalanche in vertical GaN PNDs [83] without the need for an anneal to activate Mg. Instead, the implanted positive species create a depletion layer underneath the sidewall, shielding the high electric field at the surface, thus reducing the surface leakage.



Nitrogen ion implantation compensation offers a planar edge termination without the requirement of a mesa etch (figure 4(e)). The partially compensated p-GaN layer helps to laterally distribute the electric field to support a high voltage [84, 85]. A SiN_x surface passivation layer is required to suppress the surface leakage. Contrary to the activation process of an Mg-doped p-GaN layer, hydrogen plasma treatment was demonstrated to passivate the Mg in p-GaN again by forming neutral Mg–H complexes, creating a high-resistivity layer [86–88]. Hydrogen plasma based guard ring structures showed a vertical GaN PND with 1.7 kV breakdown and $0.65 \text{ m}\Omega\cdot\text{cm}^2$ specific on-resistance [89]. Adding a field plate on the passivated p-type layer helped reduce the electric field around the corner of the junction (figure 4(f)), resulting in a 2.8 kV avalanche breakdown device, justifying the application of hydrogen plasma treatment in fabricating high-voltage GaN PNDs [90].

2.3.1.3. Junction barrier diodes and superjunctions

Junction barrier diodes (JBS) incorporate the merit of low turn-on voltage and reduced leakage current from an SBD and PND design. GaN JBS diodes fabricated by Mg ion implantation followed by a multi-cycle rapid thermal annealing (RTA) method exhibited a $>600 \text{ V}$ breakdown voltage but a very large specific on-resistance $>100 \text{ m}\Omega\cdot\text{cm}^2$ [91]. Later, multiple pulsed thermal annealing at 1350°C was reported to partially recover the implantation damage and activate the implanted Mg, leading to an improved specific on-resistance of $1.7 \text{ m}\Omega\cdot\text{cm}^2$ with a 600 V breakdown [92]. Matys *et al* obtained the high activation ratio of implanted Mg by implementing the thermal annealing under ultra-high pressure at 500 MPa , leading to a high-quality p-type JTE structure, offering a nondestructive breakdown voltage of 675 V with a low on-resistance of $0.67 \text{ m}\Omega\cdot\text{cm}^2$ [93]. Recently, Zhou *et al* also demonstrated the avalanche capability in Mg-implanted GaN JBS [94].

A superjunction structure (SJ) theoretically gives rise to a better trade-off relationship between breakdown voltage and the specific on-resistance since the charge balancing does not require lowering the doping concentration in the drift region to achieve a high-voltage blocking. However, due to the difficulties in achieving a deep column of p-type GaN, vertical SJs in GaN are rarely reported. Xiao *et al* demonstrated a heterogeneous GaN SJ by using p-type NiO as a p-type column filling [95]. The schematics of the fabricated device and SEM cross-section images are shown in figures 5(a) and (b). The forward characteristics of the device exhibited two stages of turn-on behavior, corresponding to NiO/GaN and GaN PN junction, respectively. The fabricated SJ offered a 1.1 kV breakdown voltage with an on-resistance of $0.15 \text{ m}\Omega\cdot\text{cm}^2$, exceeding the unipolar GaN limit. The leakage current was attributed to the sidewall interface of GaN/NiO and avalanche was not observed. With the development of Mg ion implantation technology in GaN, increasing reports of homogeneous GaN SJs can be expected.

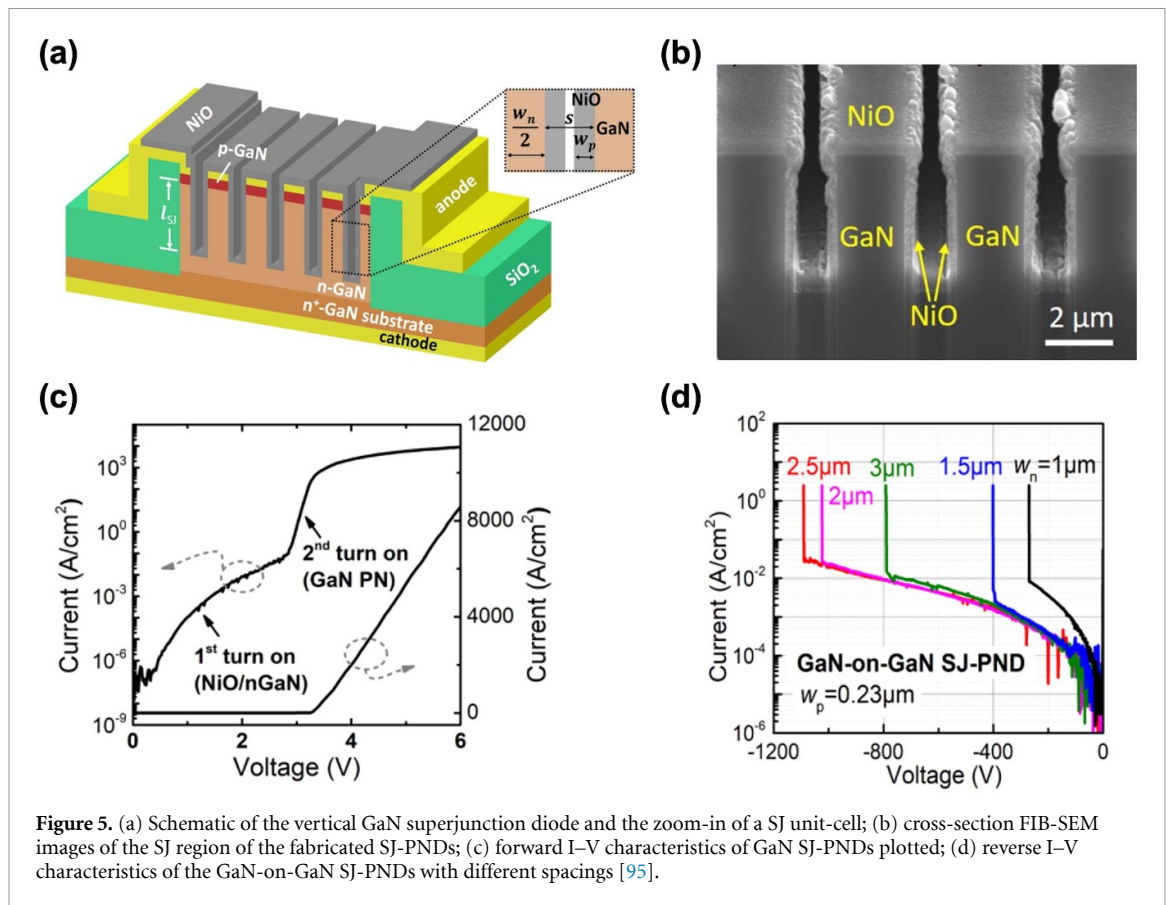


Figure 5. (a) Schematic of the vertical GaN superjunction diode and the zoom-in of a SJ unit-cell; (b) cross-section FIB-SEM images of the SJ region of the fabricated SJ-PNDs; (c) forward I–V characteristics of GaN SJ-PNDs plotted; (d) reverse I–V characteristics of the GaN-on-GaN SJ-PNDs with different spacings [95].

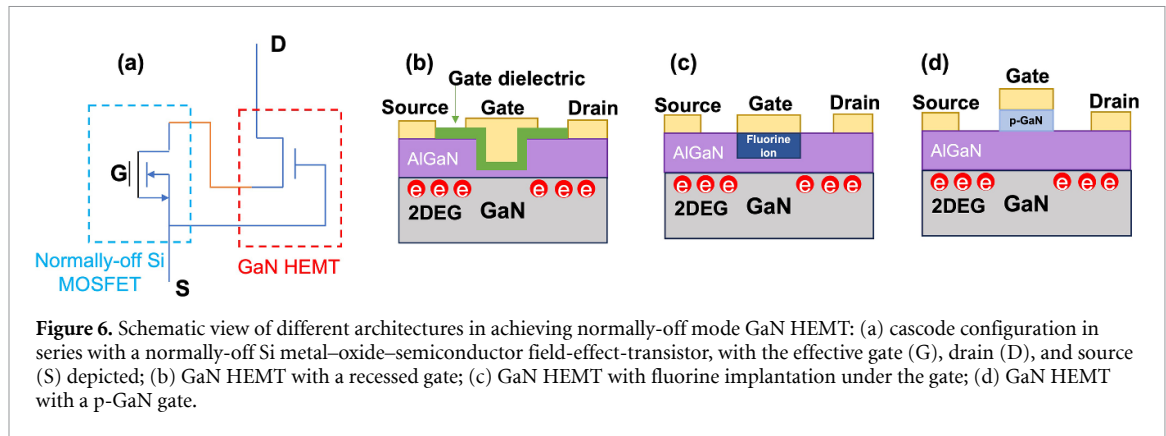
2.3.1.4. HEMTs for power electronics

A 2DEG can be generated at an AlGaIn/GaN interface without any intentional doping due to the polarization-induced charges [96, 97]. High electron mobilities up to $2000\text{ cm}^2\text{ (V}\cdot\text{s)}^{-1}$ at room temperature and high sheet carrier densities of 10^{13} cm^{-2} can be obtained in the 2DEG channel [8]. Low-resistance transistors based on the 2DEG channels in the AlGaIn/GaN heterostructures are referred to as HEMTs. The GaN HEMT has been one of the most successfully commercialized devices in the GaN family. In 2014–2015, Transphorm Inc. first announced their cascode packaged 600 V GaN HEMTs as power switches which meet the standards of the Joint Electron Devices Engineering Council (JEDEC), marking a milestone in the commercialization of GaN in system products [98, 99].

Typically, GaN HEMTs adopt a lateral configuration, consisting of several epitaxial layers on foreign substrates, such as Si, Sapphire, or SiC. The mismatch of the lattice constants and coefficients of thermal expansion between GaN and the foreign substrates usually leads to a high dislocation density (10^8 – 10^{10} cm^{-2}) [100–102], which can be a major source of leakage current and degrade the electrical properties of the 2DEG. Thus, an AlN nucleation layer is typically used as a starting layer for GaN growth to mitigate the stress during the growth and cooling process [46, 103, 104]. On top of an AlN nucleation layer, proper design and growth of buffer layers are critical for HEMTs. A step-graded AlGaIn buffer, several microns in thickness, or a GaN/AlN superlattice structure can be adopted to further mitigate the lattice mismatch before growing the AlGaIn/GaN channel [105, 106], which helps to maintain the excellent electrical properties of the 2DEG.

Due to the nature of the 2DEG channel, HEMTs are usually normally-on devices; however, normally-off operation is preferred in most electronic applications. The cascode configuration, depicted in figure 6(a), allows the normally-off operation of a GaN HEMT without changing the device structure by utilizing a normally-off Si metal-oxide-semiconductor field-effect-transistor (MOSFET) in series with the GaN HEMT device [107–109]. A monolithically integrated Si–GaN cascoded FET has been demonstrated, offering a threshold voltage (V_{th}) of 3.2 V, a specific on-resistance of $3.3\text{ m}\Omega\cdot\text{cm}^2$, and a high breakdown voltage of 696 V [110]. However, the complexity of the packaging process and the limitation of high-temperature operation by the Si devices remain challenges to be addressed [111].

The recessed gate structure (figure 6(b)) fabricated by etching the AlGaIn barrier layer beneath the gate followed by the deposition of a dielectric layer is another approach to achieve normally-off HEMTs [112–114]. The thinning of the AlGaIn layer beneath the gate selectively removes the 2DEG in that region



and shifts the threshold voltage. The etch process is critical, as the plasma-induced damage and the surface roughness caused by etching can degrade the electrical properties of the 2DEG channel [115]. The choice of the gate dielectric is also important for reducing surface states and gate leakage, thus improving the channel mobility and the stability of the threshold voltage [116–119]. The integration of a slant field plate enabled an enhancement mode GaN HEMT with a high breakdown voltage of 1.7 kV and a specific on-resistance of $3 \text{ m}\Omega\cdot\text{cm}^2$ [120]. Fluorine implantation (figure 6(c)) is another attractive method to offer a normally-off operation without plasma etching [121, 122]. The implanted negative fluorine ions change the surface potential and deplete the 2DEG underneath. However, the hysteresis related to the charge trapping effect and the stability of the fluorine ions in the AlGaIn/GaN structure are still practical concerns for this method [123, 124].

Finally, the p-GaN/AlGaIn gate (figure 6(d)) is an alternative promising technique to achieve a positive threshold voltage [125–127]. The presence of a p-type layer elevates the band diagram in the AlGaIn barrier layer, resulting in the depletion of 2DEG at zero bias. A high Mg concentration is required for the desired threshold voltage due to the low ionization ratio of Mg acceptors, however, the crystal quality of GaN may deteriorate with a high Mg concentration [111]. Another feature of the p-GaN gate architecture is the formation of a ‘p–i–n’ structure across the p-GaN gate, AlGaIn barrier, and the GaN channel, which injects additional holes and increases the current capabilities [128]. Additionally, the hole injections assist in de-trapping the electrons captured at the surface states near the drain edge. This helps mitigate current collapse in the device [129], a phenomenon in which the channel resistance increases and current decreases when a high voltage is applied and diminishes the efficiency.

2.3.1.5. Vertical transistors

Despite the excellent conductivity offered by the high carrier density as well as high mobility in GaN HEMTs, vertical configuration transistors are typically favored in power switch applications for higher current density, voltage scalability, and better suppression of the peak electric field.

The vertical trench MOSFET (figure 7(a)) was reported first during the early stages of research due to its relatively easy process in GaN technology. Normally-off operation and tuning of the threshold voltage are possible in trench MOSFETs by adjusting the doping concentration of the p-type buried layer and by choosing the gate dielectric material and thickness. Otake *et al* demonstrated a vertical V-shape trench MOSFET, with a threshold voltage of 5.1 V [130]. In 2015, Oka *et al* reported a 1.2 kV-class trench MOSFET with a specific on-resistance of $1.8 \text{ m}\Omega\cdot\text{cm}^2$ by using field plate edge termination in conjunction with a hexagonal trench gate layout [131]. The low channel mobility arising from the etched semiconductor/gate dielectric interfaces was shown to significantly degrade the on-state performance of the GaN trench MOSFET. To address this issue, the GaN interlayer-based trench MOSFET (OG-FET), as shown in figure 7(b), was proposed and prototyped by Gupta *et al* [132, 133]. The OG-FET incorporated a thin unintentionally doped (UID) GaN interlayer grown at the sidewall of the trench followed by an *in-situ* gate dielectric deposition. The regrown channel offered higher mobility by reducing impurity and interface state scattering. Ji *et al* reported an OG-FET with a channel mobility of $185 \text{ cm}^2 (\text{V}\cdot\text{s})^{-1}$, resulting in an on-resistance of $2.2 \text{ m}\Omega\cdot\text{cm}^2$ for a 1.4 kV transistor enabled by the double FP design [134]. Recently, Tanaka *et al* demonstrated a 1.2 kV vertical GaN MOSFET based on an all-planar ion implantation process without etch [135].

Unlike the trench MOSFET, a current aperture vertical electron transistor (CAVET), shown in figure 7(c) takes advantage of the high mobility of a 2DEG, offering lower on-state resistances and higher current capabilities [136, 137]. CAVETs usually operate under normally-on conditions due to the existence of the

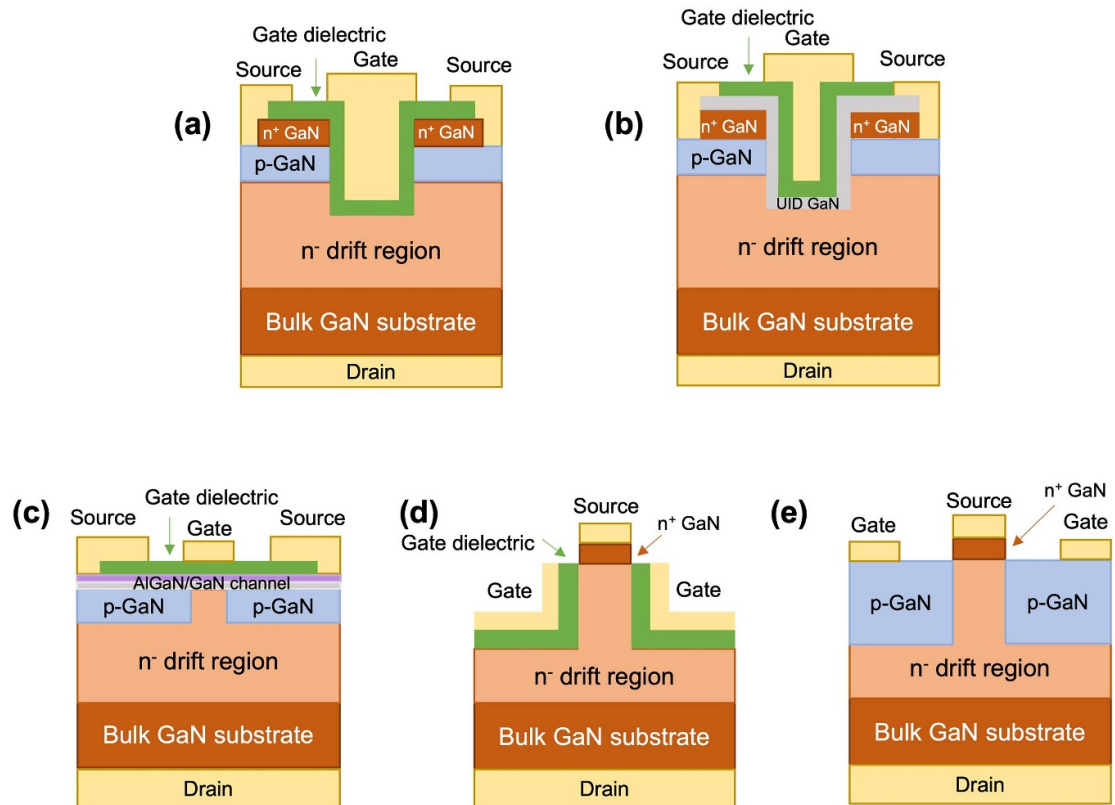


Figure 7. Schematic view of different architectures of vertical GaN transistors: (a) GaN trench MOSFET; (b) GaN interlayer-based trench MOSFET (OG-FET); (c) GaN current aperture vertical electron transistor (CAVET); (d) GaN FinFET; (e) GaN junction field-effect-transistor (JFET).

2DEG; however, normally-off devices can be achieved by adopting similar process techniques used for HEMTs, as mentioned in section 2.3.1.4 [138, 139]. In a CAVET, the current blocking layer is the key to obtaining a high breakdown voltage [140]. An active buried p-GaN layer is ideal for this and allows for avalanche capability; however, from a processing perspective, it is difficult to obtain due to the lack of a mature ion implantation process. Therefore, regrowth of the channel in the aperture is usually required for fabricating CAVETs. Shibata *et al* demonstrated a normally-off CAVET with a p-GaN gate, offering 1.7 kV breakdown voltage and 1 m Ω ·cm² specific on-resistance [141], consequently justifying this device design. Carbon-doped semi-insulating GaN has also been studied as a current blocking and channel layer in vertical GaN transistors [142]. A recent demonstration of a GaN vertical transistor with a semi-insulating channel achieved an on-off ratio of 10⁷ and only marginal trapping effects under 200 ns pulsed mode operation [143]. The growth and integration of a semi-insulating GaN layer may open alternative pathways in designing novel device configurations for vertical GaN transistors.

More recently, transistors utilizing a fin structure (often referred to as GaN-FinFETs), shown in figure 7(d) were prototyped [144–146]. Without the need for a p-type GaN layer, a sufficiently thin fin-shaped channel can be well controlled simply by electrostatic modulation of the gate. For that reason, normally-off operation can be achieved by narrowing the fin width and lowering the doping concentration in the fin. The GaN FinFET exhibited excellent on-state performance due to high electron mobility in the bulk GaN crystal. 1200 V class FinFETs have been demonstrated by Zhang *et al* with low on-resistance and normally-off behavior; however, these devices suffered from catastrophic breakdown [145]. The junction field-effect transistor (JFET), a subset of FinFETs in GaN is shown in figure 7(e). In this device, p-type GaN is regrown surrounding the n-type fin channel and pinches off the channel by expanding the depletion region of the PN junction. JFETs avoid the possible oxide reliability issues in an MOS structure, encouraging avalanche in a three-terminal device. A 1.2 kV GaN JFET was reported by Liu *et al* using nitrogen implantation termination [147]. This design exhibited robust avalanche capability up to 200 °C, showing great potential in medium-voltage power applications [148].

2.3.2. RF devices

2.3.2.1. RF and mm-wave HEMTs

Due to its WBG, high electron mobility, and saturated electron velocity, GaN offers obvious advantages for high-power and high-frequency transistors in terms of output power and efficiency [149]. The formation of a 2DEG channel at the AlGaIn/GaN interface, characterized by high sheet carrier density and high electron mobility, leads to reduced channel resistances and enhanced current capabilities. This makes GaN superior to SiC, particularly in high-frequency applications, even though both materials exhibit similar breakdown properties. However, the absence of a process to grow bulk GaN hindered the development of GaN devices and slowed down its technological maturation. GaN technology witnessed a resurgence of interest when the first GaN LEDs were developed in 1993 by Nakamura *et al* [150] sparking a global competition for the advancement of the field. The development of LEDs not only propelled the GaN market but also facilitated breakthroughs in the RF domain, particularly with the introduction of the first microwave GaN power HEMT in 1996 and the debut of the first GaN monolithic microwave integrated circuit (MMIC) occurring in 2000 [151].

