# FALLBACK AND BLACK HOLE PRODUCTION IN MASSIVE STARS 

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#### Abstract

The compact remnants of core-collapse supernovae—neutron stars and black holes—have properties that reflect both the structure of their stellar progenitors and the physics of the explosion. In particular, the masses of these remnants are sensitive to the density structure of the presupernova star and to the explosion energy. To a considerable extent, the final mass is determined by the "fallback," during the explosion, of matter that initially moves outward, yet ultimately fails to escape. We consider here the simulated explosion of a large number of massive stars ( $9-100 M_{\odot}$ ) of Population I (solar metallicity) and III (zero metallicity) and find systematic differences in the remnant mass distributions. As pointed out by Chevalier, supernovae in more compact progenitor stars have stronger reverse shocks and experience more fallback. For Population III stars above about $25 M_{\odot}$ and explosion energies less than $1.5 \times 10^{51}$ ergs, black holes are a common outcome, with masses that increase with increasing main-sequence mass up to a maximum hole mass, for very low explosion energy, of about $40 M_{\odot}$. If such stars produce primary nitrogen, however, their black holes are systematically smaller. For modern supernovae with nearly solar metallicity, black hole production is much less frequent and the typical masses, which depend sensitively on explosion energy, are smaller. The maximum black hole mass is about $15 M_{\odot}$. We explore the neutron star initial mass function for both populations and, for reasonable assumptions about the initial mass cut of the explosion, find good agreement with the average of observed masses of neutron stars in binaries. We also find evidence for a bimodal distribution of neutron star masses with a spike around $1.2 M_{\odot}$ (gravitational mass) and a broader distribution peaked around 1.4 $M_{\odot}$. Subject headings: black hole physics - hydrodynamics - stars: neutron - supernovae: general


## 1. INTRODUCTION

Colgate (1971) first introduced the idea of fallback in supernovae, attributing it to accretion in the rarefaction behind the outgoing shock. Chevalier (1989) discussed fallback in supernovae extensively and emphasized that greater accretion would occur in compact progenitors. For SN 1987A, a blue supergiant, Chevalier estimated a relatively large fallback mass of $\sim 0.1 M_{\odot}$ and, for the more common Type II supernovae from red supergiants, a value roughly 100 times smaller. He also found, using self-similarity arguments, that the accretion rate at late times when expansion dominated should scale as $t^{-5 / 3}$, and he emphasized the role of the reverse shock in fallback (see also Colgate 1988). Woosley \& Weaver (1995) studied fallback numerically in a variety of supernovae with different masses and compositions and emphasized black hole formation as an important outcome for stars of higher mass and lower metallicity, with important ramifications for their nucleosynthesis. MacFadyen et al. (2001) studied fallback numerically in a $25 M_{\odot}$ supernova with varying explosion energy and discussed the relevance of fallback for producing gamma-ray bursts.

Thus far, however, there has been no systematic study of fallback in stars with a very low metal content to determine the properties of gravitational remnants that might have existed following a first generation of stars. It has also been some time since the remnant masses of solar metallicity stars were systematically explored (Timmes et al. 1996), and no such studies have included the effects of mass loss. Calculations of fallback can be greatly influenced by the way the inner boundary is handled (MacFadyen

[^0]et al. 2001). This is particularly true in cases where a piston or reflecting inner boundary has been used to simulate the explosion and is still present in the calculation at late times (e.g., Woosley \& Weaver 1995). As we shall see, for modern supernovae that are red giants when they die, the error introduced by this artificial inner boundary is small, but it can become appreciable for zero metallicity stars with a much larger amount of fallback. Since the material that falls back must be subtracted from the element production for a given star, our results are also relevant for calculations of nucleosynthesis and (radioactive powered) light curves.

We do not study fallback in stars above $100 M_{\odot}$ and leave out the effects of rotation. Above $100 M_{\odot}$ and below $260 M_{\odot}$, nonrotating stars encounter the pair instability and either lose their outer layers before explosion (pulsational pair instability) or explode completely without fallback. Above $260 M_{\odot}$, they collapse to black holes (Heger \& Woosley 2002). We also study here only single stars, not binaries. The complications introduced by rotation and binary membership could be included in future studies. A very approximate mapping between the results of binary and single star evolution can be obtained by comparing two stars with the same final helium core (or carbon-oxygen core) and explosion energy (Wellstein \& Langer 1999; Fryer et al. 2002). Core masses for zero metallicity and solar metallicity stars are given here and in Woosley et al. (2002). However, one of our main results here is that the mass and radius of the hydrogen envelope also greatly affect the fallback and therefore the remnant mass. The structure of the entire star must be considered, not just its core mass. Similar caveats apply to the effects of rotation. Rotation tends to increase the helium core mass and thus make larger black holes for a given main-sequence mass. However, a correct calculation of the remnant mass involves not only the central engine (possibly affected by rotation) and the core mass but also the mass and radius of the hydrogen envelope.

We also do not include in our study any asymptotic giant branch stars. Stars less massive than about $9 M_{\odot}$ develop cores of either
carbon and oxygen or neon, oxygen, and magnesium that are increasingly degenerate. The core mass is thus limited by the Chandrasekhar mass, $1.39 M_{\odot}$ (for an electron mole number, $\left.Y_{e}=0.50\right)$. The fraction of such stars that produce neutron stars is probably small for solar metallicity (Poelarends et al. 2007) but could be large at low metallicity (A. J. T. Poelarends et al. 2008, in preparation). It is uncertain what fraction, if any, of these stars actually reach the Chandrasekhar mass without first losing their envelope to winds and instabilities, and those with carbonrich cores will produce thermonuclear supernovae, not neutron stars. For any that do make neutron stars, fallback is likely to be negligible and the baryonic masses of remnants will be $\sim 1.39 M_{\odot}$. Correcting for neutrino losses, the neutron star gravitational mass would be $\sim 1.26 M_{\odot}$. Because of uncertain statistics, such neutron stars are not included in our analysis but could be by others.

