

PAPER • OPEN ACCESS

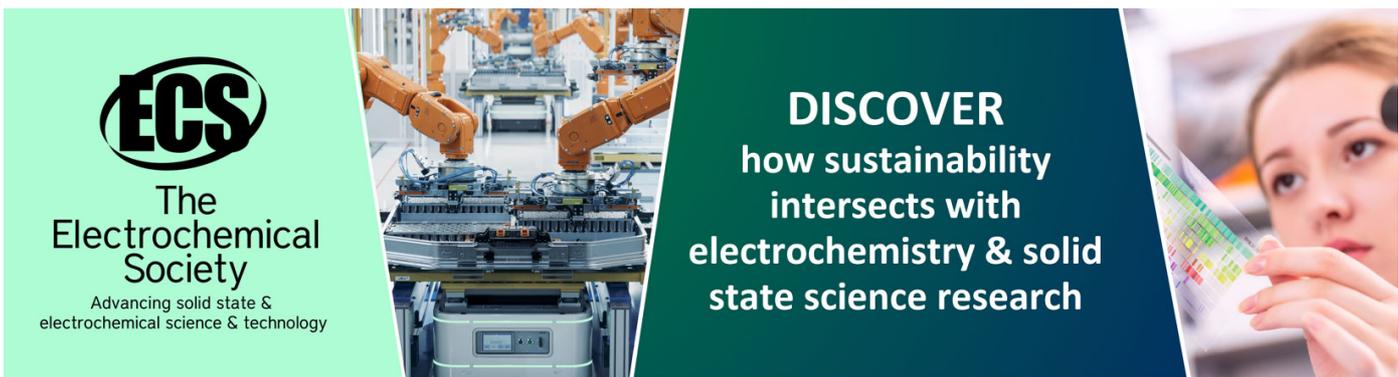
Investigation of thermal properties of raw materials of asphalt mixtures

To cite this article: R Géber *et al* 2017 *IOP Conf. Ser.: Mater. Sci. Eng.* **175** 012047

View the [article online](#) for updates and enhancements.

You may also like

- [Application of Rietveld refinement in orientated material structures](#)
E Nagy, F Kristály and V Mertinger
- [Project Management Success Factors](#)
T B Venczel, L Berényi and K Hriczó
- [Advantages of the CCD camera measurements for profile and wear of cutting tools](#)
G Varga, Z Balajti and I Dudás



ECS
The
Electrochemical
Society
Advancing solid state &
electrochemical science & technology

DISCOVER
how sustainability
intersects with
electrochemistry & solid
state science research

Investigation of thermal properties of raw materials of asphalt mixtures

R Géber, A Simon, I Kocserha

University of Miskolc, Institute of Ceramics and Polymer Engineering, Hungary

E-mail: femgeber@uni-miskolc.hu

Abstract. Asphalt mixtures are composite materials, which are made of different grades of mineral aggregates and bitumen. During the mixing process mineral materials were blended with bitumen at relatively high temperature (~200 °C). As the binding process come off in these higher temperature range, thermal properties of asphaltic materials are important.

The aim of this project is to reveal the thermal properties of raw materials. During our research two types of mineral aggregates were tested (limestone and dolomite) by different methods. Differential thermal analysis, thermal expansion and thermal conductivity were investigated at technologically important temperatures. The results showed that the structure of mineral materials did not change at elevated temperatures, expansion of samples was negligible, while thermal conductivity changed by temperature.

1. Introduction

Asphalt mixtures are the most used pavement materials all over the world. The mixtures consist of mineral aggregates and bitumen as binding material [1-5]. One of the most important components of asphalt are fillers ($d < 0.063\text{mm}$) which are the finest part in mineral aggregate. Mixed together with the binder a so-called asphalt mastic is formed. The contact between fillers and bitumen is not exactly known, until today.

During the lifetime of asphalt mixtures and the compacted pavements heat will play a significant role [6]. Raw mineral aggregates are stored in cold aggregate bins. At the beginning of the production aggregates are heated up in the drying drum in order to evaporate the adsorbed water from their surface. Furthermore, raw materials need to reach the mixing temperature. Then aggregates are transferred by the hot elevator to the hot aggregate bin, then to the mixer where hot bitumen is also added from the bitumen tank. After mixing, asphalt mixtures are loaded into heated trucks and transported to the field to be paved. Compacting process and traffic temperature both affect the properties of asphalt pavements.