Among the many challenges faced by GaN RF electronics, thermal management became of high importance in high-power GaN monolithic MMICs as this issue hindered amplifier efficiency and reliability. This concern was mitigated through the introduction of SiC semi-insulating substrates during the growth of GaN HEMTs, boasting a TC that was seven times greater than that of GaAs, and ultimately enabled record power densities exceeding 10 W mm^{-1} [152]. Initial demonstration of GaN devices showcased a tenfold improvement in output power density performance relative to Si laterally-diffused metal–oxide–semiconductor (LDMOS) devices, which offered an output power density of 1 W mm^{-1} [153].

Process innovation and novel device design to combat current collapse consume a large fraction of the current research efforts in GaN HEMTs. The surface states on top of the AlGaIn layer constitute the source of the electrons in the 2DEG channel, however, trapping effects related to these surface states are believed to be one of the major causes of current collapse (also referred to as dispersion) [154, 155]. There are three major technical routes to suppress this dispersion, which severely degrades the RF output power of GaN HEMTs. The first approach is the introduction of a passivation layer. Employing SiN_x was demonstrated to effectively reduce the surface states and led to a significant improvement of output power up to 11.2 W mm^{-1} at 10 GHz [156, 157]. Another method is the adoption of field plate technology [152, 158], which enabled the record output power of 41.4 W mm^{-1} at 4 GHz and 30.6 W mm^{-1} at 8 GHz in GaN HEMTs (figures 8(a) and (b)) [159, 160]. The double field plate not only mitigated dispersion effects but also helped in reducing the peak electric field at the drain-side edge of the gate. The third way to address the dispersion phenomenon is at the epitaxial level, by growing a thick capping layer on top of the AlGaIn/GaN channel [161, 162]. The thick capping layer increases the distance from the surface to the channel, thus reducing the trapping effects related to the surface states. The capping layer is usually combined with recessed gate technology to achieve good gate control [163]. By effectively suppressing the gate leakage using fluorine plasma treatment of the recessed gate region, 17.8 W mm^{-1} at 4 GHz was achieved even without a SiN_x passivation layer [164].

Gate length scaling is the most straightforward way to push the operating frequency towards the Ka-band (26–40 GHz) and beyond. Thus, a GaN HEMT utilizing a T-shaped gate with a small gate length of 160 nm exhibited a power density of 10.5 W mm^{-1} at 40 GHz with a power added efficiency (PAE) of 33% [166]. Furthermore, the optimization of the deposition condition of the gate dielectric and the plasma treatment were proposed to passivate the surface states and reduce the gate leakage in HEMTs [167–170]. A HEMT with a thin SiN_x gate dielectric layer grown by plasma-enhanced atomic layer deposition (PEALD) showed a significant reduction in reverse leakage and enhanced breakdown voltage, leading to a 7.16 W mm^{-1} of output power density and a PAE of 60.3% at 28 GHz [171].

While a shorter gate length works effectively to further scale down the GaN HEMT towards higher frequency operation, a high aspect ratio (gate length to the gate-to-channel distance) must be maintained to suppress the short-channel effect [172]. An AlGaIn/GaN HEMT adopting a 6 nm AlGaIn barrier and a 60 nm gate length showed a current gain cut-off frequency (f_T) of 190 GHz and a maximum oscillation frequency (f_{max}) of 227 GHz [173]. However, changing the AlGaIn barrier to a material with a stronger polarization effect, such as InAlN and AlN, was predicted to achieve a higher frequency [174]. A f_T up to 454 GHz has been demonstrated with a 3.5 nm AlN barrier layer and 20 nm gate length [175]. The success of the small-signal characteristics at these high frequencies is not the whole story, the large-signal performance, including the output power and the PAE, must also be validated for a GaN HEMT. GaN HEMT technologies utilizing the Ga-polar orientation have demonstrated good performance with 1.7 W mm^{-1} of output power density and 19.1% PAE at 95 GHz [176]. Similarly, at 86 GHz, a W-band Ga-polar GaN HEMT with an output power of 3.6 W mm^{-1} and 12.3% PAE was demonstrated [177].

With recent improvements in the epitaxial growth of N-polar GaN, N-polar GaN HEMTs have demonstrated some of the highest power densities at mm-wave frequencies, outperforming their Ga-polar

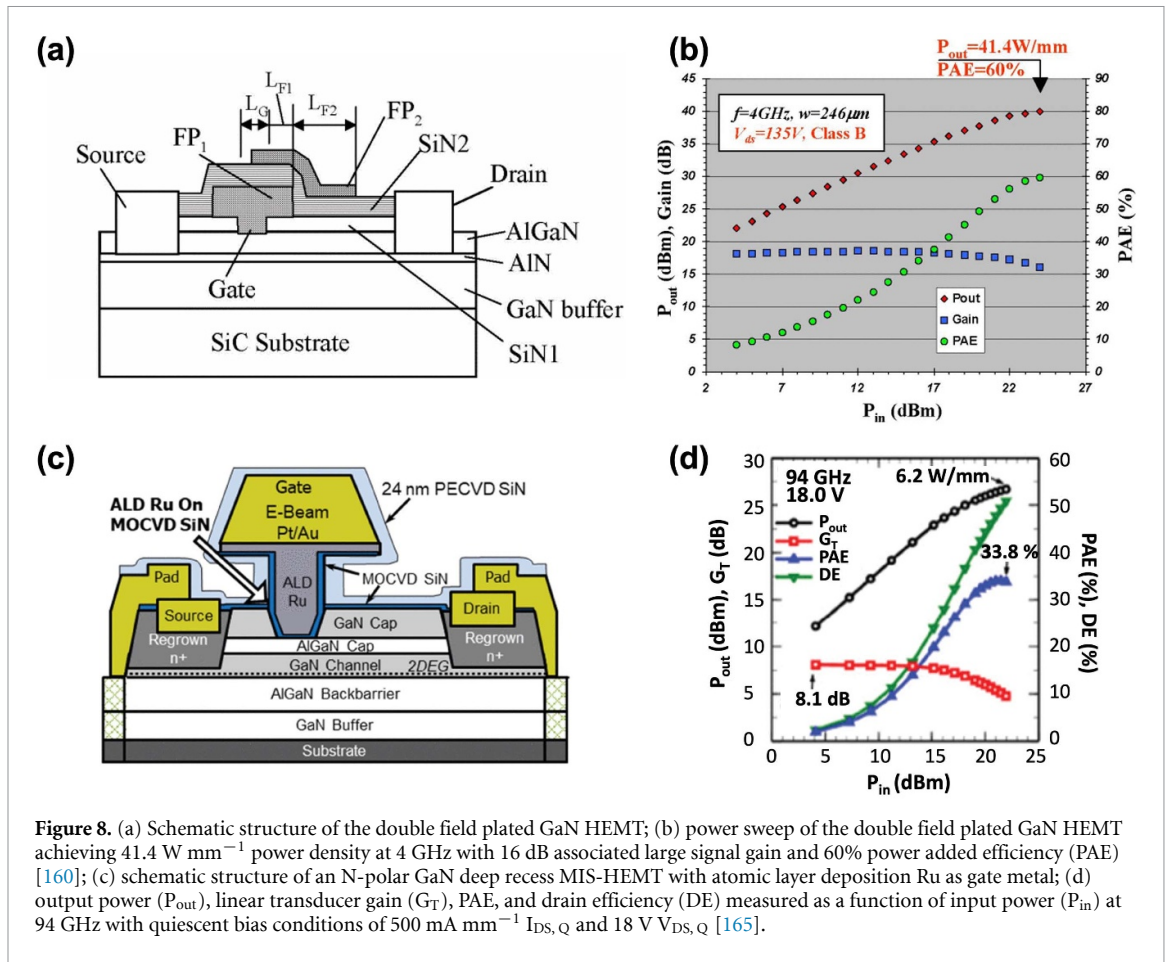
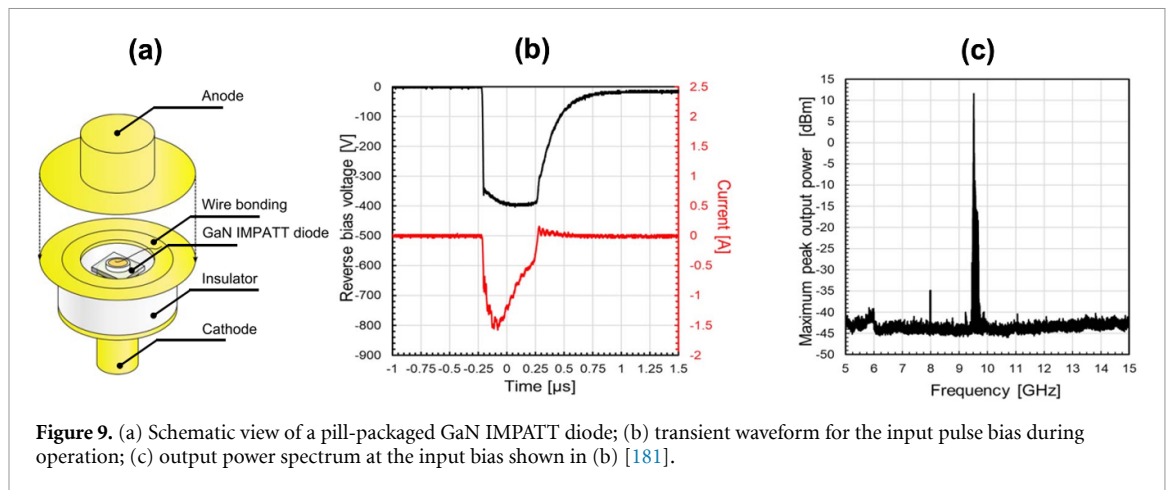


Figure 8. (a) Schematic structure of the double field plated GaN HEMT; (b) power sweep of the double field plated GaN HEMT achieving 41.4 W mm^{-1} power density at 4 GHz with 16 dB associated large signal gain and 60% power added efficiency (PAE) [160]; (c) schematic structure of an N-polar GaN deep recess MIS-HEMT with atomic layer deposition Ru as gate metal; (d) output power (P_{out}), linear transducer gain (G_T), PAE, and drain efficiency (DE) measured as a function of input power (P_{in}) at 94 GHz with quiescent bias conditions of 500 mA mm^{-1} $I_{DS,Q}$ and 18 V $V_{DS,Q}$ [165].

counterparts. The advantages of N-polar structures include higher scalability, lower resistivity ohmic contacts, lower gate capacitance, and a more effective back barrier. 8 W mm^{-1} output power at 94 GHz with a PAE of 28.8% has been achieved in an N-polar GaN HEMT using a self-aligned foot gate process [178]. Atomic layer deposited (ALD) Ru was shown to effectively fill in the T-shaped gate trench to help realize shorter gate length below 60 nm and minimize the gate resistance, giving rise to an output power density of 6.2 W mm^{-1} with a high PAE of 33.8% at 94 GHz (figures 8(c) and (d)) [165]. A record-high 9.65 dB linear transducer gain and demonstrated 42% PAE with associated 4.4 W mm^{-1} of output power density at 94 GHz have also been demonstrated for N-polar HEMTs on sapphire substrates [179].

2.3.2.2. Impact ionization avalanche time transit diodes (IMPATTs)

IMPATTs are powerful solid-state sub-THz sources in fundamental mode. When properly packaged, these devices can replace elaborate amplifiers and multiplier chains and offer exceptionally high output power at remarkably high frequencies. The output power in IMPATTs comes from the phase difference in voltage and current, caused by the time delay from carrier avalanche multiplication and transition through the drift region. To the first order, the operation frequency is inversely proportional to the thickness of the depletion region (W_{dep}), determined by $f_{opt} = \frac{v_{sat}}{2W_{dep}}$, and the operation voltage is set by the critical field of the material. Much higher performance is expected for GaN-based IMPATT diodes compared to Si and GaAs-based due to their high critical field and high electron saturation velocity. Owing to the advancement of low dislocation density bulk GaN growth, avalanche in GaN PN diodes is now more routinely achieved. Ji *et al* first demonstrated a GaN IMPATT diode as a series resonant oscillator, showing an oscillation frequency at 800 MHz [180]. Limited by the avalanche current and the lack of a heat sink, the frequency was much below the theoretical predictions. Later, Kawasaki *et al* mounted the GaN IMPATT diode on a copper heat sink in a pill package and operated the device under 500 ns pulse mode (figure 9) [181]. The device showed a maximum oscillation frequency of 9.5 GHz at a current density of 2.2 kA cm^{-2} , offering a peak output power of 14.45 mW. More recently, by decreasing the junction diameter and capacitance, more than 30 dBm output power was achieved up to 21 GHz by Kawasaki *et al* [182]. Further reduction of the series resistance and higher biasing current are expected to improve the device performance at higher frequencies.



3. Aluminum gallium nitride/aluminum nitride (AlGaN/AlN)

3.1. Material properties

From GaN, we transition into the UWBG materials family starting with AlGa_N, another III–V material. AlGa_N alloys with varying Al mole fractions are promising due to their tunable bandgaps spanning a wide range, from 3.4 to 6.0 eV. The material band gap increases as Al composition increases until 100% to form AlN. Higher critical electric fields can enable device operation with lower leakage current and higher breakdown voltages [183–185]. Thus, AlGa_N with higher a Al composition is of high interest. At the opposite extreme of GaN, AlN has one of the widest direct bandgaps of 6.0 eV, generating significant attention for applications in UV optoelectronics. The large bandgap of AlN leads to a high critical electric field of 15.4 MV cm⁻¹, and a very high TC (highest reported 321 W (m·K)⁻¹ [186]), which is naturally appealing for power and RF electronics as well.

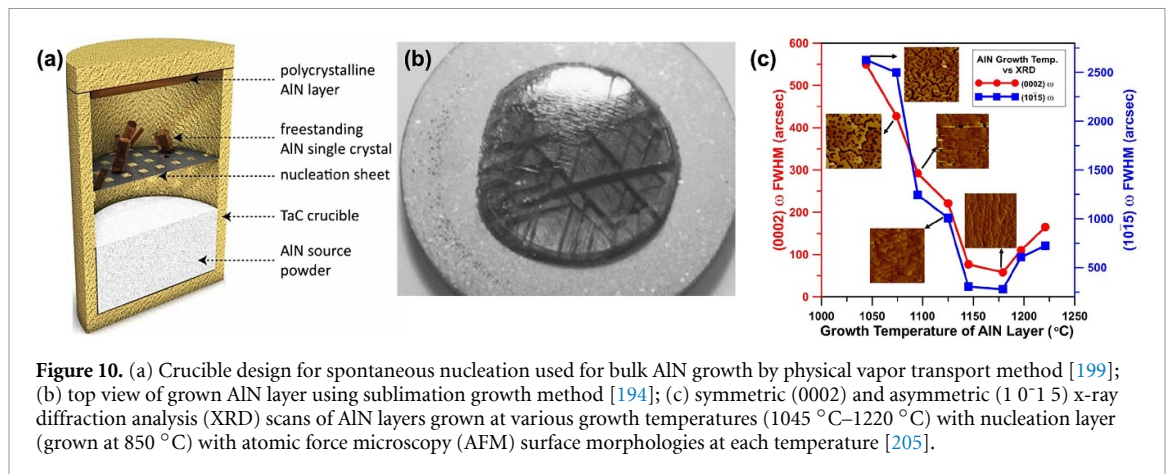
Similar to GaN, a 2DEG is formed at an AlGa_N/AlGa_N interface (with two different AlGa_N compositions) without any intentional doping due to polarization-induced charges. The 2DEG mobility in different AlGa_N channels varies based on the Al composition of the channel, and the barrier material and is dominated by alloy scattering. For example, MBE-grown HEMTs with Al_{0.06}Ga_{0.94}N and Al_{0.15}Ga_{0.85}N channels were reported to have 2DEG mobilities of 590 cm² (V·s)⁻¹ [187] and 430 cm² (V·s)⁻¹ [188], respectively. While the mobility values are lower than in GaN 2DEG channels, higher breakdown voltages are expected with increasing Al mole fractions [189]. For example, assuming the critical electric field of GaN to be 3 MV cm⁻¹, >9 MV cm⁻¹ was estimated for a 75% Al mole fraction AlGa_N channel.

In AlN, the highest room temperature bulk electron mobility measured is 426 cm² (V·s)⁻¹ with a Si doping concentration of 3 × 10¹⁷ cm⁻³, and 125 cm² (V·s)⁻¹ was achieved in more highly doped AlN (10¹⁸ cm⁻³) [190]. Previously, the same group measured a value of only 125 cm² (V·s)⁻¹ at low doping concentrations on the order of 10¹⁵ cm⁻³. The vast mobility improvement was attributed to the decreased number of threading dislocations realized by suppressing the parasitic reaction of Al and N sources during growth.

3.2. Growth and doping

3.2.1. Bulk AlN growth

Among the different polymorphs of AlN, the wurtzite crystal structure, first reported by Heinrich Otto in 1924, is most commonly studied for both bulk and epitaxially grown AlN [191]. For the growth of bulk AlN single crystals, HVPE [192] and physical vapor transport (PVT) [193] are two of the most widely used methods. Typically, AlN crystals are difficult to grow using common crystal growth methods such as pulling and hot melt [194] due to their high melting point of 2800 °C and dissociation pressure of 20 MPa. While both the HVPE and PVT methods have been utilized to grow thick AlN films with low screw dislocation density (of the order 10³ cm⁻²) [195], HVPE growth is significantly slower in comparison to PVT methods [196]. Thus, PVT methods are predominantly used in the growth of bulk AlN substrates due to their simpler and safer growth process, faster growth rate, and good crystal integrity. Two PVT approaches are primarily used: growth of thick AlN on 4H–/6H–SiC substrates [197–199] shown in figure 10(a) and spontaneous nucleation followed by freestanding AlN growth [200, 201]. A detailed study of PVT-AlN growth on SiC templates for varying growth temperatures and orientations of SiC further exhibited that off-axis Si-face SiC



offers a flat morphology and better crystalline quality [202]. The largest AlN wafer prepared by PVT to date is 40 mm in diameter with a low impurity concentration of <0.01% [197, 203].

3.2.2. Epitaxial growth of AlN

To achieve epitaxial growth of AlN, several methods, including MOCVD, MBE, pulse laser deposition (PLD), and sputtering have been demonstrated. The MOCVD method is suitable for mass production because of its low deposition temperature and wide growth temperature range [204]. Using MOCVD, high-quality AlN homoepitaxy with low background impurity concentration was demonstrated on single crystal AlN substrates [193]. Thick ($\sim 2 \mu\text{m}$), crack-free AlN growths with high crystalline quality, shown in figure 10(c), were also achieved on sapphire substrates via a sandwich method [205] and by using a patterned sapphire substrate [206]. Epitaxial lateral overgrowth-AlN layers with low crack and threading dislocation densities have also been reported to grow on thin, stripe-patterned AlN seed layers directly deposited on Si (111) substrates [207].

The epitaxial growth of AlN using MBE is limited to a slow growth rate; however, the growth process is easier to control. Using MBE, the growth of AlN on a sapphire substrate was improved to yield a better surface morphology via a nitridation step [208]. Additionally, smooth and strain-free AlN was grown by MBE directly on a Si substrate with a nanowire template [209]. The PLD method is used for the growth of thinner AlN films with good crystallinity and stoichiometry at relatively low temperatures of 800 °C [210, 211]. Under optimum growth conditions, a single-crystal AlN layer as thin as $\sim 1.5 \text{ nm}$ was demonstrated on a Si substrate [212]. For large-area deposition of AlN films, the sputtering method comes with the advantages of a simpler process and lower cost. Using RF reactive sputtering, AlN layers were directly grown on a *c*-axis sapphire substrate, and crystalline quality was found to improve with increasing nitrogen gas fraction during reactive sputtering and RF power [213].

3.2.3. Epitaxial growth of AlGaN

Following the realization of high-quality GaN grown on low-temperature AlN buffer layers in 1986 [46], the growth of AlGaN and AlGaN/GaN heterojunctions gained significant attention over the past three decades with vast application prospects in high temperature, high power, RF, and optoelectronic devices [214–217]. AlGaN films were first grown as buffer layers for the growth of GaN or AlN epilayers. Following the enhanced understanding of the growth mechanism and optimized growth process over the years, the quality of the AlGaN films was improved by adopting epitaxial growth techniques such as MBE [218] and MOCVD [219]. For example, an $\text{Al}_{0.2}\text{Ga}_{0.8}\text{N}$ layer grown at 1050 °C was demonstrated with the insertion of low-temperature AlGaN interlayers using MOCVD. This resulted in the simultaneous reduction of tensile stress and crack formation, which is typically observed from the growth of high-temperature AlGaN directly on GaN epilayers [220]. Fully relaxed, crack-free, $1.3 \mu\text{m}$ thick $\text{Al}_{0.32}\text{Ga}_{0.68}\text{N}$ layers were reported on GaN-on-porous-GaN pseudo-substrates (figure 11(a)) [221]. Moreover, UID AlGaN epilayers graded over Al compositions of 80%–90% and 80%–100% were also demonstrated using MOCVD [222]. Process condition optimizations such as low temperatures and ammonia-rich conditions were used to increase the growth rate of AlGaN up to $3.2 \mu\text{m h}^{-1}$ [223]. Concurrently, the Al composition was found to be affected by the growth temperature and growth rate.