## 2. INITIAL MODELS

The supernova models studied here are taken from two recent surveys by A. Heger \& S. E. Woosley (2008, in preparation) and Woosley \& Heger (2007). In each case, stars of various masses and metallicities were evolved using the Kepler code (Weaver et al. 1978; Woosley et al. 2002) through all stable stages of nuclear burning until their iron cores became unstable to collapse. The stars were then exploded using pistons located at or near the edge of their iron cores. For a discussion of how the piston was located and moved, and for further details of these explosion models, see Woosley et al. (2002) and Woosley \& Heger (2007).

The first of these surveys examined the evolution and simulated explosion of approximately 120 massive stars with masses in the range $10-100 M_{\odot}$ and zero initial metallicity (hence Population III; Table 1). A. Heger \& S. E. Woosley (2008, in preparation) explored 12 different choices of explosion energy and piston location for each mass. While results are given for all of them in the tables, the discussion here focuses on just five. The model names are given by a capital letter " $Z$," for "zero" metallicity, followed by a letter indicating the piston location and explosion energy. Four of these, series ZB, ZD, ZG, and ZJ, had the piston located at that point in the star where the entropy equals $4.0 k_{\mathrm{B}}$ baryon $^{-1}$ (typically this occurs at the base of the oxygenburning shell) and with kinetic energies of $0.6,1.2,2.4$, and 10 B , respectively (henceforth $1 \mathrm{~B}=1$ bethe $=10^{51}$ ergs). Series P had the piston located deeper in, at the edge of the deleptonized core (where $Y_{e}$ drops precipitously below 0.5 due to electron capture), and had an explosion energy of 1.2 B. Note that the explosion energies quoted here are not the energy input by the piston, but rather the kinetic energy of the ejecta at infinity.

The second survey treated a coarser grid of stellar masses (31 stars) with solar metallicity and masses in the range $12-100 M_{\odot}$ (Table 2). This survey is more appropriate to supernovae today in the Milky Way. Greatest attention is paid here to series SA, which had the piston at the place in the star where the entropy per baryon, $S / N_{\mathrm{A}} k$, equals 4.0 and with an explosion energy of 1.2 B . Except for metallicity effects then, series ZD and SA are directly comparable. Three other explosion models were also considered: SB, which had the piston at the entropy $=4.0$ point but had an explosion energy of 2.4 B ; SC, with the piston at the edge of the iron core (mass fraction of nuclei heavier than chromium greater than $50 \%$ ) and an explosion energy of 1.2 B ; and SD , with the piston at the edge of the iron core and an explosion energy of 2.4 B .

Models SC are thus the solar metallicity counterparts of models ZP but with a slight difference. The ZP models put the piston at the edge of the deleptonized core, while the SC models put the piston at the edge of the iron core. The difference between these
two cores in a given model is usually quite small, and we do not think it has a major effect on the outcome.

Tables 1 and 2 give an overview of these presupernova models. See also A. Heger \& S. E. Woosley (2008, in preparation) and Woosley \& Heger (2007). For the solar case, a few additional models were computed at low and high mass using the same code and physics as the original surveys. The tables give the initial mass of the star, its final mass (for the Population III stars, this is identical to the initial mass), the mass of the location where an entropy of $S / N_{\mathrm{A}} k=4.0$ is reached $\left(M_{S=4}\right)$, the size of the core where extensive electron capture has occurred ( $Y_{e}$ core), the binding energies outside these two cores (binding energy minus internal energy; $\left.\mathrm{BE}_{Y_{e} \text { core }}, \mathrm{BE}_{S=4}\right)$, and the final radius of the star ( $R_{\text {eff }}$ ). In the $R_{\text {eff }}$ column, "WNL" indicates a hydrogen-rich Wolf-Rayet (WR) star and "WC"/"WO" indicate early-type hydrogen-free WR stars. Such WR stars have optically thick winds with a photospheric "effective radius" located in this wind regime. Among the hydrogenfree WR stars, we found only the carbon-rich and oxygen-rich subtypes (WC and WO) at presupernova, but no early-type hydrogen-free WR stars that only display the pure CNO-processed N-rich He layer (WNE stars). There may be a very small transition regime between 40 and $45 M_{\odot}$ where such WNE stars occur.

At $45 M_{\odot}$, WO stars start to be produced as material from a late helium-burning stage in which oxygen dominates over carbon is exposed to the surface. At initial masses above $\sim 60 M_{\odot}$ carbon dominates over oxygen at the time the stars explode. The final mass of the star becomes smaller having lower WR mass-loss rates at the end, and the stars lose mass from earlier phases of helium core burning. Both effects increase the final carbon-tooxygen ratio at the surface.

## 3. CALCULATIONS

Calculations were carried out using Pangu, a one-dimensional hydrodynamics code based on the second-order semidiscrete finite-difference central scheme of Kurganov \& Tadmor (2000). Time evolution is carried out by a third-order total variation diminishing Runge-Kutta method (Shu \& Osher 1989). We extended the scheme to spherical coordinates based on the conservative form of hydrodynamics equations. The treatment of spherical coordinates is the same as that in the RAM code (Zhang \& MacFadyen 2006). In spherical coordinates, extra source terms are added to the equations. Geometric correction to the surface area and volume of discretized numerical cells is applied when the numerical flux is used to update conserved variables (density, momentum, and total energy) in the cells.

Gravity is implemented as source terms of the hydrodynamics equations. A point mass is placed at the center of the grid. The gravitational force at a grid point is calculated from the enclosed mass, which includes the central point mass and mass of the material on the computational grid. The central point mass is being updated by keeping track of the mass flux across the inner boundary.

The supernova models were linked from the Kepler code, in which they were initially calculated, to the Pangu code 100 s after the shock wave had been initiated. This typically corresponded to a time when explosive nucleosynthesis had ended and the outgoing shock was just exiting the core of helium and heavy elements, before it had encountered any appreciable fraction of the hydrogen envelope. The reverse shock had thus not yet developed and, for the explosion energies considered, no fallback had yet occurred.

