PAPER • OPEN ACCESS

Fatigue and fracture mechanical behavior for Chinese A508-3 steel at room temperature

To cite this article: K K Shi et al 2018 IOP Conf. Ser.: Mater. Sci. Eng. 372 012003

View the article online for updates and enhancements.

You may also like

- <u>Organic–Inorganic Hybrid Membranes for</u> <u>a PEMFC Operation at Intermediate</u> <u>Temperatures</u> Je-Deok Kim, Toshiyuki Mori and Itaru Honma
- MORPHOLOGICAL ANNOTATIONS FOR GROUPS IN THE FIRST DATABASE D. D. Proctor
- Improved Performances of LifNi_{0.65}Co_{0.00}Mn_{0.27}JO₂ Cathode Material with Full Concentration Gradient for Li-Ion Batteries Sung-Jun Yoon, Kang-Joon Park, Byung-Beom Lim et al.





DISCOVER how sustainability intersects with electrochemistry & solid state science research



This content was downloaded from IP address 3.15.153.69 on 04/05/2024 at 17:09

IOP Conf. Series: Materials Science and Engineering 372 (2018) 012003 doi:10.1088/1757-899X/372/1/012003

Fatigue and fracture mechanical behavior for Chinese A508-3 steel at room temperature

K K Shi^{1,2}, H Xie¹, B Zheng¹ and X L Fu¹

¹Science and Technology on Reactor System Design Technology Laboratory, Nuclear Power Institute of China, Chengdu, 610213, China

E-mail: shikai1000@163.com

Abstract. Material, A508-3 steel, has been used in nuclear reactor vessels. In the present study, fatigue and fracture mechanical behavior of Chinese A5083 steel at room temperature are studied by mechanical material testing machine (MTS). Test data of material's mechanical behavior including uniaxial tension, low cycle fatigue (LCF), threshold value of stress intensity factor (SIF) range, fatigue crack growth (FCG), and fracture toughness is generated and given for further study. It is worth noting that the model in predicting FCG of material from LCF parameters is verified and discussed.

1. Introduction

The basic material experimental data is important design input parameters for the structural integrity assessment of engineering components. Reactor pressure vessel (RPV) is an important part of the reactor coolant for the second and third generation nuclear power plants (NPPs). A set of operation, emergency, and accident transients could exist that allow cold water to come into contact with the inner surface of the vessel wall, producing high thermal stress. The low alloy ferritic steel, A508-3 steel, have been used to make RPVs. Because the A508-3 steel has good weld ability and radiation resistance than other low carbon ferritic steel. The A508-3 steel, firstly, is developed from A533-B steel in American for pressure vessel with the higher safety standards of nuclear. The A533-B steel's mechanical properties were widely studied [1-4] and the steel has been used extensively in heavy section pressure vessels for nuclear applications. During the operating lifetime of these vessels, neutron bombardment is sufficient to affect substantial changes in the metallurgical and mechanical properties of the vessel structural materials. Neutron irradiation increase strength properties and decrease ductility.

For the Chinese A508-3 steel, at room temperature, the uniaxial tension, low cycle fatigue (LCF), threshold value of stress intensity factor (SIF), fatigue crack growth (FCG), and fracture toughness is studied, analyzed, and discussed in the present study.

2. Mechanical behavior of ChineseA508-3 steel

In this section, test data comes from the hydraulic mechanical testing machines (MTS).

2.1. Uniaxial tension properties

Figure 1 givens the uniaxial tension engineer stress and strain curves. Before necking stage, the true stress and strain can be calculated by using Bridgman's correction factor [5].

Based on the arc funnel specimen (Radius=10 mm), the full-range stress and strain curve (figure 2)

Content from this work may be used under the terms of the Creative Commons Attribution 3.0 licence. Any further distribution of this work must maintain attribution to the author(s) and the title of the work, journal citation and DOI. Published under licence by IOP Publishing Ltd 1

IOP Conf. Series: Materials Science and Engineering 372 (2018) 012003 doi:10.1088/1757-899X/372/1/012003



is obtained by finite aided testing method [6].



Figure 1. Test specimen of equal diameter round Figure 2. Test specimen of equal diameter round bar (Diameter=8 mm) and arc funnel specimen (Radius=10 mm).

2.2. Low cycle fatigue (LCF) behavior

bar, Diameter=8 mm.

There exist many methods available to analyze the crack nucleation and failure life. For complex structures and environments, especially, finite element analyses combined with the local strain theory are often used in design phase analysis [7]. Previous studies including Basquin, Manson, and Coffin have obtain the relationship between strain range and cyclic failure life for testing materials. In addition, the average stress σ_m parameter is considered in Manson-Coffin equation which is a classic relation in order to describe the low cycle fatigue behavior of materials under different load environments. Figure 3 shows the typically low cycle fatigue curve of A508-3 steel.



Figure 3. Low cycle fatigue properties of A508-3 steel.

2.3. Threshold value of SIF

Considering the simplicity and accuracy of elastic unloading compliance theory, the amount of crack propagation is detected and calculated using elastic unloading compliance method by computer codes. Based on the definition of threshold value of stress intensity factor for metal materials, test data is obtained and analyzed when no crack propagation is found in 10^7 cyclic life. For a material, commonly, the linear relation between the load stress ratio and the threshold value of SIF does not exist. However, a conservative calculation result would be obtained based on assuming the establishment of a linear dependency for servicing engineering analysis [8]. Figure 4 givens only the threshold value of stress intensity factor (SIF) range under load stress ratio R=0.1.



Figure 4. Threshold value of stress intensity factor (SIF) range of A508-3 steel.