The HVPE method is also used for the growth of AlGaN with low threading dislocation densities and smoother surfaces. The epitaxial growth of $\text{Al}_{0.10}\text{Ga}_{0.90}\text{N}$ on an AlN/nanopatterned sapphire substrate (NPSS) template by HVPE resulted in a low threading dislocation density of $1.4 \times 10^9 \text{ cm}^{-2}$ of the AlGaN

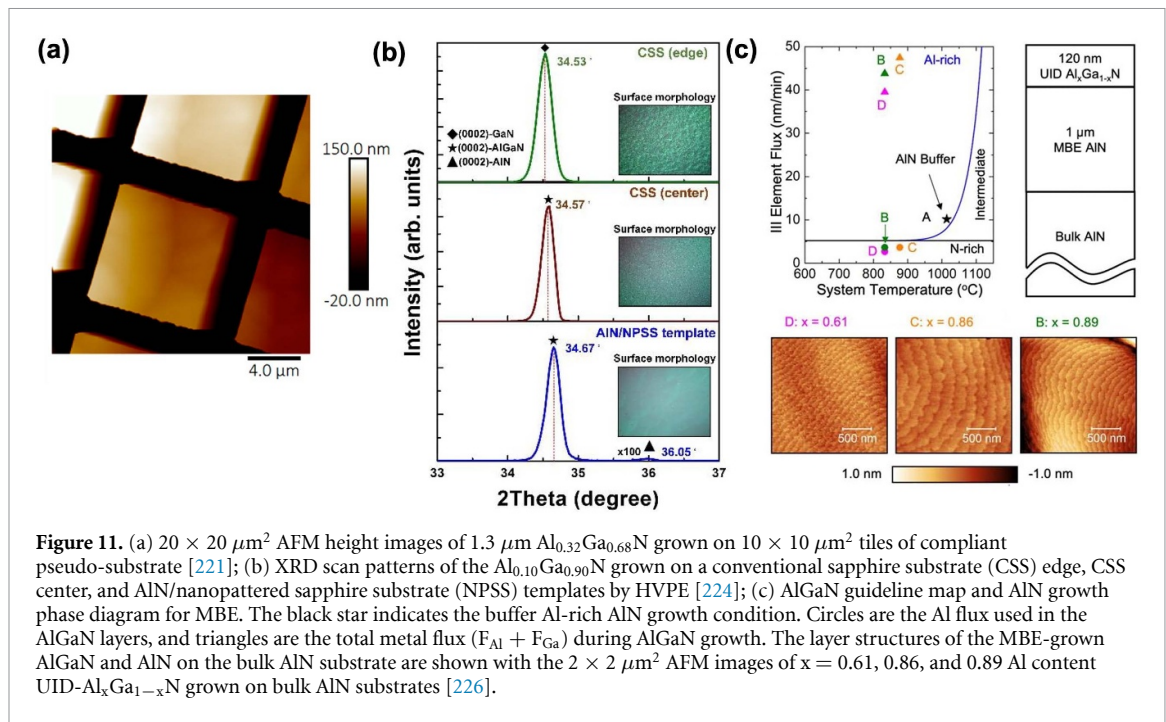
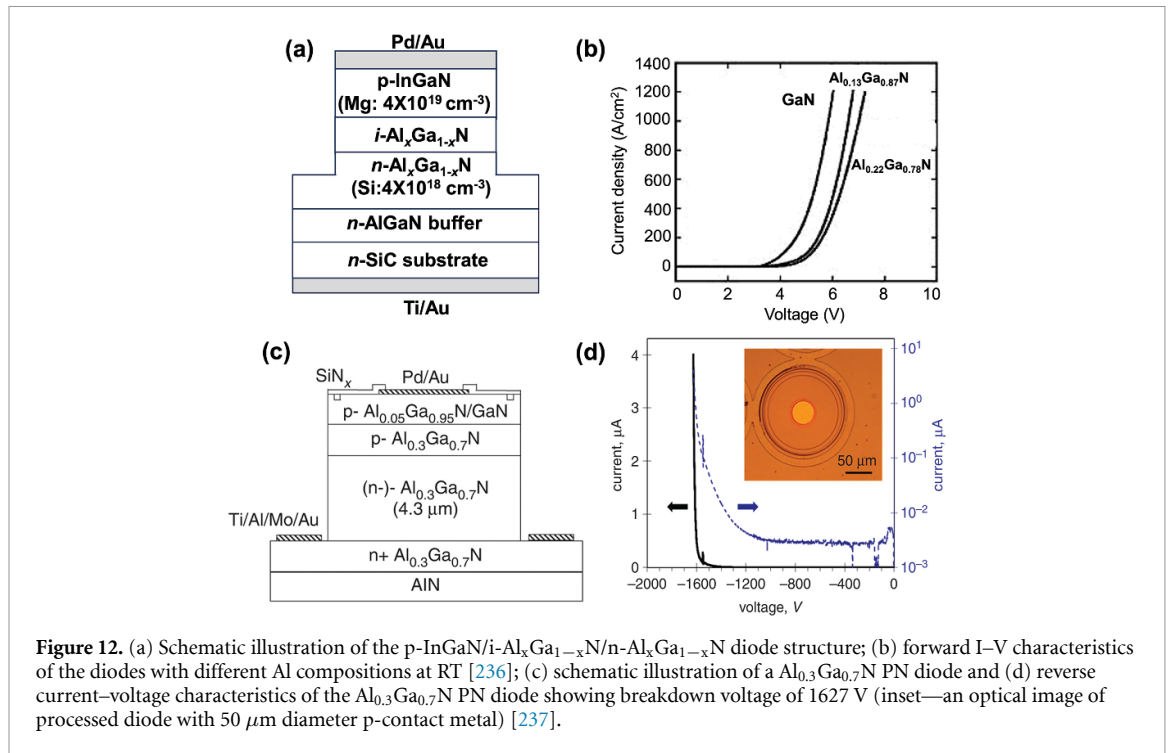


Figure 11. (a) $20 \times 20 \mu\text{m}^2$ AFM height images of $1.3 \mu\text{m}$ $\text{Al}_{0.32}\text{Ga}_{0.68}\text{N}$ grown on $10 \times 10 \mu\text{m}^2$ tiles of compliant pseudo-substrate [221]; (b) XRD scan patterns of the $\text{Al}_{0.10}\text{Ga}_{0.90}\text{N}$ grown on a conventional sapphire substrate (CSS) edge, CSS center, and AlN/nanopatterned sapphire substrate (NPSS) templates by HVPE [224]; (c) AlGaIn guideline map and AlN growth phase diagram for MBE. The black star indicates the buffer Al-rich AlN growth condition. Circles are the Al flux used in the AlGaIn layers, and triangles are the total metal flux ($F_{\text{Al}} + F_{\text{Ga}}$) during AlGaIn growth. The layer structures of the MBE-grown AlGaIn and AlN on the bulk AlN substrate are shown with the $2 \times 2 \mu\text{m}^2$ AFM images of $x = 0.61, 0.86, \text{ and } 0.89$ Al content UID- $\text{Al}_x\text{Ga}_{1-x}\text{N}$ grown on bulk AlN substrates [226].

epilayer owing to in-plane stress relaxation [224]. Further process optimization in HVPE such as etching to suppress parasitic reactions was explored to achieve thick n-AlGaIn cladding layers and free-standing AlGaIn substrates on both GaN and AlN templates [225]. MBE-grown AlGaIn alloys with high mole fractions of Al on single-crystal AlN substrates were also reported and shown in figure 11(c). For example, pseudomorph $\text{Al}_x\text{Ga}_{1-x}\text{N}$ epitaxial layers with $x \sim 0.6\text{--}1.0$ were grown using MBE at a growth rate of $0.3 \mu\text{m h}^{-1}$ [226].

3.2.4. Doping in AlGaIn/AlN

For the successful adoption of UWBG materials in technologically relevant applications, doping and its controllability are regarded as cornerstones. Doping of AlGaIn is difficult to achieve compared to GaN, and the ability to dope such alloys significantly decreases with increasing Al content. This can be attributed to the fact that most dopant ionization energies increase with bandgap, therefore decreasing the fraction of free carriers that are thermodynamically activated [3]. For AlGaIn/AlN, doping strategies that exploit broken crystal symmetries, such as polarization induced doping are useful for supplementing the traditional chemical substitutional doping. Modulation doping is also utilized for enhancing the number of confined carriers in the material system. Several p-type doping approaches, such as superlattice doping [227], Mg delta doping [228], and Mg-Si alternative co-doping [229] have been investigated for improving the doping efficiency of Al-rich AlGaIn. Using Mg delta doping, a hole concentration of $8.3 \times 10^{18} \text{ cm}^{-3}$ with Mg doping concentration of $1.6 \times 10^{19} \text{ cm}^{-3}$ was achieved, indicating a doping efficiency of up to 51.9% [230]. On the other hand, Si is primarily used as the n-type dopant for AlGaIn with high Al content [231], including AlN. For example, Taniyasu *et al* demonstrated n-type conduction in Si-doped AlN showing a room temperature Hall mobility of $426 \text{ cm}^2 \text{ V}^{-1} \text{ s}^{-1}$ and electron concentration of $7.3 \times 10^{14} \text{ cm}^{-3}$. The study also demonstrated p-type conduction in Mg-doped AlN with a Mg concentration of $2 \times 10^{20} \text{ cm}^{-3}$ and thermally annealed at 800°C for 10 min. Beyond $2 \times 10^{20} \text{ cm}^{-3}$ concentrations, Mg doped AlN becomes highly resistive due to a self-compensation effect [232], a phenomenon also found in n-type Si doped AlN. Typically, an increase in the Si content leads to an increase in free electrons; however, this trend does not continue at higher doping levels. A further increase in the Si concentration leads to a decrease in the free electron concentration, commonly referred to as the compensation knee [232–234]. A variety of compensating defects can be the culprit, but the mechanism and identity of these defects have not been conclusively determined yet. Researchers have tried different dopants as well, and successful experimental achievement of both n-type AlN:Si films using the metal modulated epitaxy (MME) method and p-type AlN:Be films was demonstrated [235].



3.3. AlGaN devices and applications

3.3.1. High power devices

3.3.1.1. PIN diodes

The larger bandgaps of AlGaN compositions are promising for offering extremely low reverse leakage currents and exceptionally high breakdown voltages in AlGaN-based PIN diodes. In 2006, Nishikawa *et al* demonstrated metal-organic vapor phase epitaxy (MOVPE)-grown AlGaN PIN diodes with intrinsic layers of unintentionally doped Al_{0.13}Ga_{0.87}N and Al_{0.22}Ga_{0.78}N, separately [236]. The PIN structure was grown on a conductive n-SiC substrate and capped by a p-InGaN layer that helped to reduce the ohmic contact resistances. Using only a ~225 nm thick intrinsic layer, the Al_{0.22}Ga_{0.78}N diode offered a breakdown voltage of 78 V with an on-resistance of 1 mΩ·cm², while the reference GaN diode exhibited a lower breakdown voltage of 54 V (figures 12(a) and (b)). The corresponding critical electric fields were calculated to be 3.5 MV cm⁻¹ and 2.4 MV cm⁻¹, respectively, assuming the intrinsic layer was fully depleted. In 2007, the same group reported another PIN diode with an intrinsic layer of Al_{0.57}Ga_{0.43}N (225 nm), showing 185 V breakdown voltage resulting in a critical electric field of 8.1 MV cm⁻¹. The maximum BFOM was shown with 30% of Al composition because of the tradeoff between breakdown voltage and on-state resistance and is twice as high as that for GaN-based diodes, showing promise for high-power operation in AlGaN-based devices [214].

In 2016, MOVPE-grown Al_{0.3}Ga_{0.7}N quasi-vertical PN diodes on a non-conductive sapphire substrate were reported where a remarkably low reverse leakage current of <3 nA was achieved. The breakdown voltage for this diode was 1600 V with an estimated critical electric field of 5.9 MV cm⁻¹ (figures 12(c) and (d)). As a comparison, an ideal planar GaN PN diode with the same breakdown would require a ~7 μm-thick drift region with a background carrier concentration of <2.4 × 10¹⁶ cm⁻³ [237]. A specific on-resistance of 16 mΩ·cm² was reported at a current density of 1.5 mA cm⁻². The relatively high resistance was a consequence of the n-type contact layer in the front-contacted device geometry, but comparable with 14 mΩ·cm² reported for a GaN PN diode grown on sapphire [238].

3.3.1.2. HEMTs

In power electronics, vertical device structures are typically favored for areal efficiency and elimination of surface state effects. Nonetheless, lateral device structures in U/WBG materials are still important, as seen in GaN-channel HEMTs, due to the advantage of higher channel mobility. Previously, the role of AlGaN in AlGaN/GaN HEMTs was introduced. Here, only fully Al_xGa_{1-x}N structures will be discussed. Both lateral and vertical AlGaN device structures are still in their infancy, but lateral devices are more readily achievable due to existing bulk growth limitations. The growth and device optimization of AlGaN channel HEMTs have been reported in several studies. A HEMT structure of Al_{0.53}Ga_{0.47}N/Al_{0.38}Ga_{0.62}N achieved a maximum breakdown voltage of 1650 V with a gate to drain distance of 10 μm [215]. In 2010, an AlGaN-channel

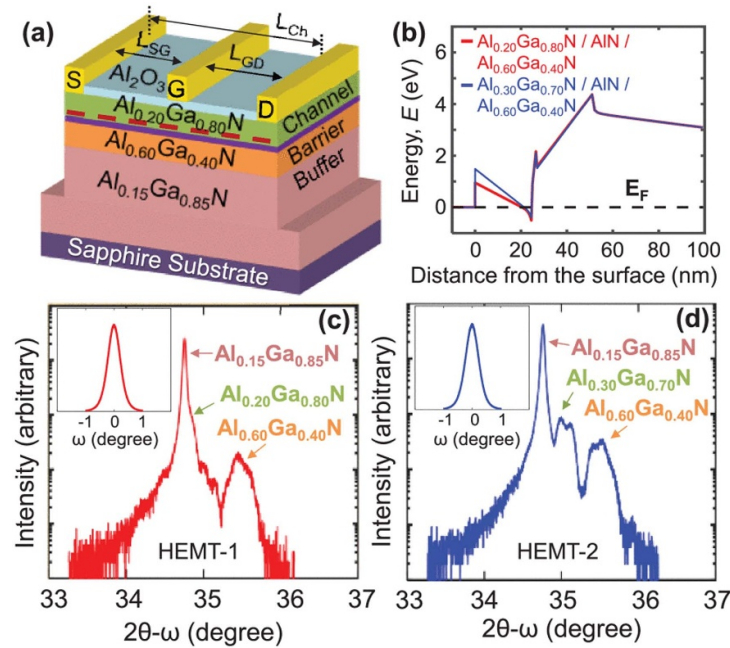
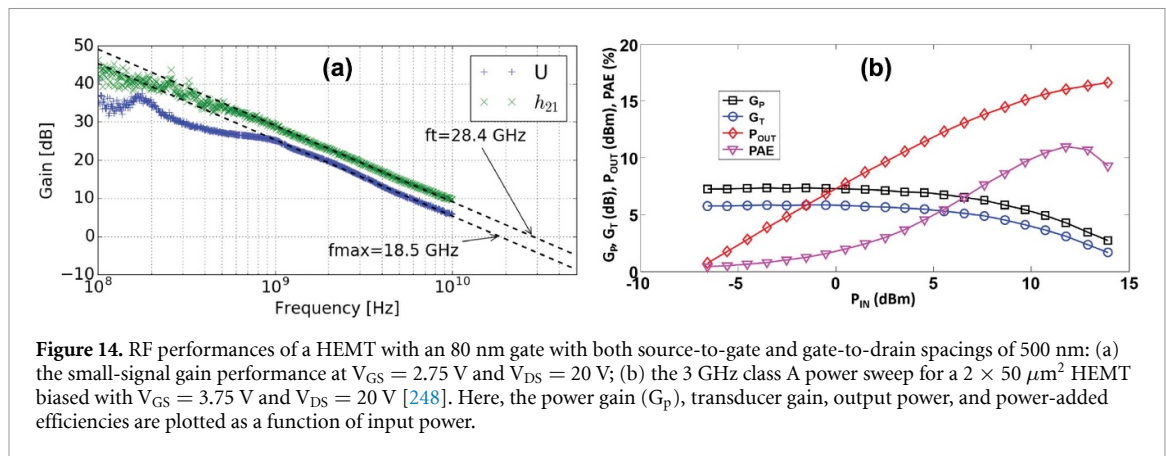


Figure 13. (a) Schematic of all-AlGaN N-polar HEMT device with an $\text{Al}_{0.20}\text{Ga}_{0.80}\text{N}$ channel layer and an $\text{Al}_{0.30}\text{Ga}_{0.70}\text{N}$ channel layer; (b) the simulated band diagrams of $\text{Al}_{0.20}\text{Ga}_{0.80}\text{N}$ channel and $\text{Al}_{0.30}\text{Ga}_{0.70}\text{N}$ channel HEMTs. (c), (d) XRD spectra (2θ - ω scan of (002) plane) of these structures, confirming the stoichiometries of all-AlGaN HEMT structures [189].

HEMT with a high Al composition of over 0.5 ($\text{Al}_{0.51}\text{Ga}_{0.49}\text{N}$) was first reported. The HEMT structure was grown on a free-standing AlN substrate to improve crystalline quality, and the fabricated device exhibited a maximum drain current of 25.2 mA mm^{-1} and a breakdown voltage of 1800 V [239]. A metal stack, composed of Zr/Al/Mo/Au, was found to show low contact resistivity for source and drain ohmic contacts for AlN/AlGaN HEMT with AlN as a barrier layer. This HEMT also demonstrated low degradation of drain current at temperatures from 300 K to 573 K showing stable high-temperature operation [240]. An $\text{Al}_{0.85}\text{Ga}_{0.15}\text{N}$ channel HEMT was demonstrated in 2016 showing a very low off-state leakage current of $10^{-7} \text{ mA mm}^{-1}$. The device's reported breakdown was 810 V, which corresponds to an average field of 0.81 MV cm^{-1} . This is only a fraction of the predicted critical electric field in $\text{Al}_{0.85}\text{Ga}_{0.15}\text{N}$ (13 MV cm^{-1}), due to the immature state of the material [216]. Although most of the reported efforts discuss the investigation of metal polar AlGaN channel based HEMT structures, very recently MOCVD-based growth of N-polar AlGaN channel HEMT structures with varying Al mole fractions in the $\text{Al}_x\text{Ga}_{1-x}\text{N}$ channel has been demonstrated [241]. The N-polar all-AlGaN HEMT with 0.2 Al in the channel and $3 \mu\text{m}$ channel length offered a drive current of 375 mA mm^{-1} while maintaining a low on-state leakage current of $\sim 0.5 \text{ nA mm}^{-1}$ and $>400 \text{ V}$ breakdown voltage [189], promising for high power electronic applications (figure 13).

3.3.2. RF HEMTs

AlGaN channel based HEMT structures as high-frequency devices have shown significant advancement in the last decade. Raman *et al* demonstrated a low Al composition $\text{Al}_{0.06}\text{Ga}_{0.94}\text{N}$ channel HEMT, which showed an f_T of 13.2 GHz and f_{max} of 41 GHz. At 4 GHz, the output power was 4.5 W mm^{-1} demonstrating the potential of AlGaN channel HEMTs for high-voltage switching and microwave power applications [242]. Bajaj *et al* demonstrated nearly constant f_T and f_{max} profiles in a scaled graded-AlGaN (0%–30% Al) channel with an f_T of 52 GHz and an associated f_{max} of 67 GHz, and the demonstrated flat f_T and f_{max} profiles could help to improve the linearity performance of devices [243]. With a linearly graded AlGaN channel polarization doped field effect transistor (PolFET), X-band power and linearity performance were reported for the first time in 2018 with a third-order output intercept (OIP3) of 33 dBm, and OIP3/ P_{DC} (DC power consumption) of 3.4 dB [244]. In 2020, Xue *et al* reported an $\text{Al}_{0.65}\text{Ga}_{0.35}\text{N}/\text{Al}_{0.4}\text{Ga}_{0.6}\text{N}$ HEMT with a current density of 900 mA mm^{-1} , f_T of 20 GHz, and f_{max} of 36 MHz. The off-state breakdown voltage in these devices was 80 V with $1 \mu\text{m}$ gate to drain separation and a gate length of 100 nm [217]. The same group demonstrated an exceptionally low gate leakage current density of $1.4 \times 10^{-8} \text{ mA mm}^{-1}$ even at a high forward gate bias of V_{GS} of 12 V, and a current on/off ratio $>10^{10}$ was achieved simultaneously. Small signal measurement showed that the device has an f_T of 3.8 GHz and f_{max} of 4.5 GHz for the same Al compositions [245].



The RF operation of AlGaIn channel transistor with Al-composition above 80% was first reported in 2018 demonstrating an impressive current density of 265 mA mm^{-1} for a gate length of $0.8 \mu\text{m}$. The reported f_T/f_{max} were 5.4/14.2 GHz respectively [246]. An $\text{Al}_{0.75}\text{Ga}_{0.25}\text{N}/\text{Al}_{0.6}\text{Ga}_{0.4}\text{N}$ HEMT was also reported with a drain current density ($I_{D,\text{max}}$) of 460 mA mm^{-1} for a gate length of 130 nm. The small signal measurement showed a current/power gain cutoff frequency (f_T/f_{max}) of 40 GHz/58 GHz [247]. Also, $\text{Al}_{0.85}\text{Ga}_{0.15}\text{N}/\text{Al}_{0.7}\text{Ga}_{0.3}\text{N}$ HEMT with 80 nm gate was reported to display a maximum current of 160 mA mm^{-1} with f_T of 28.4 GHz and f_{max} of 18.5 GHz (figure 14) [248].