The effect of temperature on the properties of mineral materials is not well known till today. Only a few research dealt with this area [7, 8]. Devecseri [8] investigated the changes of physical properties (*weight change, particle size change and colour change*) of different asphalt aggregates (*effusive and sedimentary rocks with the fraction of 11/16 mm*) by elevated temperatures (240°C and 480°C). She found that high temperatures (480 °C) cause mineralogical, physical and colour changes in aggregates. She also stated that during heating aggregates behave contrary to each other, therefore there is no exact relation between their thermophysical and mechanical properties.



Considering the above mentioned, the aims of this research is to investigate the thermal properties of raw materials (*mineral fillers*) for a better understanding of the cohesion between fillers and bitumen.

2. Materials and methodology

2.1. Sample preparation

Limestone (*Mexikóvölgy*) and dolomite (*Pilisvörösvár*) fillers were tested during the research. Both minerals are widely used in Hungary as asphalt fillers.

Samples were prepared for further tests using standard sieves. Fractions of mineral materials that are smaller than a given particle size ($d < 0.063 \text{ mm}$) were created. After sieving, fillers were dried to weight-constancy then they were hermetically sealed in containers after cooling down. The reason of this was to avoid any moisture uptake.

2.2. Testing procedures

Determination of particle size distribution of fillers were done by the use of Horiba LA-950V2 instrument. Wet method, sodium-pyrophosphate addition and ultrasonic treatment was used.

Morphological tests were carried out on Carl Zeiss EVO MA10 scanning electron microscope (SEM). Electron micrographs were taken in different magnifications. The aim of this test was to observe morphology and geometrical features of fillers.

Differential Thermal Analysis were done on MOM Derivatograph-C type instrument in temperature ranges of 50°C – 1000°C . Heating rate was $5^\circ\text{C}/\text{min}$. Weight change of fillers and their endothermic or exothermic reactions can be revealed with this method.

With differential scanning calorimetry enthalpy changes and heat capacity of fillers were determined by Mettler Toledo DSC 823 E type instrument. Heating and cooling rates of $10^\circ\text{C}/\text{min}$ were used in ranges of 30°C – 200°C . Mineral fillers were placed in a $40 \mu\text{l}$ aluminium crucible.

In order to investigate the change in length of fillers a heating microscope (*manufactured by Camar Elettronica*) and Linseis L75 laser dilatometer were used. Heating microscope was used to measure optically the change of height of compacted specimens. Compacted samples (with a diameter of 2 mm and a height of 4 mm) were heated up to 200°C with a heating rate of $5^\circ\text{C}/\text{min}$. Both fillers could be compacted for this test.

Relative length change was determined during heating and cooling runs with the use of laser dilatometer. For this test a sample with a length of 20 mm and a diameter of 7 mm was needed. Only limestone filler was tested, because of compaction difficulties.

3. Results and discussion

3.1. Test results of mineral fillers

Table 1. contains all the test results performed on mineral fillers.

Table 1. Main properties of fillers

| Material property | unit | Limestone $d < 0.063 \text{ mm}$ | Dolomite $d < 0.063 \text{ mm}$ |
|---------------------------|--------------------------------|-------------------------------------|------------------------------------|
| Mineral composition | wt% | 100 % CaCO_3 | 100 % $\text{MgCa}(\text{CO}_3)_2$ |
| Bulk density | $\text{g}\cdot\text{cm}^{-3}$ | 2.717 | 2.842 |
| BET specific surface area | $\text{m}^2\cdot\text{g}^{-1}$ | 1.02 | 0.38 |
| Hydrophilic coefficient | - | 0.76 | 0.89 |

Figure 1. shows the particles size distribution curves (*cumulative passing and hystogram*) of fillers. According to the results, it was found that these fillers can be characterized as polydisperse systems and they contain fine and coarse particles in different quantity by fraction. Mean particle diameter (d_{50}) of limestone is 16.82 μm , and the mean particle size of dolomite is 39.84 μm . 20 percent of limestone particles are under 10 microns, while in case of dolomite the amount of these fine particles are under 2 percent.