An outflow boundary condition was used at the inner boundary. That is, the ghost cells are simple duplicates of the first numerical cell on the grid. This type of boundary is very simple to implement. A potential problem of essentially any numerical boundary is that small errors at the boundary could accumulate

TABLE 1
Summary of $Z=0$ Presupernova Model Data

| $\begin{aligned} & \text { Mass } \\ & \left(M_{\odot}\right) \end{aligned}$ | $\begin{gathered} M_{S=4} \\ \left(M_{\odot}\right) \end{gathered}$ | $Y_{e}$ Core ( $M_{\odot}$ ) | $\mathrm{BE}_{Y_{e} \text { core }}$ <br> (B) | $\mathrm{BE}_{S=4}$ <br> (B) | $\begin{aligned} & R_{\mathrm{eff}} \\ & \left(R_{\odot}\right) \end{aligned}$ | Mass $\left(M_{\odot}\right)$ | $\begin{gathered} M_{S=4} \\ \left(M_{\odot}\right) \end{gathered}$ | $Y_{e}$ Core ( $M_{\odot}$ ) | $\mathrm{BE}_{Y_{e} \text { core }}$ <br> (B) | $\mathrm{BE}_{S=4}$ <br> (B) | $\begin{aligned} & R_{\mathrm{eff}} \\ & \left(R_{\odot}\right) \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10.0......... | 1.28 | 1.27 | 0.09 | 0.09 | 62 | 18.7.......... | 1.55 | 1.41 | 0.66 | 0.48 | 10 |
| 10.2......... | 1.38 | 1.18 | 0.27 | 0.04 | 38 | 18.8......... | 1.57 | 1.42 | 0.69 | 0.50 | 11 |
| 10.4......... | 1.32 | 1.18 | 0.34 | 0.11 | 34 | 18.9........ | 1.63 | 1.47 | 0.76 | 0.56 | 11 |
| 10.5......... | 1.41 | 1.20 | 0.34 | 0.07 | 27 | 19.0......... | 1.63 | 1.44 | 0.80 | 0.57 | 11 |
| 10.6......... | 1.40 | 1.20 | 0.30 | 0.06 | 21 | 19.2........ | 1.59 | 1.44 | 0.72 | 0.53 | 10 |
| 10.7......... | 1.41 | 1.19 | 0.35 | 0.08 | 20 | 19.4......... | 1.56 | 1.44 | 0.70 | 0.54 | 10 |
| 10.8......... | 1.34 | 1.17 | 0.39 | 0.13 | 19 | 19.6.......... | 1.63 | 1.45 | 0.79 | 0.57 | 11 |
| 10.9......... | 1.43 | 1.25 | 0.27 | 0.08 | 17 | 19.8......... | 1.61 | 1.43 | 0.79 | 0.58 | 10 |
| 11.0......... | 1.42 | 1.33 | 0.23 | 0.12 | 15 | 20.0......... | 1.46 | 1.46 | 0.62 | 0.61 | 13 |
| 11.1......... | 1.31 | 1.27 | 0.22 | 0.14 | 18 | 20.5......... | 1.64 | 1.46 | 0.79 | 0.56 | 13 |
| 11.2......... | 1.35 | 1.19 | 0.37 | 0.14 | 14 | 21.0......... | 1.50 | 1.49 | 0.71 | 0.70 | 10 |
| 11.3......... | 1.47 | 1.18 | 0.43 | 0.11 | 14 | 21.5....... | 1.61 | 1.45 | 0.80 | 0.59 | 14 |
| 11.4......... | 1.48 | 1.22 | 0.43 | 0.16 | 18 | 22.0....... | 1.52 | 1.36 | 0.92 | 0.72 | 11 |
| 11.5......... | 1.35 | 1.35 | 0.15 | 0.15 | 13 | 22.5......... | 1.49 | 1.43 | 0.68 | 0.58 | 11 |
| 11.6......... | 1.34 | 1.34 | 0.16 | 0.16 | 12 | 23.0......... | 1.63 | 1.46 | 0.90 | 0.68 | 11 |
| 11.7......... | 1.38 | 1.23 | 0.41 | 0.17 | 13 | 23.5........ | 1.92 | 1.58 | 1.19 | 0.87 | 12 |
| 11.8......... | 1.49 | 1.24 | 0.40 | 0.16 | 12 | 24.0......... | 2.07 | 1.64 | 1.34 | 0.98 | 12 |
| 11.9......... | 1.54 | 1.26 | 0.34 | 0.13 | 11 | 24.5........ | 2.20 | 1.67 | 1.47 | 1.07 | 13 |
| 12.0......... | 1.30 | 1.26 | 0.23 | 0.15 | 12 | 25.0...... | 2.17 | 1.59 | 1.43 | 1.02 | 19 |
| 12.2......... | 1.51 | 1.26 | 0.44 | 0.19 | 14 | 25.5......... | 1.87 | 1.62 | 1.08 | 0.82 | 14 |
| 12.4......... | 1.46 | 1.31 | 0.44 | 0.24 | 10 | 26.0........ | 1.74 | 1.53 | 1.15 | 0.90 | 15 |
| 12.6......... | 1.50 | 1.23 | 0.49 | 0.20 | 10 | 26.5......... | 1.80 | 1.54 | 1.19 | 0.90 | 16 |
| 12.8......... | 1.41 | 1.31 | 0.38 | 0.21 | 10 | 27.0......... | 1.73 | 1.52 | 1.12 | 0.89 | 18 |
| 13.0......... | 1.40 | 1.37 | 0.25 | 0.21 | 19 | 27.5......... | 1.59 | 1.46 | 1.14 | 0.96 | 16 |
| 13.2......... | 1.54 | 1.31 | 0.43 | 0.23 | 10 | 28.0......... | 1.60 | 1.46 | 1.06 | 0.88 | 21 |