3.4. AlN devices and applications

3.4.1. High power devices

3.4.1.1. Schottky barrier and PN diodes

In 2015, thick n-type AlN layers were homoepitaxially grown by HVPE on AlN (0001) seed substrates, and a SBD was fabricated using Ni/Au Schottky contacts. High rectification with a turn-on voltage of approximately 2.2 V was observed along with a reverse breakdown voltage of >550 V [249]. Maeda *et al* reported an AlN quasi-vertical SBD fabricated on an AlN bulk substrate. An undoped AlN layer, a Si-doped $\text{Al}_{0.9}\text{Ga}_{0.1}\text{N}$ current spreading layer, and an AlN buffer layer were grown by plasma-enhanced MBE. This device was reported to withstand at least 100 V reverse breakdown voltage; however, the on-resistance was high ($1.8 \Omega\cdot\text{cm}^2$) [250]. In 2017, Fu *et al* were the first to demonstrate 1 kV-class AlN SBDs on sapphire substrates grown by MOCVD. The device showed a low turn-on voltage of 1.2 V, a relatively high on/off ratio of $\sim 10^5$, and a low reverse leakage current <1 nA. The devices also exhibited excellent thermal stability over 500 K and a breakdown voltage of ~ 1 kV without any use of additional edge termination methods (figures 15(a) and (b)) [251]. Researchers have demonstrated few AlN-based PIN diodes as the challenge of growing thick AlN layers remains a primary obstacle in addition to difficulties in doping. Recently, however, an AlN PN diode with a nearly ideal turn-on voltage of ~ 6 V was demonstrated with a hole concentration of $3.1 \times 10^{18} \text{ cm}^{-3}$ and an electron concentration of $6 \times 10^{18} \text{ cm}^{-3}$ [235].

3.4.1.2. Metal–semiconductor field effect transistors (MESFETs)

In 2022, Hiroki *et al* reported the first AlN MESFET with epitaxially grown n-type AlN channel layers and achieved an off-state breakdown voltage of 1.72 kV with a $16 \mu\text{m}$ channel gate to drain distance. This result was attributed to the growth of comparatively low defect AlN using a high-temperature MOCVD with a uniquely designed reactor. To achieve good ohmic contacts, a graded AlGaIn layer between AlN and metal electrodes was used. With increasing temperature from room temperature to 500°C , both on-current and transconductance increased while maintaining a small reverse leakage current of $1.6 \times 10^{-11} \text{ A mm}^{-1}$, leading to a large on/off ratio of $\sim 10^5$ even at 500°C . The results indicate that AlN MESFETs with epitaxially grown n-type AlN channel layers are promising for high-voltage applications at high temperatures (figures 15(c)–(e)) [233].

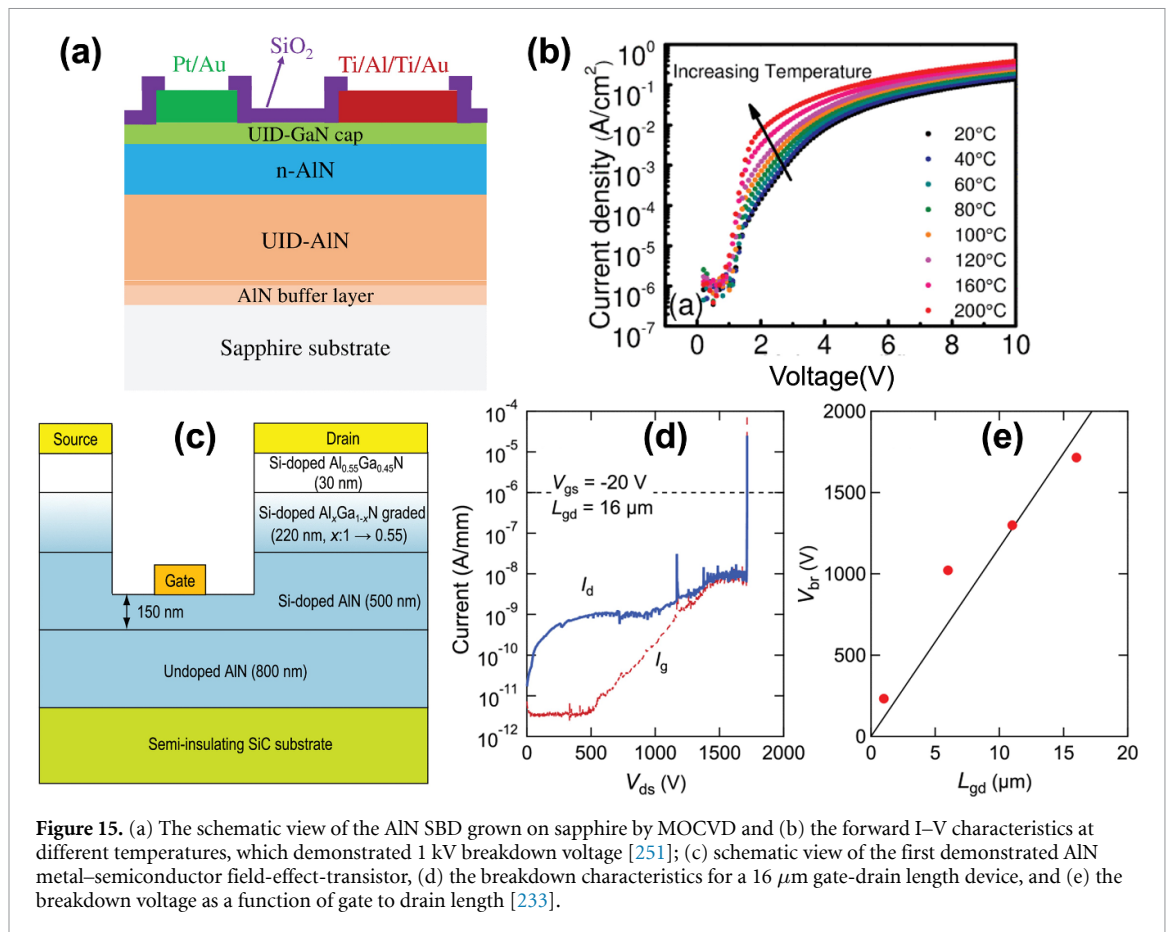


Figure 15. (a) The schematic view of the AlN SBD grown on sapphire by MOCVD and (b) the forward I-V characteristics at different temperatures, which demonstrated 1 kV breakdown voltage [251]; (c) schematic view of the first demonstrated AlN metal-semiconductor field-effect-transistor, (d) the breakdown characteristics for a 16 μm gate-drain length device, and (e) the breakdown voltage as a function of gate to drain length [233].

4. Diamond

4.1. Material properties

As depicted in figure 1(a), diamond has outstanding properties across the board for power and high frequency electronics. Diamond has an indirect band gap of 5.47 eV with an expected ultra-high critical field of $>10 \text{ MV cm}^{-1}$ at which point it would theoretically breakdown by the avalanche phenomenon [252, 253]. Indicators for avalanche breakdown have been observed by Ohmagari *et al* in PIN diodes which exhibited positive temperature coefficients [254]; however, the observation has not been widely reproduced and further studies are required to better understand the phenomenon.

While high critical field values are expected in all UWBG materials, diamond is unique in that it has both high electron and hole bulk mobilities, unlike in GaN and Ga₂O₃. Using time-of-flight experiments, low field drift mobilities of $3500\text{--}4500 \text{ cm}^2 (\text{V}\cdot\text{s})^{-1}$ and $2600\text{--}3800 \text{ cm}^2 (\text{V}\cdot\text{s})^{-1}$ were extracted for electrons and holes, respectively, and carrier lifetimes were estimated to be $>2 \mu\text{s}$. The high mobilities were attributed to the high-quality growth of homoepitaxial CVD diamond [255]. These values have been pushed even higher by the extrapolation of time-resolved cyclotron resonance measurements of ultrapure diamond to room temperature. This yielded record high mobilities of 7300 and $5300 \text{ cm}^2 (\text{V}\cdot\text{s})^{-1}$ for electrons and holes [256]. While spectacularly high values have been reported, the average Hall hole mobility measured in boron doped diamond decreases with increasing doping density and temperature. With boron doping concentrations on the order of $10^{15}\text{--}10^{17} \text{ cm}^{-3}$, simulated hole mobilities are $\sim 2000 \text{ cm}^2 (\text{V}\cdot\text{s})^{-1}$, and experimental values fall between 1000 and $2000 \text{ cm}^2 (\text{V}\cdot\text{s})^{-1}$. From $10^{18}\text{--}10^{20} \text{ cm}^{-3}$, the mobility decreases from 1000 to $30 \text{ cm}^2 (\text{V}\cdot\text{s})^{-1}$ [257]. In n-type diamond, phosphorous doped diamond from $10^{15}\text{--}10^{17} \text{ cm}^{-3}$ is simulated to have mobilities $\sim 1000\text{--}200 \text{ cm}^2 (\text{V}\cdot\text{s})^{-1}$ and decreases to below $30 \text{ cm}^2 (\text{V}\cdot\text{s})^{-1}$ above 10^{18} cm^{-3} [258]. The velocity field curves for electrons and holes were shown to be similar at room temperature [259] with the saturation velocity of electrons and holes to be on the order of $1.4\text{--}2 \times 10^7 \text{ cm s}^{-1}$ at an electric field of 10^5 V cm^{-1} [260, 261].

Moreover, diamond's extremely high TC makes it stand out among other UWBG materials. Due to diamond's strong covalent C-C bonding yielding a bond length of only $1.54 \text{ \AA}$, heat is effectively dissipated through lattice vibrations with low phonon scattering. As a result, diamond has one of the highest thermal conductivities of semiconductors and insulators, $>2200 \text{ W (m}\cdot\text{K)}^{-1}$, which is 5 times greater than even that

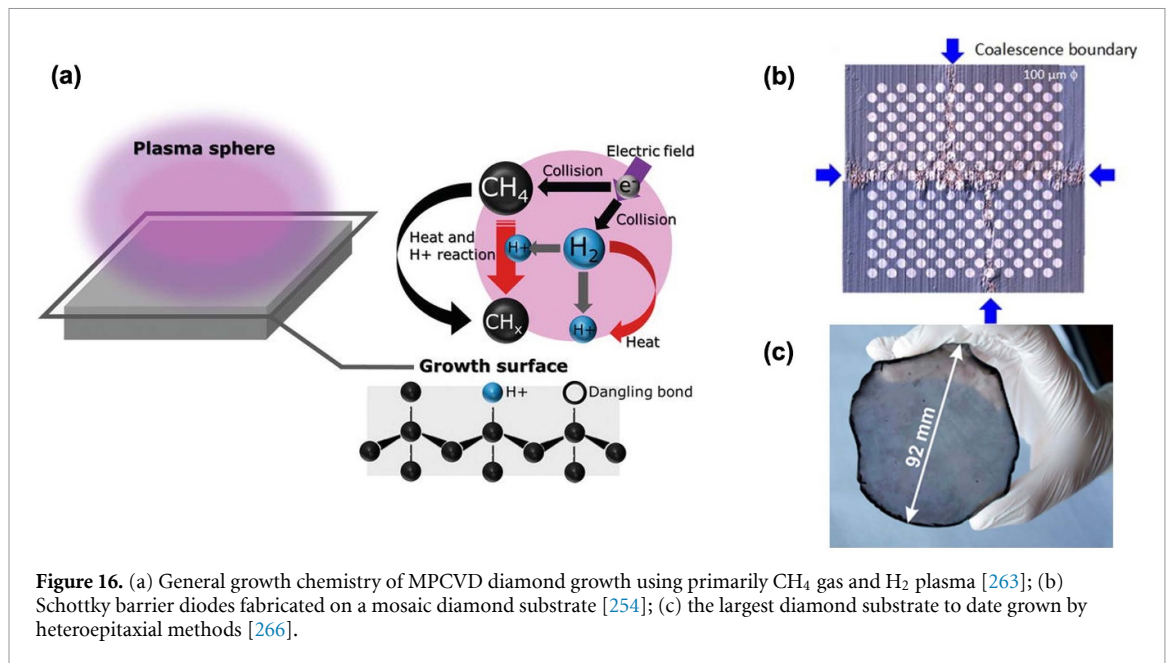


Figure 16. (a) General growth chemistry of MPCVD diamond growth using primarily CH_4 gas and H_2 plasma [263]; (b) Schottky barrier diodes fabricated on a mosaic diamond substrate [254]; (c) the largest diamond substrate to date grown by heteroepitaxial methods [266].

of copper, a common heat sink material. Isotopically enriched (using $^{13}\text{CH}_4$ or $^{12}\text{CH}_4$) diamond has shown thermal conductivities up to $3300 \text{ W (m}\cdot\text{K)}^{-1}$ [262].

4.2. Growth and doping

4.2.1. Single crystalline bulk substrate growth

While the superior properties of diamond make it an attractive candidate for future high power and frequency device platforms, manufacturing large-diameter, high-quality diamond substrate remains a challenge. The high-pressure high-temperature technique can be employed to synthesize low defect density diamond crystals; however, this method is inherently limited to $<1 \text{ cm}^2$ diamond sizes. Alternatively, microwave plasma chemical vapor deposition (MPCVD) methods are prominently used to enlarge seed crystals by outward or lateral growth. Activated atomic hydrogen from the H_2 gas precursor reacts with the hydrogen-terminated surface of a diamond seed to provide a reaction site for carbon radicals to bond to. The $\text{CH}_3^\cdot$ carbon radicals are supplied from CH_4 gas and generated using a plasma or high temperature environment in the chamber [263]. By this chemistry, monolayers of carbon are progressively deposited on the surface, as illustrated in figure 16(a). Unfortunately, this growth process is limited by the formation of PC diamond at the rim which can lead to further stress and cracking of the substrate [264]. Researchers have explored methods to suppress PC diamond formation, such as with modified pocket holders, different diamond seed geometries, and varying growth parameters. These efforts have produced substrates still on the order of 1 cm in diameter [265]. 2 inch substrates were realized by Yamada *et al* (figure 16(b)) by homoepitaxially growing diamond by CVD on a mosaic of smaller clone substrates grown from the same seed crystal, however high defect densities were present at the coalescence boundaries [252]. More recently, Ohmagari *et al* demonstrated the benefit of a W buffering layer in mitigating threading dislocations for mosaic diamond substrates [253] and showed very similar performance to Schottky diodes fabricated on and off the boundaries [254]. Finally, another method to achieve larger area diamond substrates is by heteroepitaxial growth of diamond on materials with readily available substrates. Schreck *et al* demonstrated heteroepitaxial diamond growth on an Ir/YSZ/Si (001) substrate producing a 1.6 mm thick diamond layer with a diameter of 92 mm as pictured in figure 16(c) [266]. The use of negative voltages during the bias-enhanced nucleation process and selection of Ir as the substrate, were key in enabling single-crystalline diamond formation. While the diamond substrates grown in this and other more novel methods have shown immense progress, the quality is certainly still lacking. Thus, continued progress in developing larger-scale diamond growth is critical for the practical widespread adaption of diamond as a semiconductor material.

4.2.2. Doping

In diamond, p-type doping using boron dopants can be readily achieved during bulk MPCVD diamond growth. For boron dopant concentrations up to 10^{18} cm^{-3} , boron has a relatively large activation energy of 0.37 eV, which decreases to $\sim 0.06 \text{ eV}$ when boron concentration exceeds 10^{20} cm^{-3} according to Pearson and Bardeen's model. Furthermore, at concentrations $>10^{19} \text{ cm}^{-3}$, hopping conduction, between ionized

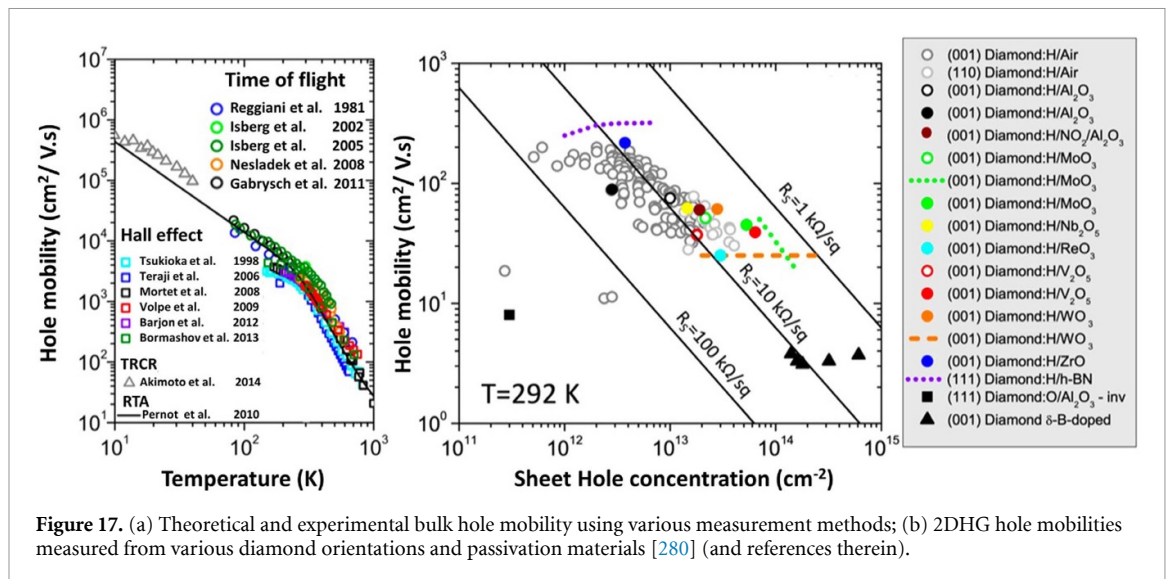


Figure 17. (a) Theoretical and experimental bulk hole mobility using various measurement methods; (b) 2DHG hole mobilities measured from various diamond orientations and passivation materials [280] (and references therein).

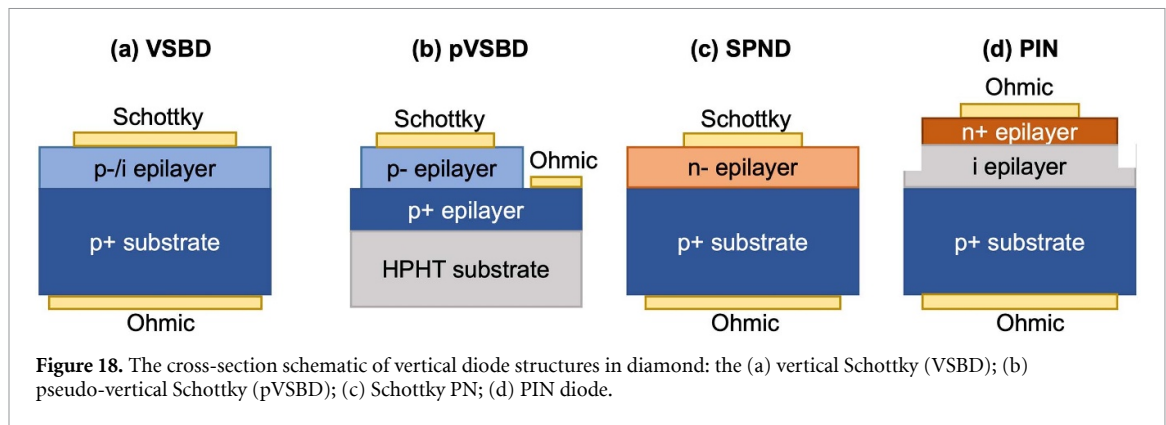
and neutral acceptors, dominates the conduction mechanism [267]. Thus, incomplete ionization and varying conduction mechanisms must be considered when designing devices.

On the other hand, n-type doping in diamond has been more difficult to achieve. Successful phosphorous doping with n-type conductivity was first measured in 1996 by Koizumi *et al* using phosphine as the dopant source during MPCVD growth [268]. Follow up growth optimizations yielded n-type diamond thin films grown on (111) Ib substrates with a maximum mobility of $240\text{ cm}^2 (\text{V}\cdot\text{s})^{-1}$ and an activation energy of $\sim 0.6\text{ eV}$ [269]. Due to the relatively high activation energy, phosphorous is not readily ionized at room temperature, with ionization levels of only 10^{-5} – 10^{-6} [270]. To realize lower resistance n-type diamond, on the order of $70\text{ }\Omega\cdot\text{cm}$, heavy phosphorous doping of diamond $>10^{20}\text{ cm}^{-3}$ is required to lower the activation energy through hopping conduction [271]. On the other side of the spectrum, fine n-type doping control was shown with phosphorous concentrations $<3 \times 10^{17}\text{ cm}^{-3}$. The study reported n-type conductivity of the lowly doped films ($2 \times 10^{15}\text{ cm}^{-3}$) with high RT mobility of $1060\text{ cm}^2 (\text{V}\cdot\text{s})^{-1}$ [272].

While phosphorous is most readily incorporated into substitutional sites in (111) diamond, 2–3 orders higher than in (100), the high defect density formed during growth creates issues in device performance. More recently, the (113) orientation was also found to be a stable plane for phosphorous doped epilayer growth in addition to boron doped. In the study, the homoepitaxial layers reached up to $4.5 \times 10^{19}\text{ cm}^{-3}$ phosphorous content, greater than that of (100) and less than that of (111), proving to be a promising avenue for phosphorous doping in the future [273].