Combination the threshold value of SIF and the low cycle fatigue (LCF) properties, material's fatigue crack growth (FCG) of second stage is estimated by kinds of prediction model of mode tension type failure cyclic life.

2.4. Fatigue crack growth (FCG)

Considering previous research results, fatigue crack growth would be studied from the following two scales, macroscopic and microscopic. Reference [9] has also studied the driving force, stress intensity factor K, near crack tip based on the stress criterion. The load stress ratio can affect the result of FCG rate of material. But, in the present study, the load stress ration is not considered and investigated.

Figure 5 shows only the fatigue crack growth (FCG) rate under second stage corresponding to the load stress ratio R=0.1.



Figure 5. Fatigue crack growth rate of A508-3 steel.

The conception that there is the highly strained zone near the crack tip is like a small low cycle fatigue (LCF) test specimen is assumed by many studies. In Pandey's model, for example, the process zone is viewed as the highly strained zone in the front of crack tip. Considering the energy of process zone equals to the energy of whole plastic zone [10]. Using the essential relationship between low cycle fatigue (LCF) and fatigue crack growth (FCG) rate, various prediction models are applied for analyzing behavior of Chinese A508-3 steel. Many prediction results including SHI-CAI model [11], Glinka model [12], and Ellyin-Li model [13] are showed in figure 6.



Figure 6. Prediction results based on estimating models of A508-3 steel.

2.5. Fracture toughness

The three primary factors which affect the fracture toughness of structural steels are temperature, loading rate, and constraint. Generally, the fracture toughness of structural steels increases with increasing temperature and decreases with increasing loading rate.



Figure 7. J integral resistance curve of A508-3 steel.

For real fracture, the crack failure degree, test specimen thickness, and experimental loading environment have influence on the constraint in front of the crack tip [14]. Figure 7 obtains the result of J integral resistance curve with different initial crack length a_0 . Results show the different J integral resistance curves for compact tensile specimens with 50mm thickness. A so-called constraint effect would be introduced into explaining above phenomenon. The constraint have defined in measuring of 2018 International Conference on Material Strength and Applied Mechanics

IOP Publishing

IOP Conf. Series: Materials Science and Engineering 372 (2018) 012003 doi:10.1088/1757-899X/372/1/012003

the resistance to plastic flow. Basically, a low J integral value corresponds to a high level of constraint near the crack tip. The reason is that the plastic deformation and associated energy dissipation are restricted by constraint. Therefore, the resistance to fracture is low. The stress triaxiality can often been used to described the level of constraint in the front of the crack tip. In other words, a high value of stress triaxiality is equivalent to a high level of constraint [15].

3. Conclusion

For Chinese A508-3 steel, the mechanical properties at room temperature are given, which include uniaxial tension, low cycle fatigue (LCF), threshold value of stress intensity factor (SIF), fatigue crack growth (FCG), and fracture toughness. These basic behaviors is analyzed and discussed, in the present study, in order to service the nuclear power plant safety.

The mechanical properties in different temperature environments will be studied and discussed in the future.

Acknowledgments

The authors gratefully acknowledge the support of Lixun CAI professor of applied mechanics and structure safety key laboratory of Sichuan Province, school of mechanics and engineering, southwest JIAOTONG University, Chengdu, China.

References

- [1] Yu M, Chao Y J and Luo Z 2015 An assessment of mechanical properties of A508-3 steel used in Chinese nuclear reactor pressure vessels *J Press Vessel-T ASME* **137**(3) 031402
- [2] Fang Y 2011 Fracture toughness prediction of domestic A508-III steel based on master curve approach and its application to reactor pressure vessel P-T curve *Master's thesis* (Shanghai: East China University) (in Chinese)
- [3] Yu M, Luo Z and Chao Y J 2015 Correlations between Charpy V-notch impact energy and fracture toughness of nuclear reactor pressure vessel (RPV) steels *Eng Fract Mech* 147 187-202
- [4] Richard Wright 2014 Creep of A508/533 pressure vessel steel United States doi: 10.2172/1166040
- [5] Bridgman P 1944 The stress distribution at the neck of a tension specimen J Press Vess-T ASME **32** 553-74
- [6] Yao D, Cai L and Bao C 2016 A new approach on necking constitutive relationships of ductile materials at elevated temperatures *Chinese J Aeronaut* **29**(6) 1626-34
- [7] Ricotta M 2015 Simple expressions to estimate the Manson–Coffin curves of ductile cast irons Int J Fatigue 78(0) 38-45
- [8] Davenport R and Brook R 1979 The threshold stress intensity range in fatigue *Fatigue Fract* Eng M 1(2) 151-8
- [9] Tang K K, Berto F and Wu H 2016 Fatigue crack growth in the micro to large scale of 7075-T6 Al sheets at different R ratios *Theor Appl Fract Mec* **83** 93-104
- [10] Pandey K and Chand S 2003 An energy based fatigue crack growth model *International Journal of Fatigue* **25**(8) 771-8
- [11] Shi K K *et al* 2015 Structural fatigue crack growth on a representative volume element under cyclic strain behavior *Int J Fatigue* **74**(0) 1-6
- [12] Glinka G 1982 A cumulative model of fatigue crack growth Int J Fatigue 4(2) 59-67
- [13] Li D, Nam W and Lee C 1998 An improvement on prediction of fatigue crack growth from low cycle fatigue properties *Eng Fract Mech* **60**(4) 397-406
- [14] Petti J P and Dodds R H Jr 2004 Constraint comparisons for common fracture specimens: C(T)s and SE(B)s Eng Fract Mech 71(18) 2677-83
- [15] Huang Y, Zhou W and Wang E 2014 Constraint-corrected J–R curve based on three-dimensional finite element analyses *Fatigue & Fract Eng M* **37** 1101-15