| 13.4......... | 1.57 | 1.35 | 0.43 | 0.21 | 9.1 | 28.5......... | 1.62 | 1.43 | 1.22 | 0.98 | 19 |
| 13.6......... | 1.42 | 1.41 | 0.27 | 0.27 | 10 | 29.0.... | 1.72 | 1.49 | 1.26 | 1.01 | 15 |
| 13.8......... | 1.45 | 1.37 | 0.44 | 0.32 | 9.0 | 29.5...... | 1.70 | 1.45 | 1.29 | 1.00 | 15 |
| 14.0......... | 1.57 | 1.37 | 0.52 | 0.29 | 9.0 | 30.0....... | 1.75 | 1.50 | 1.24 | 0.97 | 20 |
| 14.2......... | 1.58 | 1.38 | 0.53 | 0.30 | 9.0 | 30.5...... | 1.77 | 1.51 | 1.36 | 1.09 | 14 |
| 14.4......... | 1.62 | 1.39 | 0.56 | 0.31 | 9.2 | 31.0....... | 1.84 | 1.54 | 1.46 | 1.15 | 15 |
| 14.6......... | 1.56 | 1.40 | 0.55 | 0.36 | 9.0 | 31.5........ | 1.93 | 1.58 | 1.56 | 1.24 | 18 |
| 14.8......... | 1.56 | 1.41 | 0.55 | 0.37 | 9.0 | 32.0......... | 1.94 | 1.57 | 1.60 | 1.27 | 15 |
| 15.0......... | 1.43 | 1.28 | 0.53 | 0.30 | 10 | 32.5......... | 1.98 | 1.59 | 1.65 | 1.30 | 18 |
| 15.2......... | 1.45 | 1.33 | 0.49 | 0.32 | 10 | 33.0......... | 2.08 | 1.63 | 1.77 | 1.41 | 16 |
| 15.4......... | 1.43 | 1.31 | 0.50 | 0.31 | 10 | 33.5......... | 2.12 | 1.64 | 1.79 | 1.42 | 24 |
| 15.6......... | 1.46 | 1.36 | 0.52 | 0.38 | 8.9 | 34.0...... | 2.12 | 1.64 | 1.85 | 1.48 | 16 |
| 15.8......... | 1.55 | 1.36 | 0.62 | 0.40 | 8.7 | 34.5....... | 2.19 | 1.65 | 1.91 | 1.52 | 19 |
| 16.0......... | 1.58 | 1.41 | 0.62 | 0.42 | 8.9 | 35.0.. | 2.24 | 1.66 | 1.95 | 1.56 | 21 |
| 16.2......... | 1.61 | 1.42 | 0.66 | 0.44 | 8.9 | 36.0.... | 2.33 | 1.80 | 2.06 | 1.73 | 17 |
| 16.4......... | 1.63 | 1.45 | 0.67 | 0.46 | 8.8 | 37.0... | 2.25 | 1.82 | 2.20 | 1.96 | 18 |
| 16.6......... | 1.63 | 1.44 | 0.68 | 0.47 | 9.1 | 38.0... | 2.23 | 1.66 | 1.87 | 1.49 | 59 |
| 16.8......... | 1.74 | 1.32 | 0.84 | 0.48 | 10 | 39.0....... | 2.24 | 1.78 | 1.76 | 1.44 | 739 |
| 17.0......... | 1.76 | 1.35 | 0.87 | 0.52 | 9.0 | 40.0........ | 2.16 | 1.88 | 2.60 | 2.50 | 23 |
| 17.1......... | 1.77 | 1.37 | 0.86 | 0.53 | 8.9 | 41.0....... | 2.27 | 1.85 | 2.31 | 2.10 | 50 |
| 17.2......... | 1.74 | 1.34 | 0.87 | 0.52 | 9.1 | 42.0....... | 2.24 | 1.93 | 2.49 | 2.35 | 30 |
| 17.3......... | 1.82 | 1.39 | 0.84 | 0.53 | 9.0 | 43.0....... | 1.97 | 1.75 | 2.82 | 2.79 | 26 |
| 17.4......... | 1.50 | 1.37 | 0.63 | 0.45 | 10 | 44.0.......... | 1.64 | 1.64 | 2.86 | 2.86 | 23 |
| 17.5......... | 1.82 | 1.40 | 0.85 | 0.54 | 9.1 | 45.0.......... | 2.20 | 1.91 | 2.30 | 2.18 | 896 |
| 17.6......... | 1.87 | 1.46 | 0.85 | 0.59 | 10 | 50.0......... | 2.34 | 1.82 | 2.08 | 1.80 | 2020 |
| 17.7.......... | 1.73 | 1.58 | 0.64 | 0.52 | 9.1 | 55.0......... | 1.91 | 1.91 | 2.82 | 2.82 | 2048 |
| 17.8......... | 1.83 | 1.40 | 0.91 | 0.59 | 9.1 | 60.0......... | 1.91 | 1.91 | 3.21 | 3.21 | 150 |
| 17.9......... | 1.84 | 1.41 | 0.87 | 0.58 | 9.3 | 65.0......... | 1.97 | 1.95 | 3.16 | 3.15 | 1830 |
| 18.0......... | 1.49 | 1.38 | 0.55 | 0.40 | 26 | 70.0......... | 2.18 | 1.96 | 3.87 | 3.72 | 184 |
| 18.1......... | 1.53 | 1.39 | 0.65 | 0.46 | 11 | 75.0.......... | 2.15 | 2.04 | 3.71 | 3.63 | 2305 |
| 18.2......... | 1.54 | 1.41 | 0.84 | 0.70 | 9.4 | 80.0......... | 2.26 | 2.14 | 3.88 | 3.81 | 2334 |
| 18.3......... | 1.70 | 1.43 | 0.88 | 0.69 | 9.5 | 85.0......... | 2.42 | 2.03 | 4.17 | 4.05 | 2526 |
| 18.4......... | 1.51 | 1.40 | 0.48 | 0.33 | 51 | 90.0.......... | 2.40 | 1.54 | 4.11 | 3.92 | 2648 |
| 18.5......... | 1.55 | 1.41 | 0.68 | 0.50 | 11 | 95.0......... | 2.53 | 2.04 | 4.26 | 4.11 | 1214 |
| 18.6......... | 1.51 | 1.41 | 0.57 | 0.42 | 22 | 100.0........ | 2.02 | 1.44 | 3.34 | 2.92 | 1.3 |