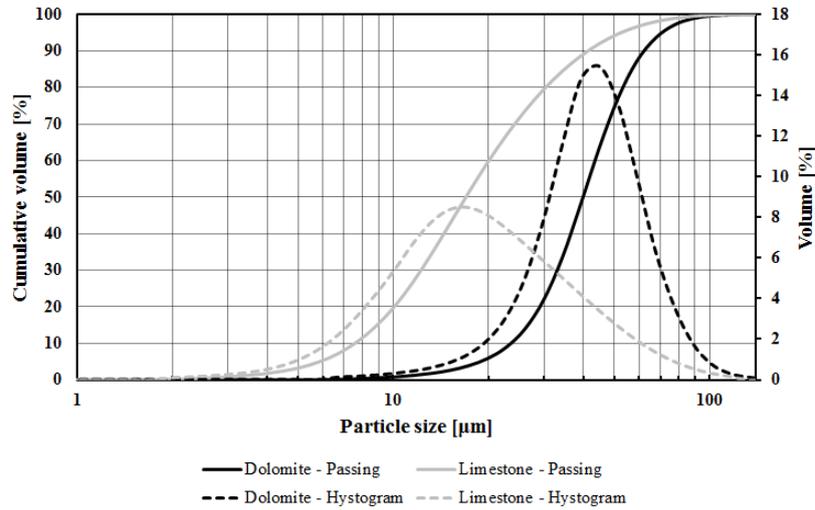


Figure1. Particle size distribution of fillers

Fig. 2. shows the microstructures of fillers (*magnification=200X and 1500X*).

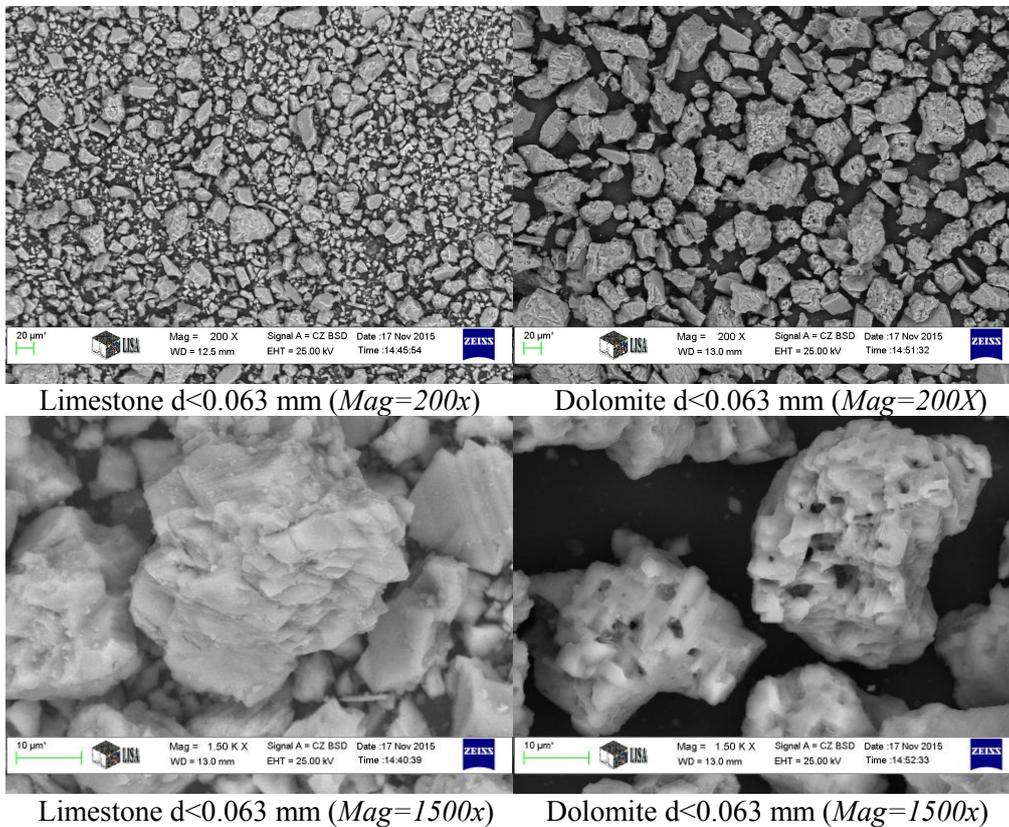


Figure 2. Scanning electron micrographs of fillers

The SEM micrographs confirm the results of particle size distribution tests. Comparing the micrographs, which were taken at a magnification of 200X, it can be observed that limestone filler is rich in fine particles while dolomite does not contain fines. This is the reason of the low BET specific surface of dolomite (*Table 1.*). Higher magnifications show well the morphology and the surfaces of particles. Limestone filler looks solid, on which submicronal particles are stuck. The shape of grains are various, mainly polygonal, because of the comminution processes. Dolomite particles are also polygonal and more porous than limestone. Fig. 3. shows results of differential thermal analysis.