4.2.3. Surface transfer doping by hydrogen termination

While p-type boron doping is accessible in diamond, the high activation energy allows only a small fraction of dopants to ionize, making it difficult to engineer highly conducting channels in devices [274]. It was discovered that when hydrogen-terminated diamond, which has a negative electron affinity, is exposed to air containing atmospheric adsorbates, a two-dimensional hole gas (2DHG) forms near the surface. This p-type surface hole accumulation layer typically has a sheet charge density of 10^{12} – 10^{13} cm^{-2} and hole mobility of 20 – $200\text{ cm}^2 (\text{V}\cdot\text{s})^{-1}$ [274]. In efforts to identify the key molecule responsible for forming the 2DHG, it was found that exposing the diamond to increasing levels of NO_2 led to an increased hole concentration, up to $2.3 \times 10^{14}\text{ cm}^{-2}$, and conductivity [275]. At high temperatures above $300\text{ }^\circ\text{C}$, the 2DHG formed from just atmospheric adsorbates was discovered to be unstable, so researchers employed an Al_2O_3 passivation layer to stabilize the 2DHG at temperatures up to $500\text{ }^\circ\text{C}$ [276]. Since then, other dielectric materials have been studied to passivate H-terminated diamond as well. More recently, transition metal oxides (TMO), particularly MoO_3 [277] and V_2O_5 [278, 279] have shown superior hole carrier concentrations on the order of 10^{14} cm^{-2} . With its high carrier density, the 2DHG has become a pathway for the most prominent diamond transistor, the H-terminated FET. However, an inverse relationship between hole sheet density and mobility has been repeatedly shown (figure 17), and thus a significant increase in conductivity may be limited. Charged surface acceptors and disorder related to the C–H surface dipoles have been proposed as mobility-limiting mechanisms [274], but more research is critical to determine whether the mobility limitations can be overcome to produce higher-performing devices.



4.3. Diamond devices and applications

4.3.1. High power devices

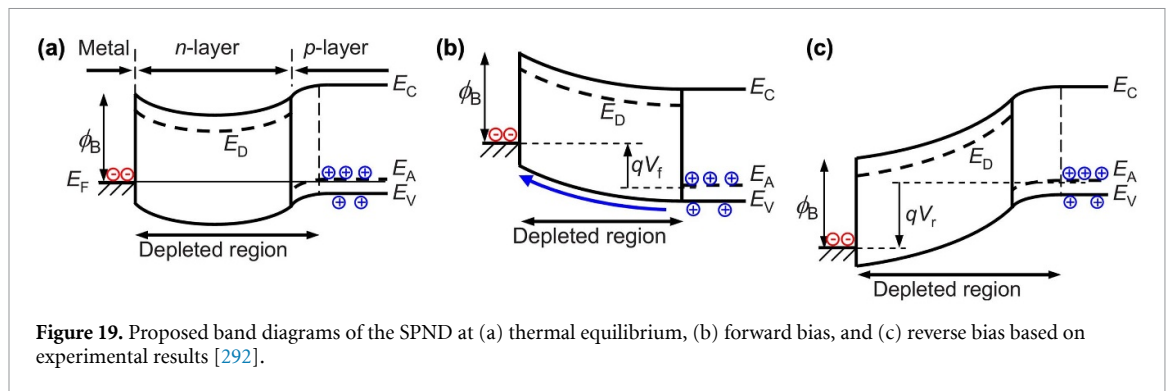
4.3.1.1. Schottky and PN diodes

As diamond lacks a reliable n-type dopant, the p-type SBD is the most mature diamond diode device. Prior to the wider availability of low resistance diamond substrates, pseudo-vertical Schottky diodes were primarily fabricated on doped epilayers with an insulating substrate (figure 18(b)). With the development of highly boron doped substrates, true vertical Schottky diodes are now commonly reported as well (figure 18(a)). The Schottky barrier height can be varied in diamond diodes by utilizing different Schottky contact metals. It was shown that diodes with greater barrier heights can yield lower leakage [281], which comes with a cost of increased on-resistance. Diodes using Schottky contact metals of Al [281, 282], Ni [282, 283], Mo [281], Pt [281], Au [282, 284, 285], Ag [283], WC [286], Zr [287], etc have demonstrated Schottky barrier heights to diamond ranging from <1 to 3.4 eV. Various surface terminations techniques can vary the Schottky barrier height as well. In the case of a hydrogen-terminated diamond surface, the p-type conductivity at the surface must be removed to prevent a leakage path from forming. With oxygen-terminated surfaces, on the other hand, the metal contact becomes rectifying. Thus, increased oxygen termination at the surface was found to increase the Schottky barrier, reduce reverse leakage, and increase breakdown [284, 288, 289]. Diamond surfaces are commonly oxidized by boiling in strong acid mixtures and/or by ultraviolet (UV)/ozone treatment during Schottky diode fabrication [290]. The oxygen content on the diamond may be varied by the wet chemical acids, treatment time, and temperature as well as the ozone concentration and treatment time for UV/ozone [282].

Diamond Schottky diodes have primarily reported breakdown electric fields of <4 MV cm $^{-1}$ even with field termination structures such as field plates. Select works have shown a breakdown field of 7.7 MV cm $^{-1}$, the record in diamond devices. Traoré *et al* reported results measured from pseudo-vertical Schottky diodes with oxidized Zr Schottky contacts that resulted in a record 244 MW cm $^{-2}$ BFOM [287]. Volpe *et al* demonstrated the high breakdown voltage capability of diamond using Au Schottky contacts to a 13.6 μ m p-epilayer (3×10^{16} cm $^{-2}$ boron doped), and set a record breakdown voltage of 10 kV [285]. In recent works, pseudo-vertical Schottky diodes have also been demonstrated on (113) orientated surfaces, with similar performance to that of (100) [291]. The (113) orientation is of interest as it has shown less surface roughness than (111), thus providing better interface qualities while being relatively favorable for both boron and phosphorous doping.

In 2009, Makino *et al* demonstrated an alternative unipolar diode, the Schottky PN diode (SPND). In this configuration, the Schottky metal contacts a lightly phosphorous doped n-type layer on a p+ layer (figure 18(c)) [292]. As a result, the n-type layer is fully depleted in the forward and reverse modes, and the diode conducts like a p-type Schottky diode in the forward bias region, enabling fast switching speeds. In the reverse bias region, the maximum electric field is primarily blocked by the n-region (figure 19). This theoretically enables a more highly doped p-type region, thus increasing the forward current density while maintaining a sufficiently thick space charge region to block high voltages in the reverse region due to the n-type region. Using the SPND structure, a record low on-resistance of 0.03 m Ω ·cm 2 was achieved with a breakdown field of 3.4 MV cm $^{-1}$ and a breakdown voltage of 55 V yielding ~ 100 MW cm $^{-2}$ BFOM [293]. A >1 kV SPIND was later demonstrated by Dutta *et al* [294] and an ultrahigh forward current density on the order of 10^5 A cm $^{-2}$ by Surdi *et al* [295], showing the overall potential of the SPIND for high power applications.

Furthermore, high temperature measurements in Schottky diodes have been measured up to 1000 °C and showed a rectification ratio of up to 10^4 at 600 °C [283, 288]. As the temperature increases, the forward



current density increases as the result of boron dopant ionization, which overtakes the decrease in mobility [283, 288, 296]. In high temperature measurements, it is also generally observed that an increase in Schottky barrier height and decrease in ideality factor occurs, indicating barrier inhomogeneity. This has been reported in other WBG materials as well [286], and further supported by conductive AFM measurements which showed that a very small fraction of the contact was active in the lower voltage range of the forward bias region [296].

Due to the challenge of n-type doping, PN diodes are relatively underdeveloped. Several studies have demonstrated PN diodes, with a focus on UV light emission indicating bipolar transport; however, the electronic performance is lacking. Due to the high resistivity of n-type diamond, the on-state current density remains limited, with 140 A cm^{-2} as the highest reported, while a reverse blocking voltage up to 920 V [297] and breakdown field of 3.9 MV cm^{-1} [294] have been achieved.

The current breakdown field values are still far from theoretical predictions in diamond, so efforts to reduce reverse leakage current and premature breakdown are highly relevant. The reverse bias leakage current in Schottky diamond diodes has been fit to the thermionic emission model with image-force lowering at lower fields, and the thermionic field emission model at fields $>1 \text{ MV cm}^{-1}$ [286, 298]. While this observation has been common in other wide-bandgap semiconductors as well, another prominent source of leakage is the presence of defects formed during growth, which can affect any type of device. These include non-epitaxial crystallites, which have been characterized as killer defects [298], and crystallographic defects like threading dislocations. In a study of PIN diodes, the reverse bias current characteristics, analyzed up to 150°C , were attributed to hopping conduction and Poole–Frenkel emission through threading dislocations [299]. Furthermore, it was found that as the drift layer increases in thickness, the breakdown field does not proportionally increase in most cases, which indicates poorer epitaxial quality with thicker drift layer growth [300]. While the reduction of defects requires improvement in growth techniques, a common cause for reverse breakdown and increased leakage is field enhancement at the edge of the electrode, a common issue in other materials as well. In response, field-plated Schottky diodes with sputtered Al_2O_3 were studied and found to increase the breakdown voltage appreciably by more than 2 times, from $0.6\text{--}0.8$ to $1.6\text{--}2.0 \text{ MV cm}^{-1}$ [301, 302]. While the impact of the field plate has been experimentally shown, more recent studies have not reported similarly effective field plates. Other edge termination structures such as ramped field plates, junction termination, etc have yet to be successfully demonstrated in diamond due to fabrication limitations such as selective doping. Thus, in diamond two-terminal devices, there is still significant room for optimization, improved performance, and reliability studies, which should naturally follow the development of improved growth and doping techniques.

4.3.1.2. MESFETs and MOSFETs

In oxygen terminated diamond, FETs can be fabricated which rely on bulk conduction in the channel as illustrated in figures 20(a)–(c). Due to the large Schottky barrier heights achievable in diamond on oxygen-terminated diamond, MESFETs have been studied with relatively low gate leakage. Umezawa *et al* demonstrated diamond Pt-gated MESFETs with increasing breakdown voltages from 693 V to 1530 V as gate-to-drain distance was increased from 5 to $30 \mu\text{m}$ [303]. The less-than-ideal breakdown field, approximately 2.15 MV cm^{-1} , can be attributed to electric field spiking at the drain-side edge of the gate electrode. Another FET structure that has been demonstrated is the deep depletion mode MOSFET by Pham *et al* [304, 305]. The structure utilizes an Al_2O_3 dielectric and has achieved a high hole mobility in the conducting channel of $1000 \pm 200 \text{ cm}^2 (\text{V}\cdot\text{s})^{-1}$. This structure has the potential to take advantage of bulk hole mobility while limiting gate leakage which is typically higher in MESFETs.

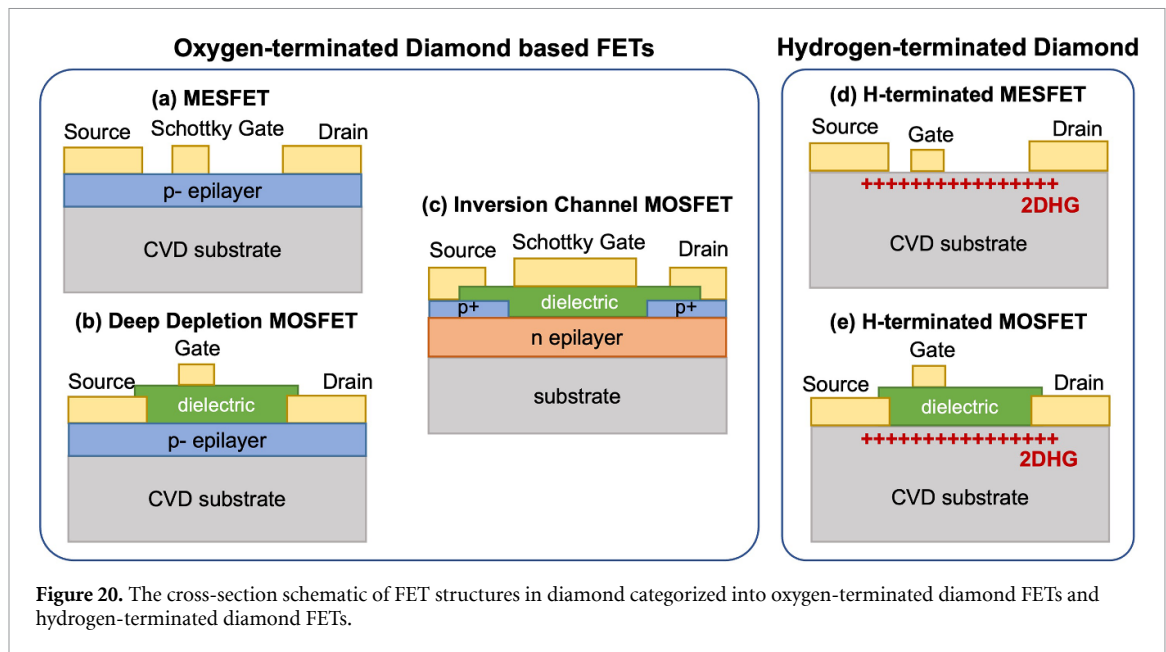


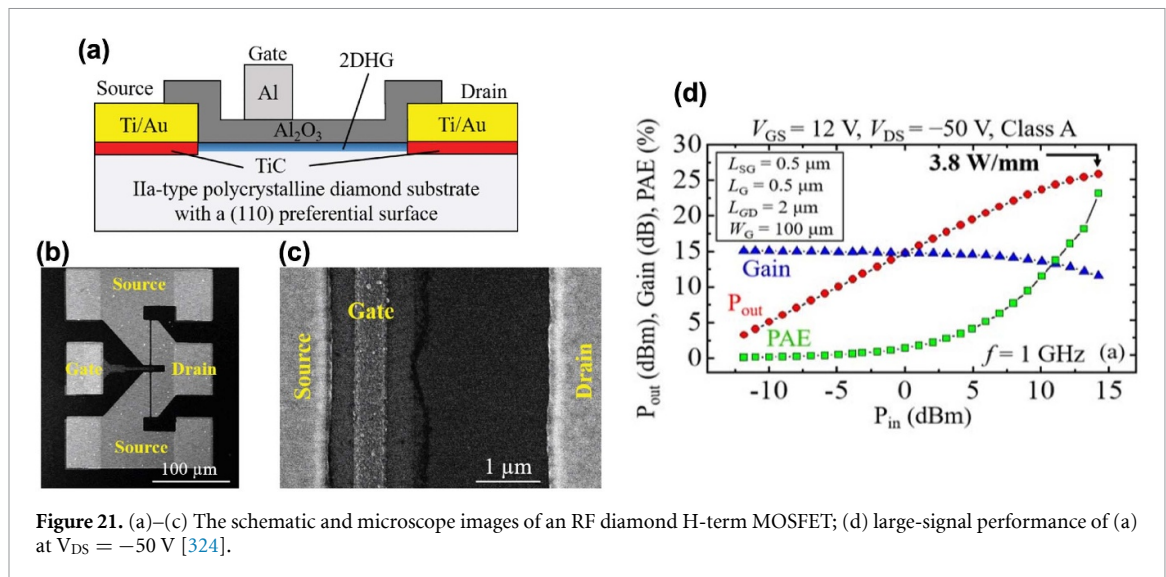
Figure 20. The cross-section schematic of FET structures in diamond categorized into oxygen-terminated diamond FETs and hydrogen-terminated diamond FETs.

While more difficult to achieve due to the challenge of n-type doping and the WBG of diamond, classic inversion channel MOSFETs have been shown due to improvements made in phosphorous doping. Such devices have advantages in gate controllability and threshold voltage tunability [306]. In 2016, Matsumoto *et al* reported the first inversion p-channel diamond MOSFET with normally-off characteristics utilizing a phosphorous-doped n-type body grown on a (111) substrate. A high-quality interface by wet annealing was formed between the Al_2O_3 gate oxide and O-terminated n-type diamond. The devices with a gate length of $5\ \mu\text{m}$ delivered a maximum drain current density of $1.6\ \text{mA mm}^{-1}$, an on/off ratio $>10^{10}$, and a field-effect mobility of $8.0\ \text{cm}^2 (\text{V}\cdot\text{s})^{-1}$. The low mobility was attributed to high interface defect density, which can be reduced by achieving flatter surfaces [306]. Further studies showed that decreased phosphorous doping density ($2 \times 10^{15}\ \text{cm}^{-3}$) resulted in greater smoothness and lower interface defect density, and as a result, higher mobility, up to $20\ \text{cm}^2 (\text{V}\cdot\text{s})^{-1}$ and higher drain current density [307]. Thus, the interface state density between the n-type diamond and the oxide must be further studied and reduced to improve the performance of inversion channel MOSFETs. More recently they also demonstrated an inversion p-channel MOSFET on nitrogen doped diamond, which is much easier to dope albeit has a much larger activation energy, 1.7 eV. Nonetheless, the MOSFET exhibited a drain current density very similar to that of MOSFETs fabricated using a phosphorus n-type diamond body [308].

Hydrogen-terminated (H-term) FETs are the most studied diamond transistor, in which the surface 2DHG formed by hydrogen termination of single-crystalline (SC) or PC diamond generates a conductive channel with a high density of hole carriers (figures 20(d) and (e)). In an H-term MESFET, a Schottky contact, commonly Al, is directly deposited on the diamond as the gate metal. In a MOSFET, Al_2O_3 is often used as the gate oxide since it preserves the 2DHG and stabilizes it for high temperature operation. A NO_2 -enhanced H-term MOSFET showed the highest reported breakdown voltage to date, 2.6 kV at a field of $2\ \text{MV cm}^{-1}$ [309]. The highest drain current density is reported to be $1.35\ \text{A mm}^{-1}$ using NO_2 exposure to increase hole density and Al_2O_3 passivation [310].

Because the 2DHG consists of surface charges formed by hydrogen termination, it is very sensitive to the surface and interface quality. H-term FETs may be depletion or enhancement mode devices based on the surface treatment of diamond and interface defects. To form enhancement mode devices, several strategies have been employed such as selecting low work function gate material [311], partially oxidizing the H-diamond surface [312, 313], and choosing gate oxides with different deposition methods [314–316]. The highest current density for enhancement mode devices, $400\ \text{mA mm}^{-1}$, was recently reported by Zhu *et al* using PC diamond MOSFETs with a heavily boron-doped layer as the source/drain region [315].

While Al_2O_3 is the most popular dielectric used, many others have been studied as well such as HfO_2 and h-BN [314]. Exfoliated single crystalline h-BN is known to have a very flat surface with few charged impurities and no dangling bonds. Thus, it has the potential to form a high-quality interface with diamond. Recently, Sasama *et al* used a h-BN gate insulator which resulted in a $>300\ \text{cm}^2 (\text{V}\cdot\text{s})^{-1}$ channel mobility device [317]. The high mobility was attributed to the low density of defects in h-BN, and follow-up studies



were able to further enhance the mobility to $680 \text{ cm}^2 (\text{V}\cdot\text{s})^{-1}$ by eliminating air exposure between the hydrogen termination and h-BN lamination steps during fabrication [318].

4.3.2. RF hydrogen terminated FETs

Around 2001, researchers first began to report on the high-frequency performance of H-term FETs; however, high-frequency devices in diamond are still very much in the early stages of development. A series of studies from Kasu *et al* culminated in a device (gate length = $0.1 \mu\text{m}$, width = $100 \mu\text{m}$) yielding 2.1 W mm^{-1} output power density [319]. This relatively high value in diamond was attributed to the high-purity gas used during homoepitaxial layer growth. Later, the group demonstrated a MESFET (gate length = $0.4 \mu\text{m}$, width = 1 mm) with a record 23.2 dB maximum power gain and 56.3% PAE [320] measured at 1 GHz and drain-to-source voltage (V_{DS}) = -20 V. Published in the mid-2000s, these RF measurement values remain difficult to surpass. While SC diamond is typically preferred for more ideal electronic properties, PC diamond is much more accessible, offering lower costs and larger diameters, and is also actively studied for fabricating H-term FETs. MESFETs fabricated on preferentially (110) oriented PC diamond by Ueda *et al* demonstrated a high f_T of 45 GHz and f_{max} of 120 GHz and leakage was not observed in the large grain ($100 \mu\text{m}$) PC diamond substrate [321].

In 2007, Hirama *et al* measured the RF characteristics of H-term MOSFETs on SC and PC diamond using an alumina gate insulator for the first time [322]. The gate oxide was formed by the oxidation of 3 nm thick Al. The (001) homoepitaxial devices demonstrated a similar output power density to that of Kasu *et al*, with 2.14 W mm^{-1} at 1 GHz. Furthermore, the PC (110) devices yielded higher current density and 1.5 times the f_T than the SC (001) devices. This was attributed to the differing orientations rather than the PC and SC nature of the substrates. Previous reports have shown that H-terminated (110) diamond resulted in higher C–H bond density and thus higher hole densities in the 2DHG.

In recent studies, Yu *et al* reported the highest f_T/f_{max} in diamond MOSFETs of 70/80 GHz, which was attributed to continued scaling of the source-drain distance and thin 6 nm gate oxide [323]. Then in 2019, Imanishi *et al* demonstrated the highest power density at 1 GHz to date, 3.8 W mm^{-1} in a MOSFET diamond device with 100 nm ALD Al_2O_3 on a (110) preferential PC diamond substrate (figure 21) [324]. In 2022, the highest RF power densities were measured at 2, 4, and 10 GHz to date: 4.2, 3.1, and 1.7 W mm^{-1} , respectively, on homoepitaxial (001) single crystalline diamond substrates with 100 nm Al_2O_3 [325]. In both these studies, V_{DS} was pushed to greater than 40 V, which contributed to the record power densities measured in diamond.