TABLE 2
Summary of Solar Metallicity Presupernova Model Data

| Mass <br> $\left(M_{\odot}\right)$ | $\begin{gathered} M_{\text {final }} \\ \left(M_{\odot}\right) \end{gathered}$ | $\begin{gathered} M_{S=4} \\ \left(M_{\odot}\right) \end{gathered}$ | Fe Core ( $M_{\odot}$ ) | $\mathrm{BE}_{\mathrm{Fe} \text { core }}$ (B) | $\mathrm{BE}_{S=4}$ <br> (B) | $\begin{aligned} & R_{\text {eff }} \\ & \left(R_{\odot}\right) \end{aligned}$ | Mass $\left(M_{\odot}\right)$ | $\begin{gathered} M_{\text {final }} \\ \left(M_{\odot}\right) \end{gathered}$ | $\begin{gathered} M_{S=4} \\ \left(M_{\odot}\right) \end{gathered}$ | Fe Core $\left(M_{\odot}\right)$ | $\mathrm{BE}_{\mathrm{Fe} \text { core }}$ (B) | $\mathrm{BE}_{S=4}$ <br> (B) | $\begin{aligned} & R_{\text {eff }} \\ & \left(R_{\odot}\right) \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10.0............... | 9.70 | 1.35 | 1.30 | 0.19 | 0.11 | 458 | 27.0...... | 15.21 | 1.74 | 1.52 | 1.08 | 0.83 | 1449 |
| 11.0............... | 10.67 | 1.37 | 1.31 | 0.23 | 0.19 | 558 | 28.0. | 15.17 | 1.54 | 1.48 | 1.09 | 1.03 | 1466 |
| 12.0............... | 10.91 | 1.53 | 1.36 | 0.30 | 0.17 | 618 | 29.0.............. | 14.17 | 1.64 | 1.47 | 1.05 | 0.85 | 1477 |
| 13.0................ | 11.40 | 1.55 | 1.40 | 0.46 | 0.28 | 709 | 30.0.... | 13.88 | 1.73 | 1.50 | 1.08 | 0.84 | 1489 |
| 14.0............... | 12.01 | 1.70 | 1.51 | 0.44 | 0.28 | 759 | 31.0.............. | 13.63 | 1.70 | 1.48 | 1.12 | 0.86 | 1446 |
| 15.0............... | 12.79 | 1.81 | 1.48 | 0.53 | 0.32 | 803 | 32.0.............. | 13.41 | 1.78 | 1.52 | 1.22 | 0.94 | 1362 |
| 16.0............... | 13.59 | 1.50 | 1.37 | 0.51 | 0.34 | 839 | 33.0.............. | 13.24 | 1.84 | 1.55 | 1.30 | 1.01 | 1296 |
| 17.0............... | 14.12 | 1.54 | 1.40 | 0.57 | 0.39 | 883 | 35.0.............. | 13.66 | 1.97 | 1.63 | 1.47 | 1.16 | WNL |
| 18.0................ | 14.82 | 1.89 | 1.49 | 0.70 | 0.37 | 942 | 40.0.............. | 15.34 | 2.34 | 1.82 | 1.93 | 1.61 | WNL |
| 19.0................ | 15.48 | 1.64 | 1.45 | 0.68 | 0.45 | 990 | 45.0.............. | 13.02 | 2.27 | 1.79 | 1.76 | 1.44 | WO |
| 20.0............... | 15.93 | 1.82 | 1.54 | 0.89 | 0.60 | 1032 | 50.0.............. | 9.82 | 1.70 | 1.49 | 1.05 | 0.81 | WO |
| 21.0............... | 16.16 | 1.46 | 1.46 | 0.48 | 0.47 | 1085 | 55.0.............. | 9.38 | 1.65 | 1.47 | 1.03 | 0.82 | WO |
| 22.0............... | 16.16 | 1.84 | 1.54 | 0.95 | 0.65 | 1139 | 60.0.. | 7.29 | 1.60 | 1.45 | 0.71 | 0.53 | WO |
| 23.0............... | 16.37 | 2.12 | 1.73 | 1.18 | 0.86 | 1207 | 70.0. | 6.41 | 1.72 | 1.50 | 0.82 | 0.56 | WC |
| 24.0............... | 16.22 | 2.05 | 1.70 | 1.17 | 0.87 | 1270 | 80.0............. | 6.37 | 1.66 | 1.48 | 0.76 | 0.54 | WC |
| 25.0............... | 15.84 | 1.90 | 1.59 | 1.16 | 0.86 | 1329 | 100.0............ | 6.04 | 1.81 | 1.54 | 0.81 | 0.58 | WC |
| 26.0............... | 15.41 | 1.73 | 1.54 | 0.97 | 0.74 | 1386 | 120.0............ | 6.00 | 1.60 | 1.43 | 0.68 | 0.48 | WC |

and affect the calculation. To avoid the problem, one should make sure that the flow across the boundary is supersonic. Thus, the information at the boundary cannot propagate outward and affect the upstream fluid. In our calculations, the inner boundaries are chosen to be small enough to ensure the supersonic condition. However, it could be expensive to use a very small radius for the inner boundary because of the constraint of the Courant-Friedrichs-Lewy condition. Fortunately, the sound speed at the inner boundary is decreasing during fallback due to the decrease of temperature, whereas the infall velocity is increasing during fallback. Therefore, the sonic point is moving outward over the time.

Calculations are performed in two steps to save computing time. In the first step, the numerical grid has an inner boundary at $r=10^{9} \mathrm{~cm}$, which is also the inner boundary of the initial Kepler models, and an outer boundary at $r=10^{14} \mathrm{~cm}$. A logarithmic grid with 1000 zones is used for the $r$-direction. The region outside the star is filled with a low-density medium with a pressure of $p=10 \mathrm{dyn} \mathrm{cm}^{-2}$, a density of $\rho=10^{-12} \mathrm{~g} \mathrm{~cm}^{-3}$, and zero velocity. The calculation is run to $t=10^{5} \mathrm{~s}$. Then the model is remapped to a new grid for the second step of calculations. For red giants in which the forward shock could have moved beyond the outer boundary at $r=10^{14} \mathrm{~cm}$ already at $t=10^{5} \mathrm{~s}$, the link to the second step is at an earlier time (e.g., $t=5 \times 10^{4} \mathrm{~s}$ ) so that the forward shock still presents at the second step.