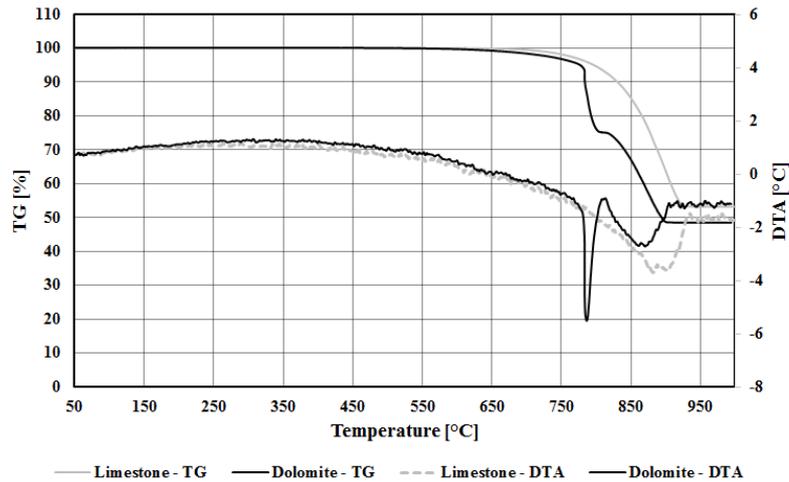


Figure 3. TG and DTA curves of fillers

TG (*thermogravimetric*) curves represent the weight change of fillers, while DTA (*differential thermal analytical*) curves show the temperature changes occurring within the materials. Limestone filler has a slow weight loss in 670–900 °C temperature range. This is due to the decarbonisation of CaCO_3 . During this reaction CaO is formed while CO_2 is released. This phenomenon is an endothermic reaction, as the DTA curve shows a negative peak. TG curve of dolomite shows also a thermal decomposition, but in this case this process is a two-stage reaction. The first endothermic reaction belongs to the decomposition of dolomite, while the second endothermic reaction belongs to the decomposition of CaCO_3 . Up to 200°C, fillers behave as inert materials (*in the viewpoint of asphalt technology*) because no reactions occur in this range. In Fig. 4. results of DSC analysis are summarized.

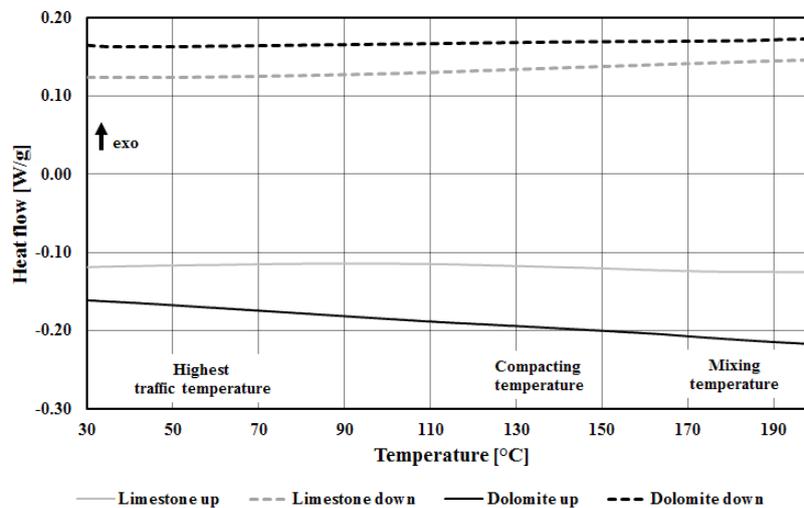


Figure 4. DSC curves of fillers

Heat flow curves recorded in the heating and cooling runs are shown. It can be concluded that there is no reaction, no significant enthalpy change occurs during the runs, no peaks are observed. As the diagram shows, no reaction occurred at the important temperatures.

Specific heat capacity can also be determined from DSC results, as Fig. 5. shows. As it can be seen dolomite has a higher specific heat capacity in the tested temperature ranges (30°C–200°C) than limestone. Specific heat capacity of fillers increased almost linearly in the tested ranges.

Heating microscope was used to measure the height change of compacted specimens during heating and it showed no change (Fig. 6.). The instrument is able to detect the silhouette of a lighted specimen by a digital camera. By image analysis the height change of the sample can be determined. In our case the height of the fillers was not changed during the test.