4.3.3. Heterogeneous integration of diamond for device-level thermal management

The efficiency and reliability of power and RF devices are not only limited by the electronic properties of the material but also by their thermal management [326], as mentioned in section 2.3.2.1. At the device level, Joule heating occurs in the channel due to increased power density and switching speeds. As a result, device performance can suffer from high temperatures which can eventually result in premature failure. While developing diamond-based devices can be a solution due to diamond's excellent thermal and electronic properties, enormous research efforts and progress are still needed to achieve high-performance devices. On the other hand, heterogeneous integration of diamond can serve as a heat spreader solution for more mature

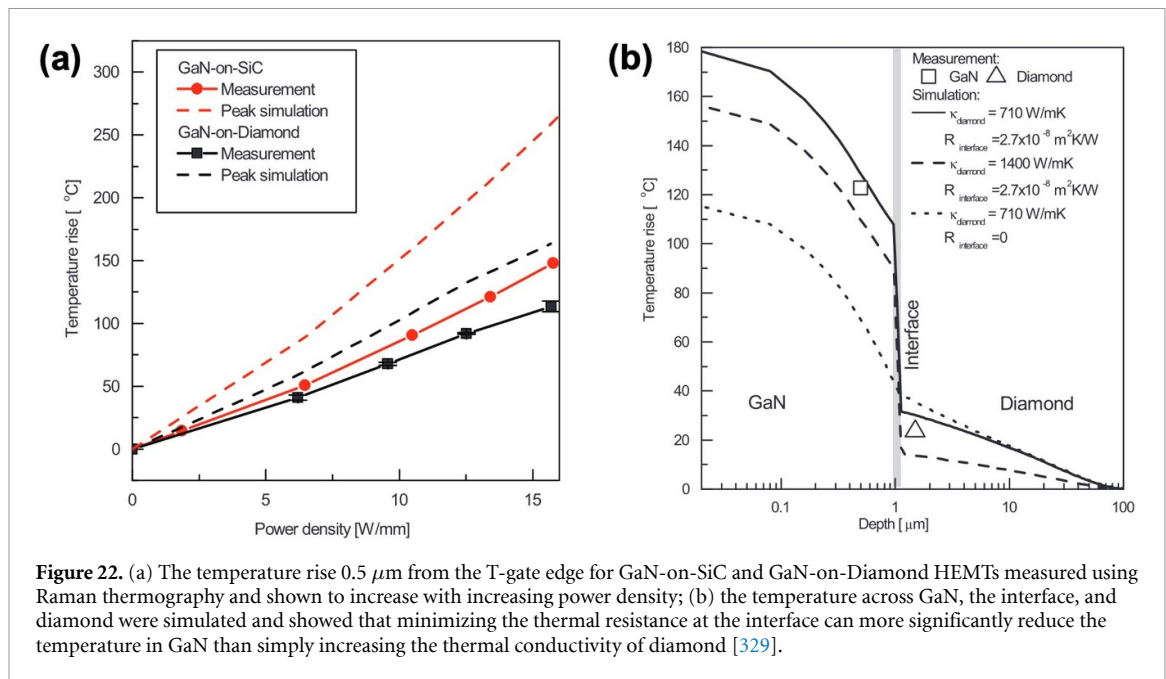


Figure 22. (a) The temperature rise $0.5 \mu\text{m}$ from the T-gate edge for GaN-on-SiC and GaN-on-Diamond HEMTs measured using Raman thermography and shown to increase with increasing power density; (b) the temperature across GaN, the interface, and diamond were simulated and showed that minimizing the thermal resistance at the interface can more significantly reduce the temperature in GaN than simply increasing the thermal conductivity of diamond [329].

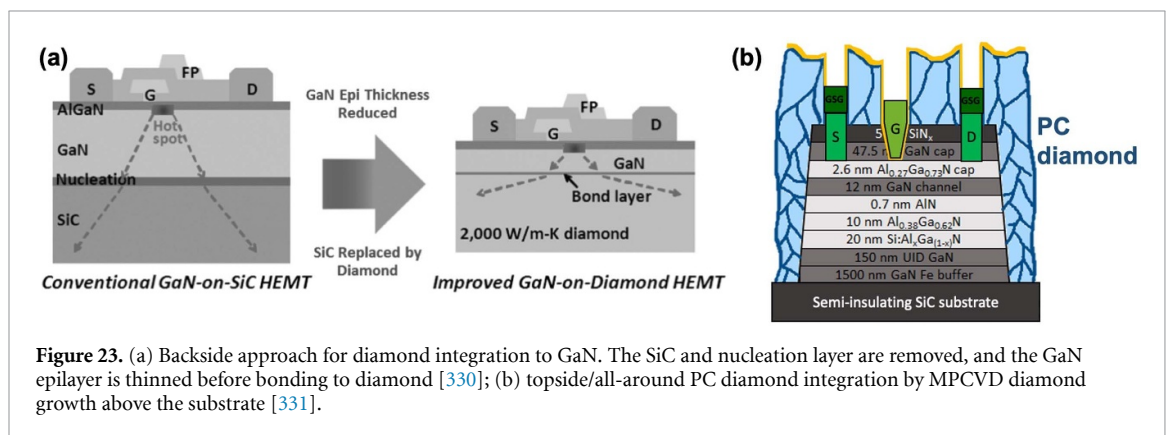


Figure 23. (a) Backside approach for diamond integration to GaN. The SiC and nucleation layer are removed, and the GaN epilayer is thinned before bonding to diamond [330]; (b) topside/all-around PC diamond integration by MPCVD diamond growth above the substrate [331].

material technologies like GaN as well as other emerging UWBG materials such as Ga_2O_3 and AlGaIn which have inferior thermal properties [327, 328]. GaN technology, more specifically AlGaIn/GaN HEMTs at its current stage, has already penetrated the high-frequency, high-power device market for power amplifiers. Thus, there is particularly high interest in device-level cooling for these structures to enhance their power output. Due to silicon carbide's relatively high TC, GaN-on-SiC technology is customarily used for power RF devices. As diamond possesses a significantly higher TC, Pomeroy *et al* demonstrated that GaN-on-diamond could yield a 40% decrease in peak channel temperature in comparison to GaN-on-SiC AlGaIn/GaN HEMTs based on a combination of Raman thermography measurements and thermal modeling (figure 22) [329]. To implement such a diamond-based thermal management strategy, there are two primary approaches as illustrated in figure 23: backside diamond substrate bonding and PC CVD heteroepitaxial diamond growth.

Several works have shown the feasibility of GaN to diamond bonding at lower annealing temperatures of 150°C – 180°C using 15–40 nm thick undisclosed/Si-based adhesion interlayers [330, 332]. However, the thermal boundary resistance (TBR) of the GaN/diamond interface including the adhesion layer can become a dominating source of thermal resistance as displayed in figure 22(b) [329]. To take full advantage of a diamond heat spreader, a low diamond to substrate TBR is required in addition to a high diamond TC. More recently, the process of surface-activated bonding (SAB) at room temperature under high vacuum was developed (figure 24) [333]. Using this technique resulted in a relatively low GaN/diamond interface TBR of $\sim 11 \text{ m}^2\text{K} (\text{GW})^{-1}$ with a 4 nm bonding sputtered Si bonding layer [334]. While this method requires a specialized tool, a more recent study has established a low temperature, easy-access method in which no pre-deposited interlayer is needed [335]. In this process, a GaN substrate first underwent HCl chemical treatment and the diamond $\text{NH}_4\text{OH}/\text{H}_2\text{O}_2$ treatment. Then, a 2 h, 200°C , 1 MPa bonding was sufficient to

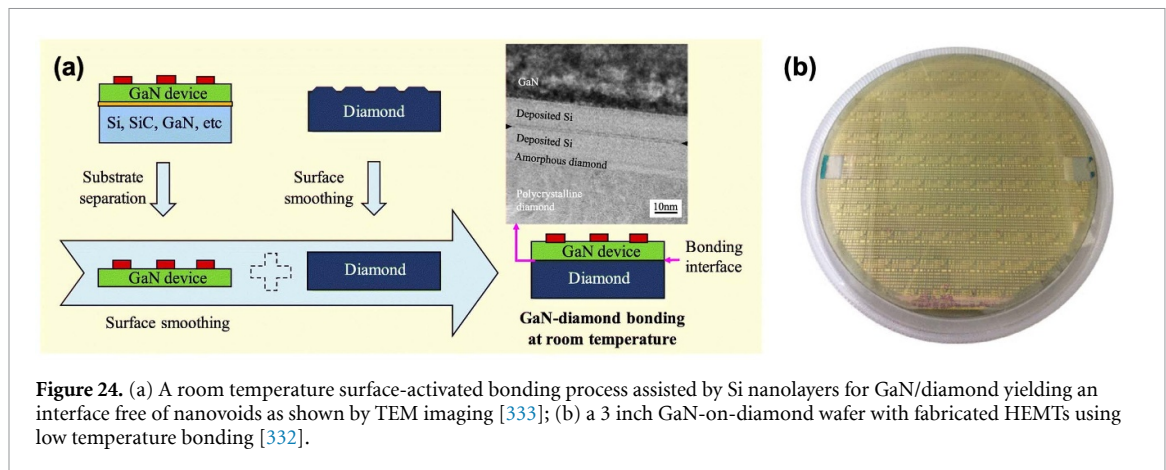


Figure 24. (a) A room temperature surface-activated bonding process assisted by Si nanolayers for GaN/diamond yielding an interface free of nanovoids as shown by TEM imaging [333]; (b) a 3 inch GaN-on-diamond wafer with fabricated HEMTs using low temperature bonding [332].

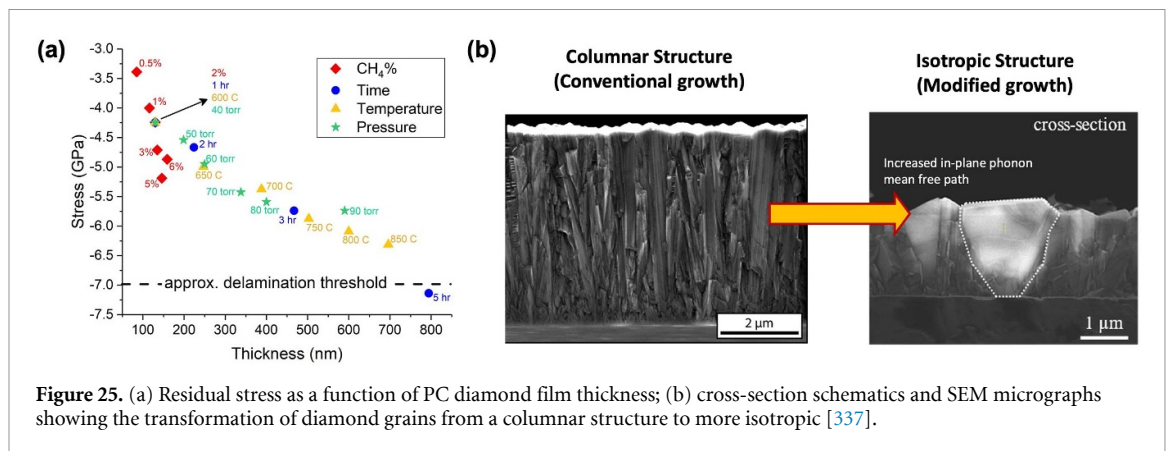


Figure 25. (a) Residual stress as a function of PC diamond film thickness; (b) cross-section schematics and SEM micrographs showing the transformation of diamond grains from a columnar structure to more isotropic [337].

bond the two materials. TEM images showed the formation of a 3 nm amorphous layer, which was predicted to produce a low TBR due to its thinness, although it has not been measured.

In addition to studying diamond thermal management from a material perspective, diamond heat spreading technology must also demonstrate integration without degradation of the device, show an operational temperature decrease, and ultimately enhance device performance and reliability. Using low temperature bonding methods to PC diamond substrates, several groups have shown device-first transfer technology of GaN HEMTs. Chao *et al* maintained a high-performance HEMT with a maximum output power density of 11.0 W mm^{-1} at 10 GHz and a PAE of 51% following the transfer to diamond [330]. Furthermore, IR imaging showed three times higher dissipated power in the same active area of a GaN-on-diamond HEMT in comparison to that of GaN-on-SiC. Liu *et al* later successfully demonstrated 3 inch GaN-on-diamond HEMTs with >80% yield and measured a 50°C decrease in peak channel temperature (from 241°C to 191°C) at 10 W mm^{-1} [332]. With these promising device-level results, similar studies must continue as advancements in the thermal properties of diamond heat spreader technology are made.

Alternatively, a topside PC diamond heat spreader can be advantageous since the diamond can be integrated closer to the channel and more effectively transfer heat away from the channel hot spot. Furthermore, it has increased potential for scalability since it is not limited by the diamond substrate size. To implement this approach, heterogeneous epitaxial growth of diamond must be well-understood. First, to nucleate diamond grains on foreign substrates, a seeding process using diamond nanoparticles is performed. After, the seeded substrate is placed in a hot filament or MPCVD chamber for growth at 400°C – 1000°C , relying on the same chemistry as that of substrate growth described in section 4.2.1. An important parameter when growing diamond on a foreign substrate is the residual stress due to a coefficient of thermal expansion (CTE) mismatch between the two materials [336]. Since diamond has a very low CTE of $\sim 1.1 \times 10^{-6} \text{ K}^{-1}$, it typically contracts less than the substrate while cooling down from growth temperatures, causing compressive stress to form in diamond. The magnitude of stress increases with growth thickness (figure 25(a)), eventually causing the diamond to delaminate from the substrate [337]. This limits the thickness of PC diamond that can be grown on foreign substrates.

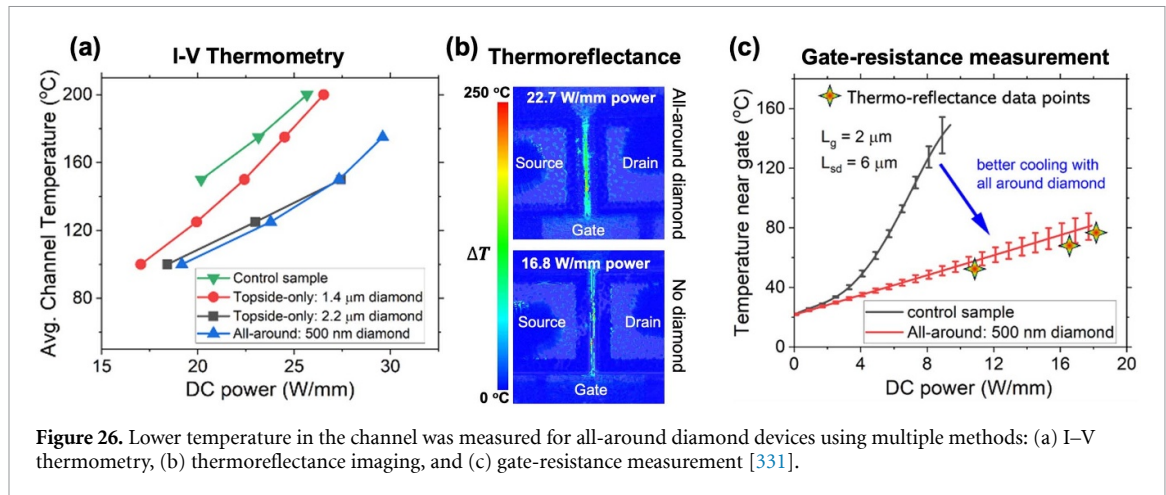


Figure 26. Lower temperature in the channel was measured for all-around diamond devices using multiple methods: (a) I–V thermometry, (b) thermoreflectance imaging, and (c) gate-resistance measurement [331].

Depending on the growth parameters (e.g. gas pressure, plasma power, surface temperature, CH₄%, etc), seeds may grow in the vertical and lateral directions at different rates. Figure 25(b) shows how the change in the growth parameters can transform the columnar structure into a more-isotropic structure [338]. Because one primary drawback of heteroepitaxial PC diamond growth on GaN is the reduced TC in comparison to SC diamond, the formation of large, isotropic diamond grains is crucial. Developing more isotropic growth enhances in-plane phonon transport by reducing scattering sites at the grain boundaries, thus increasing the effective TC and overall capability for device cooling. For example, the more isotropic diamond grains grown by Malakoutian *et al* compared to others resulted in a relatively higher TC of $\sim 648 \text{ W m}^{-1} \text{ K}^{-1}$ for a 2 μm thick epilayer [338]. Furthermore, there are tremendous efforts in reducing heteroepitaxial diamond-on-GaN TBR for the same reasons highlighted earlier in this section. Zhou *et al* and Yates *et al* showed that using a SiN_x interlayer between diamond and GaN produced an average TBR of $6.5\text{--}9.5 \text{ m}^2 \text{ K (GW)}^{-1}$, while using an AlN interlayer averaged $15.9\text{--}18.2 \text{ m}^2 \text{ K (GW)}^{-1}$ [339, 340]. In another work, Malakoutian *et al*, reported the lowest measured TBR between diamond and GaN $\sim 3.1 \text{ m}^2 \text{ K (GW)}^{-1}$ by using a 1 nm SiN_x interlayer [338], indicating that the heat transfer will not be hindered significantly at the interface.

Because typical diamond growth takes place under high temperatures (HT), between 600 °C and 1000 °C, diamond integration with many semiconductor technologies will inevitably damage the device or substrate material. As a result, there have been many efforts to reduce the growth temperature for compatibility with low thermal budget materials and processes. Low temperature (LT) diamond growth has been reported in a temperature range from 100 °C to 500 °C. The growth of a high-quality PC diamond at back end of line compatible temperature, 400 °C, was achieved by modifying the gas chemistry at different nucleation stages. A sharp sp³ Raman peak (full width at half maximum $\approx 6.5 \text{ cm}^{-1}$) and high phase purity (97.1%), like that of HT-diamond (>98%) were measured in the near-isotropic PC diamond [341]. Furthermore, the LT diamond exhibited a relatively high in-plane and cross-plane TC of $\sim 300 \text{ W (m·K)}^{-1}$, and a TBR as small as $5 \text{ m}^2 \text{ K (GW)}^{-1}$. The results of these studies highlight the feasibility of diamond integration with various semiconductor technologies and open a path for heat spreading solutions for practical adoption.

By using the LT diamond growth technique, Soman *et al* demonstrated the cooling effect of an integrated all-around PC diamond structure on the topside of a GaN HEMT. The thermal resistance between the device's active region and heat sink was reduced using PC diamond integration, ultimately resulting in a channel temperature decrease of $>70 \text{ °C}$ at 25 W mm^{-1} power operation shown using I–V thermometry [331]. The thermal benefits were further confirmed using thermoreflectance and gate-resistance measurement techniques illustrated in figure 26. As the inefficiency due to heating is a universal problem in electronics, particularly in high-frequency and high-power switching, continued research in diamond integration for thermal mitigation has the potential to highly impact the field.

Among the emerging UWBG semiconductors, $\beta\text{-Ga}_2\text{O}_3$, discussed later in section 5, has already demonstrated great potential for power device technologies while offering a low-cost method for large-diameter wafer growth. Nonetheless, a notable drawback of this material is its markedly low, anisotropic TC ranging from 11 to $27 \text{ W m}^{-1} \text{ K}^{-1}$. As a result, there is particularly high interest in employing diamond as a heat spreader for Ga₂O₃. A few key studies have been published that parallel the integration approaches undertaken in GaN. Low-temperature bonding of Ga₂O₃ and diamond was achieved by Matsumae *et al* by first OH terminating both diamond and Ga₂O₃ using H₂SO₄/H₂O₂ and oxygen plasma irradiation, respectively. The contacted materials were then annealed at 250 °C for hydrophilic bonding to

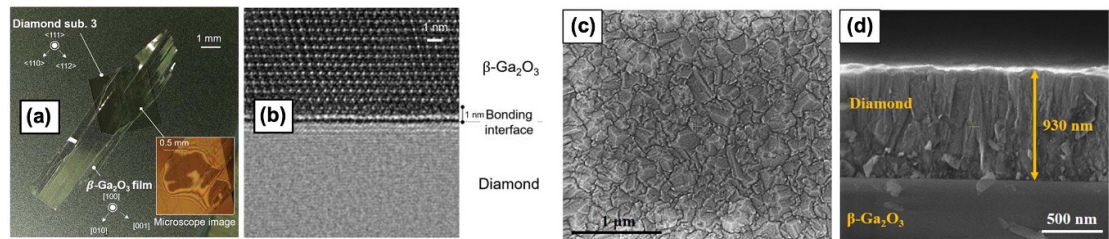


Figure 27. (a), (b) Exfoliated 10 μm $\beta\text{-Ga}_2\text{O}_3$ bonded to diamond and the TEM image of its interface [342]; (c), (d) MPCVD-grown diamond on a 100 nm SiO_2 interlayer on $\beta\text{-Ga}_2\text{O}_3$, yielding an average grain size of 400 nm [327].

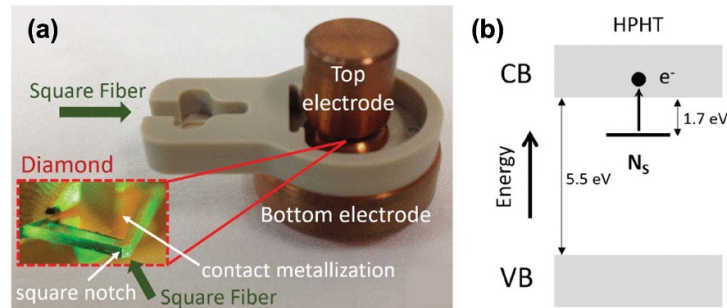


Figure 28. (a) A vertical extrinsic diamond PCSS excited by 532 nm light; (b) the band diagram representation of the mechanism by which electrons are excited from the nitrogen deep donor level in diamond to the conduction band in response to 532 nm light [349].

take place (figures 27(a) and (b)) [342]. Additionally, PC diamond heteroepitaxial growth on $\beta\text{-Ga}_2\text{O}_3$ substrates was shown using a relatively thick SiO_2 protective interlayer that prevented substrate damage and enabled uniform diamond nucleation [327, 343]. As illustrated in figures 27(c) and (d), at lower magnifications, the diamond-on- Ga_2O_3 film exhibits remarkable uniformity, and at high magnification SEMs, dense PC diamond was observed [327]. These results mark a significant step towards device-level thermal management for $\beta\text{-Ga}_2\text{O}_3$.