The grid for the second phase of calculations also has 1000 logarithmic zones, but the boundaries are at $r=10^{10}$ and $10^{16} \mathrm{~cm}$. Again the outside medium is set to a constant state with a pressure of $p=10$ dyn $\mathrm{cm}^{-2}$, a density of $\rho=10^{-12} \mathrm{~g} \mathrm{~cm}^{-3}$, and zero velocity. The second step of the calculation is run to at least $t=10^{6} \mathrm{~s}$. Then the simulation continues until the accretion rate is below $10^{-8} M_{\odot} \mathrm{s}^{-1}$ or it has reached $t=2.0 \times 10^{6} \mathrm{~s}$.

## 4. RESULTS

### 4.1. Fallback in Population III Supernovae

Two distinguishing properties of evolved Population III stars are that they have lost little mass and also typically have more compact envelopes than modern stars. Most of them die as hot blue stars. In some of the more massive stars, however, penetration of the convective helium-burning core into the hydrogen en-
velope leads to the enrichment of the latter with supersolar abundances of carbon and nitrogen. Hydrogen shell burning by the CNO cycle then expands the star to supergiant proportions. Another special case is stars around $100 M_{\odot}$, which begin to encounter the pulsational pair instability. Strong pulses lead to the ejection of the entire hydrogen envelope and even parts of the helium core before the final core collapse (e.g., Heger \& Woosley 2002). This weakens the reverse shock in such stars.

In the usual case, however, the explosion of Population III stars is accompanied by a stronger reverse shock and much more fallback than in their solar counterparts. Since mass loss is likely to be greatly reduced in stars with no metals (Kudritzki 2002; Mokiem et al. 2007; although see also Ekström et al. 2006), higher main-sequence mass implies a monotonically increasing helium core mass when the star dies, and along with it the potential for making more massive compact remnants, especially if the explosion energy is small. This is particularly interesting since several current simulations of primordial star formation (e.g., O'Shea \& Norman 2007) predict rather high initial masses for these first stars. While not studied here, it is expected that still more massive stars (i.e., much above $100 M_{\odot}$ ) will encounter an increasingly violent pair instability leading to the complete disruption of the star and, eventually, above about $260 M_{\odot}$, the direct production of massive black holes without an initial supernova explosion (Heger \& Woosley 2002). These limiting masses would be reduced by rotation.

### 4.1.1. Hydrodynamics in a Representative Case

Figure 1 shows the pressure, density, and velocity profiles at 100, 200, and 1000 s as calculated in a typical Population III model, Z25D, using both Pangu and Kepler. Both the forward and reverse shocks are clearly visible in the pressure and velocity plots. The reverse shock forms as the expanding helium core runs into the star's hydrogen envelope (where the quantity $\rho r^{3}$ increases; Woosley \& Weaver 1995) and is decelerated. The hydrogen envelope in the presupernova star had its base at $1.5 \times 10^{10} \mathrm{~cm}$. With time the reverse shock moves inward in mass but outward in radius. Starting at the edge of the helium core at $7.6 M_{\odot}$, by 1000 s the reverse shock has moved into $3.3 M_{\odot}$. The forward shock at this time is located at $19.19 M_{\odot}$ and will shortly exit the star.


Fig. 1.-Pressure, density, and velocity profiles at 100 (red lines and squares), 200 (green lines and plus signs), and 1000 s (blue lines and stars) in model Z25D calculated using Kepler (symbols) and Pangu (solid lines). The agreement is excellent except near the origin. Since Pangu uses a more realistic representation of the fallback at small radii, its results are preferred. The inner boundary in Pangu is inside the sonic radius at all times.

In the part of the star that is sonically disconnected from the origin, the results of Kepler and Pangu are in very good agreement. As time passes, however, there is an increasing discrepancy near the origin where Pangu gives much higher collapse speeds than Kepler, since the latter increasingly feels the effect of the reflecting inner boundary held fixed at $1.0 \times 10^{9} \mathrm{~cm}$. The inner boundary in Pangu is also located at $1.0 \times 10^{9} \mathrm{~cm}$, but matter can flow through it without deceleration. The sonic radius at 1000 s is located at $3.27 \times 10^{10} \mathrm{~cm}$ where the sound speed is $488 \mathrm{~km} \mathrm{~s}^{-1}$.

Figure 2 gives the accretion rate as a function of time calculated by Pangu for this model. There are clearly four stages to the accretion: (1) an early rapid accretion of material that failed to achieve escape speed on the first try, (2) a decline in accretion rate to an asymptotic dependence on $t^{-5 / 3}$ as appropriate for free expansion (Chevalier 1989), (3) a greatly enhanced fallback as the reverse shock arrives at the core at $1.17 \times 10^{4} \mathrm{~s}$, and (4) a final stage of free expansion.

The final value of the remnant masses from Pangu can be determined in two ways. After a sufficiently long time (i.e., a while after the reverse shock has arrived at the center), the inner part of the supernova will approach its asymptotic behavior. Thus, the profiles of pressure, density, and velocity near the center are very simple for the last dump of the simulation. Both density and pressure have a negative gradient. The velocity is negative near the center and increases monotonically outward. In the first method,


Fig. 2.-Accretion rates and central point mass for models Z25D (blue lines) and S25A (red lines). The dashed line shows the asymptotic accretion rate, $\sim t^{-5 / 3}$. Note the prominent appearance of the reverse shock at the core at about $10^{4} \mathrm{~s}$ in Z25D. For model S25A the reverse shock has not arrived back at the origin at $10^{6} \mathrm{~s}$ and, in fact, is still moving outward in space. Its eventual arrival will have little consequence for the mass of the remnant. Note a period of about 1000 s during which the initial accretion rate is nearly constant.
a lower bound and upper bound of the final remnant mass can be estimated from the last dump. All material with a negative velocity will fall into the center. This gives us a lower bound estimate of the final remnant mass. All material with a velocity larger than the escape velocity will be able to escape. This gives us an upper bound estimate of the mass. Our first estimate is the average of the two bounds.