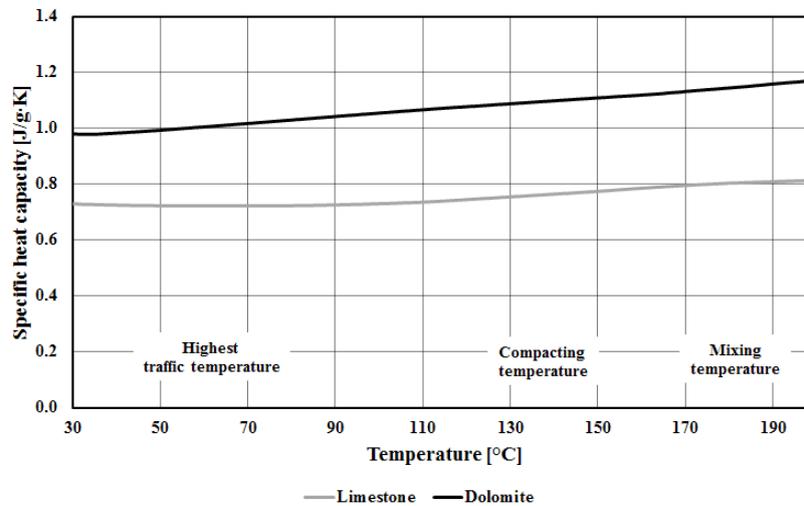


Figure 5. Specific heat capacity curves of fillers

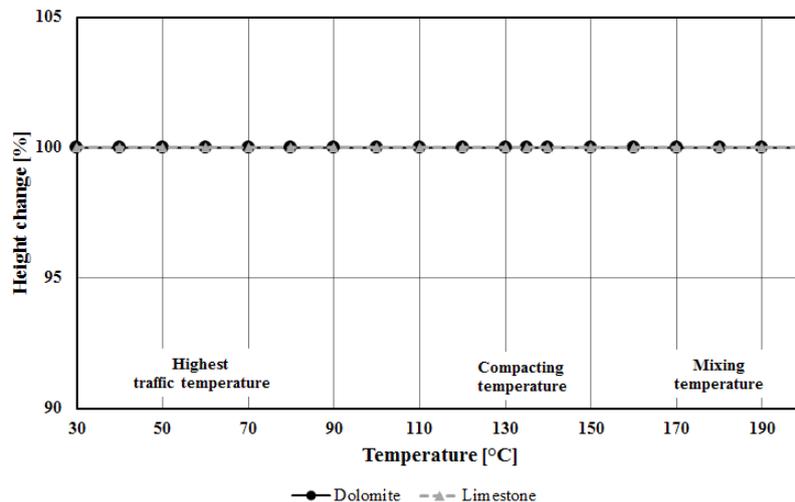


Figure 6. Height change of compacted fillers during heating

Dilatometric test by a precise laser dilatometer was also obtained. This method was used only on limestone filler, because dolomite was not able to compact. The reason of this is the particle size distribution of the mineral material (Fig.1. and Fig. 2.).

In Fig. 7. the relative length change curves (heating and cooling runs) are shown. At the maximum testing temperature ($T_{max}=200$ °C) the relative length change of the sample reached 0.15%. After cooling this change remained at 0.04 %, which is not a significant value. According to the dilatometric

test and heating microscopic tests it can be concluded that neither filler change its dimensions during the heating process.