4.3.4. Photoconductive semiconductor switching

Photoconductive semiconductor switches (PCSS) are optically controlled electronic devices that are desired for their high voltage, high speed, and jitter-free operation [344]. This is achieved by modulating the conductivity of a semiconductor substrate with a light energy source. These devices are especially effective in pulsed power technology, such as radar, particle acceleration, and pulsed high-power lasers. Furthermore, as there are increased efforts toward electrification, developing safer mechanisms for making and breaking high power circuits is a priority. By decoupling the trigger from the circuit with an optical source, the chances of false triggering are reduced and more simple and resilient circuits can be enabled [345]. One of the main issues of photoconductive switches is their short lifespan resulting from voltage and current overloads as well as thermal runaway effects at high-power levels [344]. The use of diamond and other UWBG semiconductors to fabricate PCSS devices could mitigate some of these issues owing to their superior material properties.

Past studies have shown photoconductivity in intrinsic diamond by UV-band excimers in high electric fields up to 0.7 MV cm^{-1} , $>10 \text{ kV}$ conditions, and with picosecond to nanosecond response times [346–348]. In contrast to intrinsic PCSSs, which depend on high photon energies above the bandgap (band-to-band excitation), extrinsic PCSS operates with below bandgap photon energies due to the excitation of carriers from dopants and defect levels as illustrated in figure 28(b). This enables PCSS functionality with more accessible sub-bandgap excitation sources in the visible or infrared range while maintaining the desirable properties of diamond. Nitrogen-doped diamond-based PCSSs have shown nanosecond pulsed responses to 532 nm light by exciting an electron from the deep defect level (1.7–2.0 eV) of nitrogen into the conduction band [345, 349]. Since diamond's nitrogen dopants are largely inactivated at room temperature, making ohmic contacts is challenging for PCSS devices. However, Woo *et al* showed that the contact resistivity is reduced when the electrodes are under illumination which enabled a high $I_{\text{on}}/I_{\text{off}}$ ratio ($>10^{11}$ at 33 kV cm^{-1} in response to 0.8 mJ, 10 ns pulsed, 532 nm light). The responsivity of nitrogen-doped diamond to 532 nm light was found to be less than that of diamond UV light, but

comparable to the responsivity of SiC and GaN extrinsic PCSSs [349]. On the other hand, boron doped diamond was found to be responsive to both 532 and 1064 nm light due to its lower activation energy (0.37 eV). While its large off-state conductivity renders it a poor candidate as a switch on its own [345], photoexcitation of boron dopants may still lend itself to other optically triggered electronic devices. Further studies to increase the quantum efficiency of the PCSS and explore the use of other defect states will greatly contribute to the practicality of light-triggered devices in diamond.

5. Beta-gallium oxide (β -Ga₂O₃)

5.1. Material properties

Five types of Ga₂O₃ polymorphs were reported in 1952, denoted as α , β , γ , δ , and ε , respectively. However, recent high-resolution structural characterizations revealed that a transient κ -phase polymorph could form an ordered subgroup in the ε -phase, and an ε/κ phase could coexist instead of a pure-phase Ga₂O₃ polymorph [350, 351]. Among all the five polymorphs, β -Ga₂O₃ is the only thermodynamically stable phase and therefore, the most extensively studied. In this review, the discussions will only focus on the material properties and device applications of β -Ga₂O₃.

The most attractive merit of β -Ga₂O₃ is its high critical field due to its large bandgap of 4.9 eV. Based on the empirical relationship between the critical field and the material's bandgap, a critical field as high as 8 MV cm⁻¹ was predicted for β -Ga₂O₃ theoretically [3, 352]. However, almost all the experimental results demonstrated a premature destructive breakdown for β -Ga₂O₃ devices due to the field crowding at the edge of the gate dielectric or the anode electrode. The highest average critical field reported was around 6 MV cm⁻¹ in vertical SBDs [353, 354], and no avalanche was reliably observed in a β -Ga₂O₃ device.

The electron mobility at room temperature for the doping range of 10¹⁵–10¹⁶ cm⁻³ is reported to be around 150–200 cm² (V·s)⁻¹ [355–357], and is mainly limited by the longitudinal optical phonons in the β -Ga₂O₃ [358]. The saturation velocity of electrons in β -Ga₂O₃ was calculated to be around 1–2 × 10⁷ cm s⁻¹ [359], which is sufficient for many high-frequency applications. Unfortunately, due to the flat valence band maximum in β -Ga₂O₃, leading to a heavy hole effective mass, the mobility of holes is expected to be very low and nearly no measured values have been reported.

Another one of the main drawbacks of β -Ga₂O₃ is its low TC, posing another challenge for its high-power applications. The extracted TC of β -Ga₂O₃ is 0.27 W (m·K)⁻¹ along the [010] direction and 0.11 W (m·K)⁻¹ along the [99] direction [360]. Since these values are only 1/10 of the values for SiC and GaN, more efficient thermal management for Ga₂O₃ devices is demanded.

5.2. Growth and doping

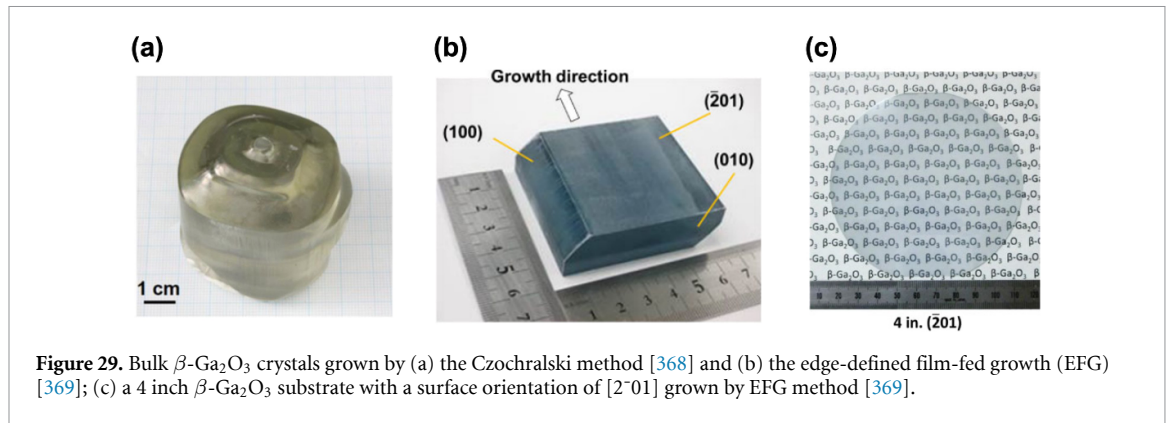
5.2.1. Bulk substrate growth

One of the distinctive features of β -Ga₂O₃ among U/WBG materials is that its native substrates can be grown via the melt growth method. Consequently, mass production of β -Ga₂O₃ substrates with large wafer sizes, high structural quality, and low manufacturing costs is more feasible. The β -Ga₂O₃ substrates can be grown from various melt growth methods: float zone [361–363], Czochralski [364, 365], vertical Bridgman, and edge-defined film-fed growth (EFG) [366], pictured in figure 29. Among these methods, the EFG growth method shows great potential in offering large-diameter β -Ga₂O₃ substrates. 4 inch single-crystalline β -Ga₂O₃ substrates have been successfully grown via the EFG method with a low dislocation density of 10³–10⁴ cm⁻² and a surface roughness of 0.1 nm [367]. To date, 2 inch β -Ga₂O₃ substrates are commercially available to the public.

5.2.2. Epitaxial layer growth

Like other compound materials in this review, several familiar techniques: MBE, HVPE, and MOCVD are often used for the epitaxial growth of Ga₂O₃. MBE, which can offer high-purity growth with precise control of thickness, has been the most commonly used technique for thin film Ga₂O₃ growth at the beginning of its research and development [370–372]. The growth typically occurs by oxidizing the supplied Ga atoms using ozone or oxygen radicals [373, 374]. Intentional dopants, such as Si, Sn, and Ge can be incorporated during MBE growth. However, it is difficult to achieve a doping density on the order of 10¹⁶ cm⁻³ or less due to the oxidization of the dopant source by background O species during the growth [375].

HVPE growth of Ga₂O₃ was demonstrated in 2014 by using GaCl and O₂ as precursors [376]. Like HVPE growth of GaN, the GaCl is formed by the reaction of gallium metal source and Cl₂ gas at 850 °C in a source zone first and then transported to the growth zone and reacted with O₂. Here, SiCl₄ is commonly used as an n-type dopant source. The growth rate of HVPE can reach up to 20 μm per hour without degrading the film



quality. A low unintentional doping of 10^{13} cm^{-3} has been achieved by HVPE growth and intentional doping density in the range of 10^{15} – 10^{19} cm^{-3} can be accurately controlled by adjusting the flow of SiCl₄ [377].

MOCVD is well established in several other compound semiconductors, as mentioned earlier, and can mass produce high-quality epitaxial films. Gallium precursors, such as trimethylgallium (TMGa) and triethylgallium (TEGa), and high-purity O₂ are typically used for MOCVD growth of Ga₂O₃. At the beginning of development, MOCVD growth of Ga₂O₃ faced challenges of low growth rates, high background carrier concentrations, and low electron mobilities [375]. Thanks to the tremendous efforts in optimizing the growth conditions, the structural and electrical properties of Ga₂O₃ film grown by MOCVD have been significantly improved over the recent years [378–382]. Another unique advantage of MOCVD growth is its ability to produce a β -(Al_xGa_{1-x})₂O₃/Ga₂O₃ heterostructure [375, 383, 384], which constitutes an important architecture in Ga₂O₃-based RF applications.

While the aforementioned growth methods are currently the leading techniques and attract significant research interest in Ga₂O₃ epitaxy, additional growth methods, including low pressure chemical vapor deposition (LPCVD) [385–388], mist chemical vapor deposition (Mist-CVD) [389–391], liquid injection metalorganic chemical vapor deposition (LI-MOCVD) [351, 392], and pulsed laser deposition (PLD) [393, 394], have offered epitaxial Ga₂O₃ films of comparable film qualities with the benefits of relatively low deposition temperatures, large carrier concentration ranges, high deposition rates and relatively inexpensive deposition equipment. Lastly, heteroepitaxy of Ga₂O₃ device structures on more thermally conductive foreign substrates for heat mitigation employs epitaxial growth methods described in this section. However, more specific works are further described in section 5.3.3.

5.2.3. Doping

Silicon (Si), Tin (Sn), and Germanium (Ge) are commonly used as donors in β -Ga₂O₃ [395]. At room temperature, the donors show a high activation ratio due to the shallow donor states, typically around 30 meV below the conduction band [396–400]. These dopants can be incorporated into the β -Ga₂O₃ through *in-situ* growth, ion implantation, or diffusion method. The conductivity of the n-type β -Ga₂O₃ can be well modulated by controlling the donor concentration, within the range of 10^{15} – 10^{20} cm^{-3} .

In contrast to the ease and success in achieving n-type doping in β -Ga₂O₃, p-type doping in β -Ga₂O₃ has evaded researchers and has become a primary limitation in the rapid development of various β -Ga₂O₃ devices [3, 375]. Several elements, including Mg, and N, were reported to serve as deep acceptors in β -Ga₂O₃, though with an activation energy larger than 1 eV [401, 402]. Besides, the first principle calculations predict a very flat valence band, leading to a large hole effective mass and low mobility [403, 404]. Moreover, self-trapping of holes limits the free hole conduction in β -Ga₂O₃ due to the local lattice distortion [405–407]. The combination of these factors contributes to the difficult nature of achieving well-behaved hole conduction. Recently, Chikoidze *et al*, reported that undoped β -Ga₂O₃ after an oxygen anneal exhibited p-type nature above 500 °C. A free hole concentration of around 10^{17} cm^{-3} (mobility $\sim 0.4 \text{ cm}^2 (\text{V}\cdot\text{s})^{-1}$) was measured and attributed to the large formation energy of the oxygen donor vacancies [408, 409]. These findings help the community understand the mechanism behind the carrier formation and potentially shed light on achieving better p-type conductivity suitable for practical use in Ga₂O₃.

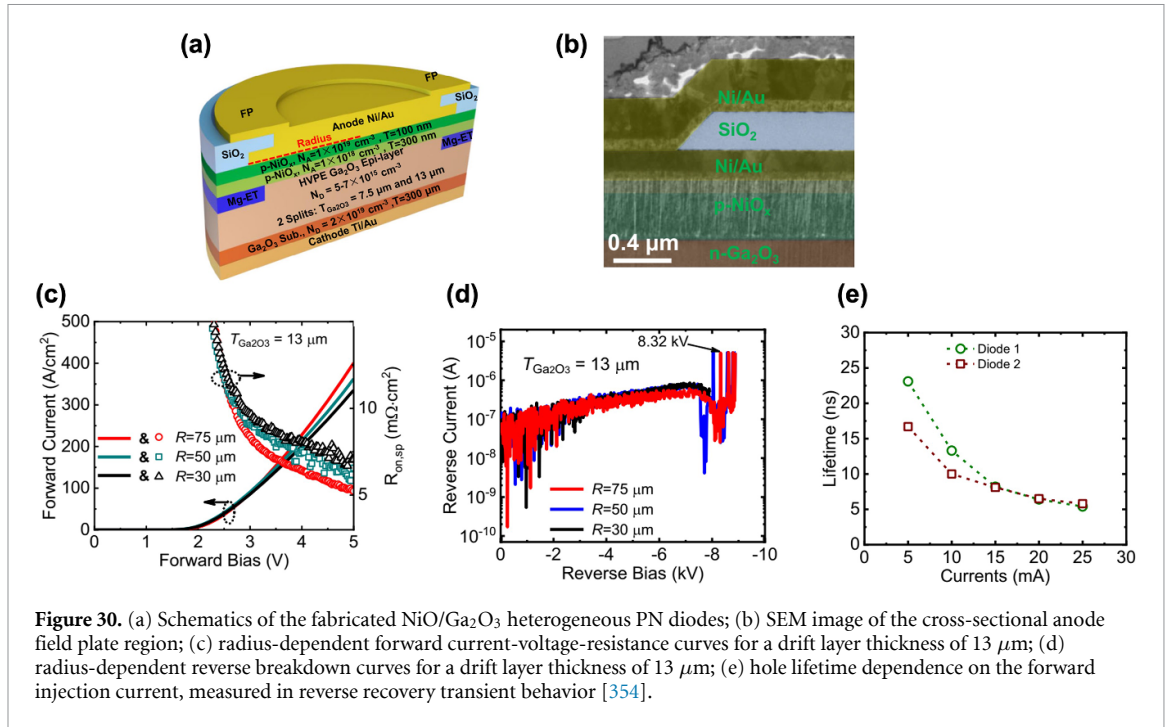


Figure 30. (a) Schematics of the fabricated NiO/Ga₂O₃ heterogeneous PN diodes; (b) SEM image of the cross-sectional anode field plate region; (c) radius-dependent forward current-voltage-resistance curves for a drift layer thickness of 13 μm; (d) radius-dependent reverse breakdown curves for a drift layer thickness of 13 μm; (e) hole lifetime dependence on the forward injection current, measured in reverse recovery transient behavior [354].

5.3. β-Ga₂O₃ device and applications

5.3.1. High power devices

5.3.1.1. SBDs

Ga₂O₃ SBDs were first demonstrated on native n-type Ga₂O₃ substrates, due to the absence of suitable epitaxial growth methods for thick n-drift layers on Ga₂O₃ substrates. In 2013, a Ga₂O₃ SBD fabricated on a bulk (010) substrate grown by the float zone method was reported [410]. A Schottky barrier height of 1.3–1.5 eV was extracted for the Pt contact, and the SBD exhibited a near-unity ideality factor, indicating high crystal quality and good Schottky contact properties. The diodes showed a 150 V breakdown voltage and a high on-resistance of 7.85 mΩ·cm², which was attributed to the low conductivity of the bulk substrates. Later, with the advancement of HVPE growth, a 7 μm-thick Si doped drift layer with doping concentration around 2×10^{16} cm⁻³ was grown on highly Sn-doped (2.5×10^{18} cm⁻³) (001) native Ga₂O₃ substrates. The fabricated SBDs showed a breakdown voltage of 500 V with an improved on-resistance of 3 mΩ·cm² [411]. Catastrophic breakdown occurred in the devices due to the electric-field concentration at the edge of the anode, requiring efficient edge termination to suppress the peak electric field and reduce the leakage current. Several approaches, such as field plating [412–414], junction termination extensions [415–417], and trench metal–insulator–semiconductor (MIS) structures [418, 419], have been proposed and prototyped in Ga₂O₃ SBDs. By deploying a self-aligned field plate with a deep trench filled with thick SiO₂, a 6 kV SBD with a specific on-resistance of 3.4 mΩ·cm² was successfully fabricated. This device offered a high BFOM of 10.6 GW cm⁻² [353] and exceeded the 1D unipolar limit of SiC and GaN.

5.3.1.2. Heterogeneous PN diodes

Though effective p-type β-Ga₂O₃ is still under development, the use of heterogeneous PN structures that employ NiO as the p-type material establishes another route for achieving high voltage diodes [420–425]. The high turn-on voltage, which leads to conduction losses, is characteristic of homogeneous PN structures in WBG materials. However, the band offset of NiO can reduce the threshold voltage, partially resolving this issue [354]. Recently, Zhang *et al* reported a NiO/Ga₂O₃ heterogeneous PN diode by combining Mg implantation termination and field plating architectures with schematics and SEM cross-sections shown in figures 30(a) and (b). These devices produced an 8.32 kV breakdown voltage and the highest BFOM of 13.2 GW cm⁻² among all UWBG power diodes to date [354]. The reverse recovery behavior of the fabricated heterogeneous PN diodes was measured, and the hole lifetime was determined to be 5.4–23.1 ns (figure 30(e)), yielding a mobility of 1.9–8.3 cm² (V·s)⁻¹. Despite the difficulties in observing free hole conduction in Ga₂O₃ as discussed in section 5.2.3, this result indicates that holes can be manufactured in Ga₂O₃ via hole injection, and their presence is not limited by the self-trapping effect.

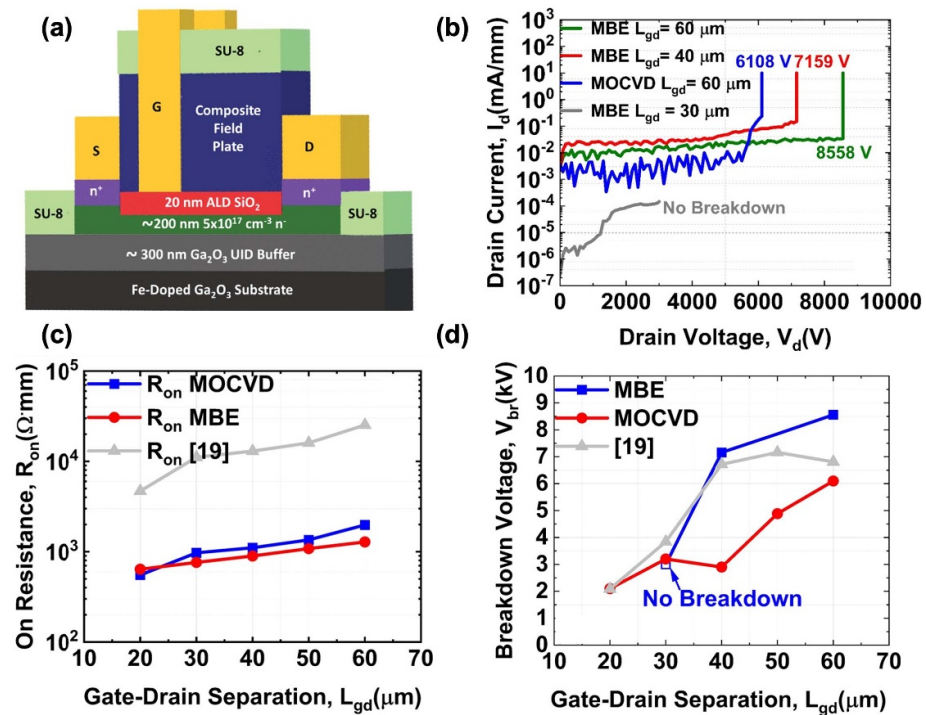


Figure 31. (a) Schematic view of lateral Ga_2O_3 MOSFET based on vacuum annealing with a composite field plate and SU-8 encapsulation layer; (b) breakdown characteristics for the device, the highest breakdown voltage was 8558 V for a $60\ \mu\text{m}$ channel length grown by MBE; (c) comparison of the on-state resistance with vacuum annealing for the channel grown by MOCVD (blue line) and grown by MBE (red line), and without vacuum annealing grown by MBE (gray line); (d) comparison of the breakdown voltage with vacuum annealing for the channel grown by MBE (blue line) and MOCVD (red line), and without vacuum annealing grown by MBE (gray line) [434].

5.3.1.3. MESFETs and lateral MOSFETs

MESFETs were successfully fabricated on Mg-doped semi-insulating Ga_2O_3 substrates in 2011 [352]. A 300 nm thick Sn-doped channel layer was grown by MBE and a Pt/Ti/Au metal stack was deposited as the Schottky gate. The device showed an on-off ratio of 10^4 and a decent three-terminal breakdown voltage of 250 V. However, the unpassivated surface led to a small gate leakage, and the devices suffered from low on-state current due to the high contact resistance of the source/drain electrodes. Later usage of Si ion implantation or diffusion at the source/drain electrode significantly reduced the contact resistance to the order of $10^{-5}\ \Omega\cdot\text{cm}^2$ [426, 427] and thus resolved a significant limitation of the on-state current for Ga_2O_3 transistors.