The second estimate is based on the asymptotic behavior of the accretion rate, $\dot{M} \sim t^{-5 / 3}$. Using the point mass and accretion rate at the last dump of the simulation, we can get the second estimate by a simple analytic integration. For most models, the two estimates are almost the same. For example, the difference is less than $0.01 M_{\odot}$ in 958 out of 1440 Z-series and 123 out of 124 S-series models. This gives us more confidence about our results. In principle, the two estimates should be identical provided that the simulation is run long enough. To determine which estimate is more accurate, we did the two estimates using earlier dumps. We found that the second estimate was generally more accurate. In this paper we use the values of the second estimate. Tables 3 and 4 show the results of the final remnant masses calculated by Pangu. In the end, Pangu gave a remnant mass of $4.157 M_{\odot}$ for this star (Z25D), whereas the corresponding calculation with Kepler gave $2.173 M_{\odot}$.

### 4.1.2. Remnant Masses for the Population III Survey

Figures 3 and 4 give the remnant masses for the Population III survey. Above about $35 M_{\odot}$ the results are influenced by the

TABLE 3
$Z=0$ Baryonic Remnant Masses

|  |  |  |  |  |  | Remnant | Mass ( $M_{\odot}$ ) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Initial <br> Mass <br> $\left(M_{\odot}\right)$ | $\begin{gathered} \text { Run ZA, } \\ E=0.3 \mathrm{~B}, \\ \text { Piston at } S=4 \end{gathered}$ | $\begin{gathered} \text { Run ZB, } \\ E=0.6 \text { B, } \\ \text { Piston at } S=4 \end{gathered}$ | $\begin{gathered} \text { Run ZC, } \\ E=0.9 \mathrm{~B}, \\ \text { Piston at } S=4 \end{gathered}$ | $\begin{gathered} \text { Run ZD, } \\ E=1.2 \mathrm{~B} \text {, } \\ \text { Piston at } S=4 \end{gathered}$ | $\begin{gathered} \text { Run ZE, } \\ E=1.5 \mathrm{~B}, \\ \text { Piston at } S=4 \end{gathered}$ | $\begin{gathered} \text { Run ZF, } \\ E=1.8 \mathrm{~B}, \\ \text { Piston at } S=4 \end{gathered}$ | $\begin{gathered} \text { Run ZG, } \\ E=2.4 \mathrm{~B}, \\ \text { Piston at } S=4 \end{gathered}$ | $\begin{gathered} \text { Run } \mathrm{ZH}, \\ E=3.0 \mathrm{~B}, \\ \text { Piston at } S=4 \end{gathered}$ | $\begin{gathered} \text { Run ZI, } \\ E=5.0 \mathrm{~B}, \\ \text { Piston at } S=4 \end{gathered}$ | $\begin{gathered} \text { Run ZJ, } \\ E=10.0 \mathrm{~B}, \\ \text { Piston at } S=4 \end{gathered}$ | $\begin{gathered} \text { Run ZP, } \\ E=1.2 \mathrm{~B}, \end{gathered}$ <br> Piston at $Y_{e}$ Core | $\begin{gathered} \text { Run ZV, } \\ E=10.0 \mathrm{~B} \text {, } \end{gathered}$ <br> Piston at $Y_{e}$ Core |
| 10.0...... | 1.37 | 1.28 | 1.28 | 1.28 | 1.28 | 1.28 | 1.28 | 1.28 | 1.27 | 1.27 | 1.28 | 1.27 |
| 10.2...... | 1.39 | 1.38 | 1.38 | 1.38 | 1.38 | 1.38 | 1.38 | 1.38 | 1.38 | 1.38 | 1.18 | 1.18 |
| 10.4...... | 1.60 | 1.33 | 1.32 | 1.32 | 1.32 | 1.32 | 1.32 | 1.32 | 1.32 | 1.32 | 1.20 | 1.18 |
| 10.5...... | 1.53 | 1.43 | 1.42 | 1.42 | 1.41 | 1.41 | 1.41 | 1.41 | 1.41 | 1.41 | 1.20 | 1.20 |
| 10.6...... | 1.44 | 1.41 | 1.41 | 1.40 | 1.40 | 1.40 | 1.40 | 1.40 | 1.40 | 1.40 | 1.20 | 1.20 |
| 10.7...... | 1.55 | 1.43 | 1.42 | 1.42 | 1.41 | 1.41 | 1.41 | 1.41 | 1.41 | 1.41 | 1.20 | 1.19 |
| 10.8...... | 1.60 | 1.49 | 1.36 | 1.35 | 1.34 | 1.34 | 1.34 | 1.34 | 1.34 | 1.34 | 1.18 | 1.17 |
| 10.9...... | 1.59 | 1.46 | 1.45 | 1.44 | 1.43 | 1.43 | 1.43 | 1.43 | 1.43 | 1.43 | 1.27 | 1.25 |