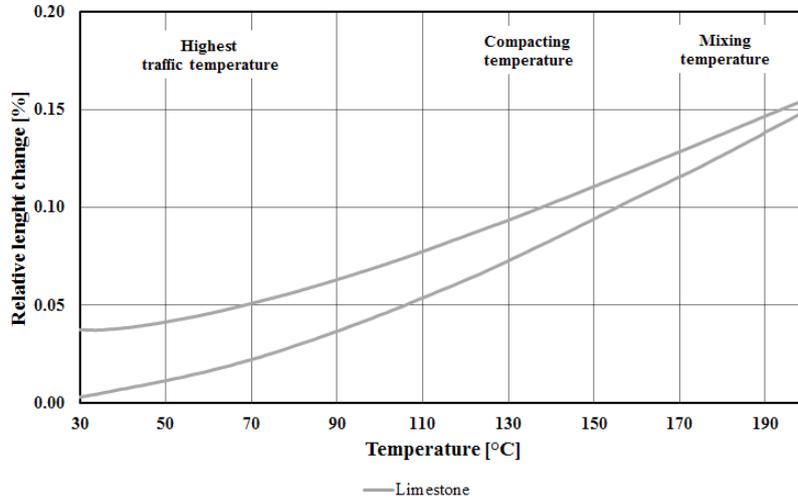


Figure 7. Relative length change of limestone filler

Fig. 8. shows the results of thermal conductivity measurements. 4 testing temperatures were used (20°C =room temperature, 60°C =highest traffic temperature, 135°C =compacting temperature and 180°C =asphalt mixing temperature). Thermal conductivity values are increased by the increase of temperature. Dolomite has slightly higher conductivity values than limestone, but this difference is not significant ($\sim 0.03 \text{ W/m}\cdot\text{K}$), except at room temperature. At this temperature the difference is almost two times higher.

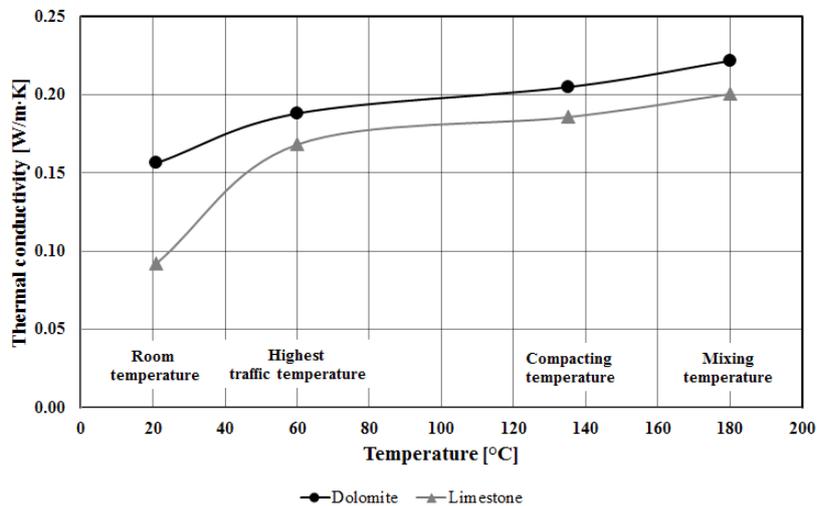


Figure 8. Thermal conductivity of fillers

4. Conclusions

During this research work two types of fine particle mineral materials were tested as asphalt fillers. Examinations of thermal properties of fillers were made by different techniques.

According to the particle size distribution, these mineral fillers can be characterized as polydisperse systems and they contain fine and coarse particles in different quantity by fraction.

The Authors have also observed the morphological features of the mineral materials. The morphology of fillers is various; dolomite has higher porosity in the particles, but does not contain much fine particles.

The samples were tested to reveal the thermal properties. According to the results, heat during the technological processes do not influence the properties of fillers (*no reactions, no change in length*). Difference was found only in specific heat capacity and in thermal conductivity. Dolomite has a higher specific heat capacity and thermal conductivity than limestone.

Acknowledgement

This work has been carried out as part of the TÁMOP-4.2.1.B-10/2/KONV-2010-0001 and TÁMOP-4.2.2/B-10/1-2010-0008 project within the framework of the New Hungarian Development Plan. The realization of this project is supported by the European Union, co-financed by the European Social Fund.

References

- [1] J. Chen 1997 *Journal of Materials, Concrete Structures and Pavements* **36** 269 (in Chinese)
- [2] A Kavussi, R G Hicks 1997 *Journal of Association of Asphalt Paving Technologists* **66** 153
- [3] B M Harris, K D Stuart 1995 *Journal of Association of Asphalt Paving Technologists* **64** 54
- [4] J Craus, I Ishai, A Sides 1978 *Journal of Association of Asphalt Paving Technologists* **47** 558
- [5] L A Gömze and Á Kovács 2005 *Építőanyag-JSBCM* **57** 34
<http://dx.doi.org/10.14382/epitoanyag-jsbcm.2005.7>
- [6] T B Moghaddam, H Baaj 2016 *Construction and Building Materials* **114** 805
- [7] U. Isacsson, H. Zeng 1997 *Construction and Building Materials* **11** 83
- [8] G. Devecseri 2010 *Építőanyag – Journal of Silicate Based and Composite Materials* **62 (1)** 23
<http://dx.doi.org/10.14382/epitoanyag-jsbcm.2010.5>