MOSFETs have been studied to improve the performance of Ga_2O_3 transistors. Depletion-mode Ga_2O_3 MOSFETs have been demonstrated with an ALD Al_2O_3 layer as the gate dielectric as well as the surface passivation layer to reduce surface leakage [428]. On the other hand, a SiO_2 dielectric/ Ga_2O_3 interface was reported to have a large conduction band offset and low interface state density [429], offering an enhancement-mode Ga_2O_3 MOSFET using a Pt gate [430]. These devices showed a breakdown voltage of 400 V without a field plate structure, and the integration of field plate structures enabled a much higher breakdown up to 8 kV [431–433]. Figure 31(a) depicts the device schematic of a lateral Ga_2O_3 MOSFET with a composite field plate design, offering a record-high breakdown voltage of 8.56 kV [434]. The authors reported that vacuum annealing significantly reduced the on-resistance by recovering the surface damage caused by a reactive-ion etching process during fabrication. The on-resistance was reduced by one-order of magnitude while excellent blocking capability was maintained.

5.3.1.4. Vertical transistors

Vertical Ga_2O_3 transistors are favorable in power applications due to their high volume utilization and high power density. Using a fin-shaped channel in vertical transistors (FinFET), as pictured in figure 32(a), removes the need for a p-type material. This structure can also avoid the low effective channel mobility caused by etching damage and interface states in MOSFETs. The demonstration of a 2.6 kV transistor with an on-resistance of $25.2\ \text{m}\Omega\cdot\text{cm}^2$ [435] promoted continued interest and development of FinFET technology in Ga_2O_3 . Although FinFETs have exhibited a high breakdown voltage in Ga_2O_3 , the complicated and costly fabrication process with potentially low device yield is a concern for the technology.

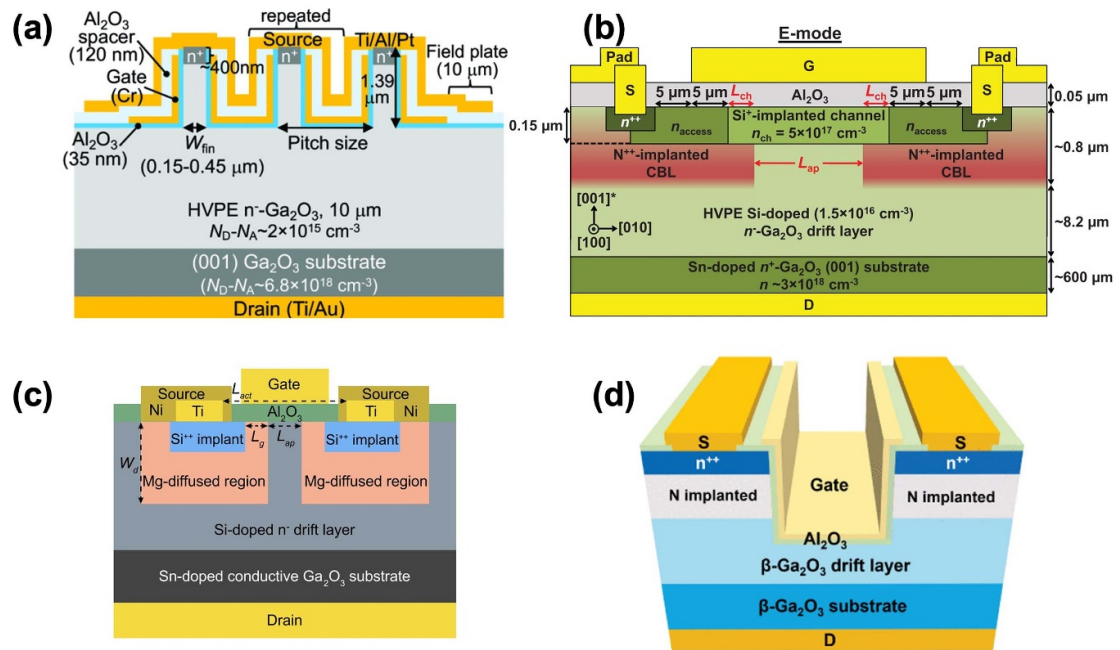


Figure 32. Schematic view of different architectures of vertical Ga_2O_3 transistors: (a) FinFET [435]; (b) current aperture vertical MOSFETs with nitrogen implanted blocker layer [438]; (c) vertical transistor with a diffused barrier (VDBFET) [441]; (d) U-shape trench gate MOSFET with nitrogen ion implantation [442].

Though p-type Ga_2O_3 remains a challenge for the whole community, n-type conductive Ga_2O_3 can be converted to insulating materials by oxygen annealing [436, 437] or by Mg/N implantation or diffusion [438–440]. This can be useful for forming effective current blocking layers in developing vertical transistors. Wong *et al* reported the first Ga_2O_3 CAVET (figure 32(b)) with a Mg implanted blocking layer [439]. However, the devices showed relatively high leakage and poor gate modulation. A possible reason was the diffusion of Mg caused by high temperature annealing used to repair crystal damage after implantation. Later, the same group reported on an N implantation based Ga_2O_3 CAVET [438], demonstrating a breakdown voltage of 253 V with a decent on–off ratio of 10^7 , but a large specific resistance of $135 \text{ m}\Omega\cdot\text{cm}^2$. In contrast to the use of implantation technology, Zeng *et al* utilized an Mg-diffusion process (figure 32(c)) to form a current blocking layer [441], thus avoiding unwanted Mg diffusion during the post-annealing process. The prototype exhibited normally-off operation and a high on–off ratio of 10^8 . Though the breakdown voltage was limited to 73 V, this novel diffusion doping method opens an alternative route toward developing vertical Ga_2O_3 transistors.

Similar to SiC and GaN, the U-shaped trench MOSFET (UMOSFET) (figure 32(d)) has also attracted great research interest and was successfully fabricated based on oxygen-annealed and N-implanted channel layers [442, 443]. The nature of the MOSFET made it easy to achieve normally-off operation. Recently, a UMOSFET with a N-implanted current blocking layer exhibited a breakdown voltage of 455 V with a low on-resistance of $10.4 \text{ m}\Omega\cdot\text{cm}^2$ [442].

5.3.2. RF devices

Green *et al* reported the first RF measurement data in Ga_2O_3 employing a lateral MOSFET architecture with a 180 nm MOVPE-grown Si-doped epitaxial layer on semi-insulating Ga_2O_3 substrates. A gate recess was utilized to reduce the channel thickness to 90 nm [444]. Their devices delivered an f_T of 3.3 GHz and a f_{max} of 12.9 GHz, as well as a continuous wave mode output power of 0.23 W mm^{-1} and PAE of 6.3% measured at a drain voltage of 25 V at 800 MHz. Later, Singh *et al* proved that self-heating was a dominant factor limiting the performance of Ga_2O_3 RF devices [445]. By adopting a pulsed mode measurement method, the device produced 0.13 W mm^{-1} at 1 GHz with a higher PAE of 12%. This finding urges more effective thermal management strategies to address the low TC issue for Ga_2O_3 . In addition, the pulsed IV measurements indicated that drain-dispersion, likely caused by traps located either at the surface of the gate dielectric or gate-oxide–semiconductor interface, limited the RF output power as well [446].

Gate length scaling can boost the frequency of RF devices; however, it is limited by the thickness of the channel. A high gate-channel aspect ratio (gate length over gate-to-channel distance) needs to be maintained to suppress the short-channel effect. By growing a 65 nm thick channel layer with a carrier concentration of

$2 \times 10^{18} \text{ cm}^{-3}$ and decent mobility of $90 \text{ cm}^2 (\text{V}\cdot\text{s})^{-1}$, Chabak *et al* further scaled down the gate length to 140 nm, achieving an f_T/f_{max} of 5.1/17.1 GHz [447]. Kamimura *et al* utilized shallow Si implantation to define a thin channel to maintain the high aspect ratio. Their devices offered a high f_T/f_{max} of 10/27 GHz [448]. Similarly, the growth of a delta-doped Si layer is another way to achieve high sheet charge density and better confinement in the channel, thus enabling an f_T/f_{max} of 27/16 GHz [449]. The $(\text{Al}_x\text{Ga}_{1-x})_2\text{O}_3/\text{Ga}_2\text{O}_3$ heterostructure is an alternative architecture that can achieve better carrier confinement and reduced effective channel thickness [450, 451]. High carrier densities between 10^{12} and 10^{13} cm^{-2} have been reported in $(\text{Al}_x\text{Ga}_{1-x})_2\text{O}_3/\text{Ga}_2\text{O}_3$ modulation-doped transistors (MODFET) with enhanced carrier mobilities [452–456]. A record-high f_T/f_{max} of 30/37 GHz has recently been reported in $(\text{Al}_x\text{Ga}_{1-x})_2\text{O}_3/\text{Ga}_2\text{O}_3$ MODFETs [457].

5.3.3. Thermal management for Ga_2O_3 devices

Ga_2O_3 is notorious for its low TC and will especially suffer from self-heating. Self-heating not only degrades the reliability and lifetime of a device but also limits its electrical performance. Several cooling strategies have been reported for thermal management at the device level in Ga_2O_3 , including heteroepitaxial channel grown on foreign substrates with high TC, wafer bonding to high-thermal-conductivity substrates, and integration of heat spreading layers in close proximity to the active device areas. Details regarding diamond-based thermal management for $\beta\text{-Ga}_2\text{O}_3$ were discussed in section 4.3.2.

Various studies have reported thin Ga_2O_3 epitaxial growth on SiC [458, 459], AlN [460], and diamond substrates [461, 462] due to their much higher thermal conductivities. The TC of an 81 nm thick $\beta\text{-Ga}_2\text{O}_3$ grown on 4H-SiC substrate was measured to be $3.1 \pm 0.5 \text{ W (m}\cdot\text{K)}^{-1}$ and the thermal boundary conductance between $\beta\text{-Ga}_2\text{O}_3/\text{SiC}$ interface was $140 \pm 60 \text{ MW (m}^2\cdot\text{K)}^{-1}$ [459]. Despite the promising results shown by thermal characterization and device simulation, experimental demonstration of an active device of Ga_2O_3 on foreign substrates without degrading the electrical performance is yet to be shown.

Besides the direct growth of Ga_2O_3 on foreign substrates, the integration of $\beta\text{-Ga}_2\text{O}_3$ with highly thermally conductive substrates has also been reported through ion cutting [463, 464] and fusion bonding processes [465]. A thermal boundary conductance of $60\text{--}130 \text{ MW (m}^2\cdot\text{K)}^{-1}$ between the $\beta\text{-Ga}_2\text{O}_3/\text{SiC}$ interface formed via the ion cutting process was reported [464]. Minimizing the thermal boundary resistance and Ga_2O_3 substrate thinning is key in facilitating efficient heat removal. A Ga_2O_3 SBD on a thinned-down, 100 μm -thick bulk substrate showed a significant reduction in junction-to-case thermal resistance by 30% compared to the reference device on 250 μm -thick substrates [466], and further substrate thinning to less than 50 μm with the integration of a backside heat sink are predicted to offer further improvements of heat transfer [467].

6. Conclusion

Over the course of recent decades, GaN-based electronics have undergone extensive exploration for various applications, including optoelectronics, high-power devices, and high-frequency electronics. This surge in interest can be attributed to GaN's exceptional material properties. Substantial progress has been achieved in pushing the boundaries of device performance, encompassing both fundamental research and advancements in industrial processes. This continuous improvement in the fields of physics, materials science, and manufacturing processes has expanded the horizons for WBG materials, ushering in new possibilities and catalyzing numerous research breakthroughs, particularly in the realm of UWBG technology. To quantify the progress achieved in the domain of U/WBG materials, figure 33 has been plotted as a benchmark, utilizing Baliga's figure of merit, specifically the relationship between R_{on} and breakdown voltage, as a measure of performance for power devices. Remarkable advances have been made by researchers, resulting in the development of kilovolt-class diodes and transistors across all the materials discussed within this review. This accomplishment underscores the immense potential of these U/WBGs for high-power applications.

In the field of RF applications, GaN HEMTs have demonstrated outstanding performance metrics and have successfully transitioned into commercialization for applications within the X-Ka band. Conversely, the landscape for UWBG materials is still in its nascent stages of development, as depicted in figures 34(a) and (b). These figures vividly illustrate that the state-of-the-art power and RF performance across various UWBG materials significantly lags behind that of GaN.

In the final part of this review article, we are choosing a few common research directions that will significantly impact the WBG to UWBG transition.

Substrates serve as the fundamental building blocks for semiconductor technology, forming the critical foundation upon which it is constructed. The issue of scalable substrates is a pervasive challenge across all the materials under discussion here. Bulk GaN devices have garnered significant research interest due to their potential for higher performance and enhanced reliability. However, the availability of suitable substrates

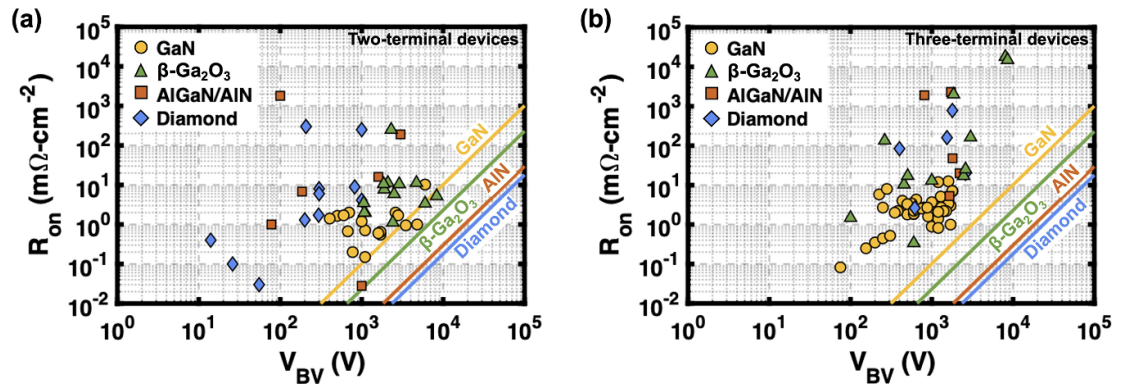


Figure 33. BFOM unipolar limit and experimental data for (a) two-terminal and (b) three-terminal devices. References for (a) GaN SBDs: [61, 67, 69, 72, 73, 468, 469]; GaN PNDs: [79–82, 89, 90, 470]; GaN JBS, SJs: [92, 93, 95]; AlGaIn/AlN: [214, 236, 237, 250, 251, 471]; diamond: [281, 287, 292–294, 302, 472–475]; Ga₂O₃ SBDs: [353, 412, 413, 415, 417–419, 476]; Ga₂O₃/NiO PNDs: [354, 421, 423, 424, 477] and (b) lateral GaN: [114, 120, 128, 478, 479] and references therein [480], and references therein; vertical GaN: [131, 134, 135, 139, 141, 145, 147, 481]; AlGaIn: [215, 216, 233, 239, 482]; diamond: [309, 312, 483–485]; lateral Ga₂O₃: [432–434, 486, 487] Ga₂O₃ vertical [435, 438, 442, 443, 488, 489].

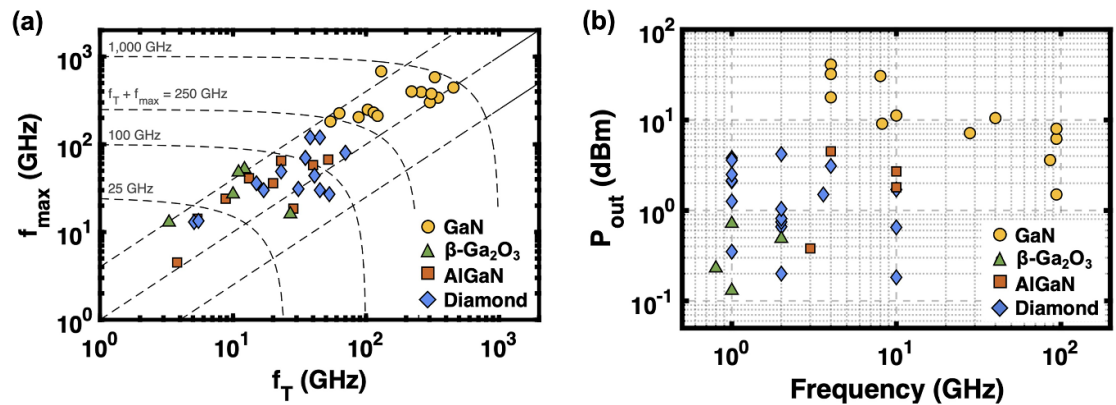


Figure 34. State-of-the-art RF performance: (a) $f_{\max}$ vs f_T and (b) P_{out} vs frequency of U/WBG transistors. References for (a) GaN HEMTs: [490–501]; AlGaIn: [217, 242–248, 502]; diamond: [321–324, 503–510]; Ga₂O₃: [444, 448, 449, 511] and (b) GaN HEMTs: [157, 159, 160, 164–166, 171, 176, 178, 490, 512]; AlGaIn: [217, 242, 247, 248]; diamond: [319, 320, 322, 324, 503–508, 325, 513, 514]; Ga₂O₃ [444–446].

remains constrained by both size and cost limitations. For instance, the cost of a 2 inch bulk GaN substrate remains prohibitively high, and the commercial availability of substrates larger than 4 inches remains a formidable challenge as of the present date. The development of electrically conducting and optically transparent AlGaIn substrates is still in its infancy, and in the case of diamond substrates, typical MPCVD growth methods limit their size to less than 1 cm. Although ongoing efforts in the realm of novel growth methods have resulted in the production of larger substrates, the demonstration of large-diameter bulk GaN, AlN, AlGaIn, and diamond substrates with both low defect densities and affordable manufacturing costs remains a formidable hurdle for researchers to overcome.

While it is widely recognized that achieving improved doping control and faster growth rates is imperative for all the materials under discussion, we believe that a pivotal area of research lies in selective area doping within UWBG materials. Selective area doping has the potential to yield remarkable advancements in many device concepts. Generally, due to the substantial bandgap in UWBG materials, the activation of dopants to attain high carrier densities has presented a persistent challenge. The overall proficiency of doping through innovative techniques such as light-assisted doping and selective area regrowth methods holds the promise of facilitating more effective device technology. To date, the absence of reliable n-type and n+ doping methods in diamond, coupled with the scarcity of p-type and p+ doping techniques in AlGaIn and the absence of an effective p-type doping method in Ga₂O₃, hinders the creation of properly designed PN junctions, the implementation of effective field termination techniques, and the formation of robust ohmic contacts.

The success of ion-implantation can streamline various processes, offering simplifications with significant implications. For instance, in devices like CAVET, the need for a complex regrowth step could

potentially be reduced or entirely eliminated if ion-implantation can be consistently and effectively achieved. Similarly, the creation of a deep p-well column, essential for fabricating superjunction structures, could become a more practical manufacturing process if ion-implanted dopants could be reliably activated. Therefore, it is imperative to continue researching doping techniques and alternative methods, some of which have been discussed in this review.

For power electronics applications, achieving a robust and uniform avalanche effect in devices is of paramount importance for safeguarding devices against the extreme conditions encountered in real-world scenarios. This capability not only reduces the need for excessive over-design but also permits device operation close to its material limits. While the avalanche phenomenon has been more consistently realized in GaN PN diodes fabricated on native bulk GaN substrates, further data is necessary to fully comprehend the mechanisms and harness their potential in practical applications. However, in UWBG materials, the reliable observation and generation of the avalanche phenomenon remain elusive. This challenge can be attributed in part to the immaturity of the materials and limitations in device architecture, underscoring the need for the development of the physics governing avalanche in UWBGs.

High- k dielectric materials occupy a pivotal role in addressing the requirements of UWBG device technologies. Gate dielectrics with superior electrical strength compared to the semiconductor channel are essential for effective gate technology. These dielectrics must exhibit a very high critical electric field while also providing substantial band offsets to minimize gate leakage. Given the limited space (in thickness) available for the dielectric layer under the gate, the pursuit of high- k value materials becomes crucial. An ideal dielectric should possess a large band offset, a high dielectric constant, low gate leakage, and minimal interface traps to ensure the functionality and reliability of device technology. Insufficiently engineered dielectric layers can significantly impact and even limit a device's performance. Additionally, the emerging branch of nitride ferroelectric gate stacks [515, 516], not discussed in this article, is poised to acquire substantial research interest in the coming decade.

Lastly, the concept of electro-thermal co-design is gaining prominence, particularly in GaN RF devices. Elevated channel temperatures can degrade the mobility of the 2DEG and jeopardize device reliability under high-power operation. Traditional thermal management techniques, such as heat sinks and appropriate thermal interface materials at the package level, remain important. However, the heterogeneous integration of PC diamond with other WBG materials and even silicon technology as a heat-spreading layer presents an alternative approach to device-level cooling. Effective thermal management is essential for UWBG devices, as they are expected to operate at higher voltages and significantly higher power densities, rendering them more susceptible to thermal-related issues.

In summary, U/WBGs represent a highly fascinating and rapidly advancing domain, offering the scientific community a vast array of research prospects in both materials science and device physics. The anticipated range of applications is equally promising, following the path set by SiC and GaN.

Data availability statement

All data that support the findings of this study are included within the article (and any supplementary files).

Acknowledgments

This work was funded by ULTRA, an Energy Frontier Research Center (EFRC) funded by the U.S. Department of Energy, Office of Science, Basic Energy Sciences under Award No. DE-SC0021230.

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