| 11.0...... | 1.64 | 1.57 | 1.47 | 1.44 | 1.43 | 1.43 | 1.43 | 1.43 | 1.43 | 1.43 | 1.35 | 1.33 |
| 11.1...... | 1.96 | 1.40 | 1.32 | 1.31 | 1.31 | 1.31 | 1.31 | 1.31 | 1.31 | 1.31 | 1.28 | 1.27 |
| 11.2...... | 1.71 | 1.60 | 1.39 | 1.36 | 1.36 | 1.35 | 1.35 | 1.35 | 1.35 | 1.35 | 1.23 | 1.19 |
| 11.3...... | 1.76 | 1.51 | 1.49 | 1.48 | 1.47 | 1.47 | 1.47 | 1.47 | 1.47 | 1.47 | 1.26 | 1.18 |
| 11.4...... | 2.03 | 1.74 | 1.53 | 1.50 | 1.49 | 1.49 | 1.49 | 1.48 | 1.48 | 1.48 | 1.27 | 1.22 |
| 11.5...... | 1.80 | 1.64 | 1.40 | 1.36 | 1.36 | 1.36 | 1.35 | 1.35 | 1.35 | 1.35 | 1.36 | 1.35 |
| 11.6...... | 1.89 | 1.67 | 1.41 | 1.36 | 1.35 | 1.35 | 1.35 | 1.34 | 1.34 | 1.34 | 1.36 | 1.34 |
| 11.7...... | 1.93 | 1.72 | 1.52 | 1.42 | 1.39 | 1.39 | 1.38 | 1.38 | 1.38 | 1.38 | 1.54 | 1.23 |
| 11.8...... | 2.03 | 1.78 | 1.57 | 1.53 | 1.50 | 1.50 | 1.50 | 1.49 | 1.49 | 1.49 | 1.54 | 1.24 |
| 11.9...... | 2.03 | 1.67 | 1.56 | 1.54 | 1.54 | 1.54 | 1.54 | 1.54 | 1.53 | 1.53 | 1.46 | 1.26 |
| 12.0...... | 2.02 | 1.63 | 1.32 | 1.31 | 1.31 | 1.31 | 1.30 | 1.30 | 1.30 | 1.30 | 1.32 | 1.26 |
| 12.2...... | 2.43 | 2.01 | 1.64 | 1.54 | 1.52 | 1.51 | 1.51 | 1.51 | 1.51 | 1.51 | 1.72 | 1.26 |
| 12.4...... | 2.36 | 2.03 | 1.87 | 1.62 | 1.50 | 1.47 | 1.46 | 1.46 | 1.46 | 1.46 | 1.78 | 1.31 |
| 12.6...... | 2.46 | 2.04 | 1.72 | 1.55 | 1.53 | 1.51 | 1.50 | 1.50 | 1.50 | 1.50 | 1.82 | 1.23 |
| 12.8...... | 2.52 | 2.11 | 1.74 | 1.44 | 1.42 | 1.41 | 1.41 | 1.41 | 1.41 | 1.41 | 1.60 | 1.31 |
| 13.0...... | 2.57 | 2.09 | 1.60 | 1.41 | 1.40 | 1.40 | 1.40 | 1.40 | 1.40 | 1.40 | 1.45 | 1.37 |
| 13.2...... | 2.77 | 2.23 | 1.89 | 1.60 | 1.57 | 1.55 | 1.54 | 1.54 | 1.54 | 1.54 | 1.93 | 1.31 |
| 13.4...... | 2.84 | 2.23 | 1.66 | 1.59 | 1.58 | 1.57 | 1.57 | 1.57 | 1.57 | 1.57 | 1.93 | 1.35 |
| 13.6...... | 2.94 | 2.38 | 2.08 | 1.62 | 1.45 | 1.43 | 1.42 | 1.42 | 1.42 | 1.42 | 1.66 | 1.41 |
| 13.8...... | 3.10 | 2.52 | 2.29 | 1.90 | 1.57 | 1.47 | 1.45 | 1.45 | 1.45 | 1.45 | 2.05 | 1.37 |
| 14.0...... | 3.24 | 2.60 | 2.30 | 1.83 | 1.66 | 1.61 | 1.58 | 1.57 | 1.57 | 1.57 | 2.19 | 1.37 |
| 14.2...... | 3.32 | 2.67 | 2.35 | 1.89 | 1.68 | 1.63 | 1.59 | 1.59 | 1.58 | 1.58 | 2.24 | 1.38 |
| 14.4...... | 3.51 | 2.87 | 2.52 | 1.98 | 1.73 | 1.67 | 1.63 | 1.63 | 1.62 | 1.62 | 2.37 | 1.39 |
| 14.6...... | 3.65 | 2.94 | 2.69 | 2.36 | 1.84 | 1.62 | 1.56 | 1.56 | 1.56 | 1.56 | 2.48 | 1.40 |
| 14.8...... | 3.75 | 2.98 | 2.71 | 2.41 | 1.91 | 1.65 | 1.57 | 1.57 | 1.56 | 1.56 | 2.51 | 1.41 |
| $15.0 \ldots . . .$ | 3.82 | 3.00 | 2.41 | 1.65 | 1.47 | 1.44 | 1.44 | 1.43 | 1.43 | 1.43 | 2.07 | 1.28 |
| 15.2...... | 4.04 | 3.13 | 2.61 | 1.78 | 1.50 | 1.46 | 1.45 | 1.45 | 1.45 | 1.45 | 2.08 | 1.33 |
| 15.4...... | 3.96 | 3.05 | 2.55 | 1.79 | 1.50 | 1.45 | 1.44 | 1.43 | 1.43 | 1.43 | 2.17 | 1.31 |
| 15.6...... | 4.30 | 3.30 | 2.85 | 2.15 | 1.69 | 1.52 | 1.47 | 1.46 | 1.46 | 1.46 | 2.39 | 1.36 |
| 15.8...... | 4.37 | 3.40 | 2.99 | 2.58 | 1.90 | 1.68 | 1.57 | 1.56 | 1.55 | 1.55 | 2.73 | 1.36 |
| 16.0...... | 4.59 | 3.56 | 3.19 | 2.88 | 2.17 | 1.68 | 1.59 | 1.58 | 1.58 | 1.58 | 2.91 | 1.41 |
| 16.2...... | 4.77 | 3.63 | 3.25 | 3.02 | 2.61 | 1.90 | 1.62 | 1.61 | 1.61 | 1.61 | 3.02 | 1.42 |

TABLE 3-Continued

|  | Remnant Mass ( $M_{\odot}$ ) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Initial Mass $\left(M_{\odot}\right)$ | $\begin{gathered} \text { Run ZA, } \\ E=0.3 \mathrm{~B}, \\ \text { Piston at } S=4 \end{gathered}$ | $\begin{gathered} \text { Run ZB, } \\ E=0.6 \mathrm{~B}, \\ \text { Piston at } S=4 \end{gathered}$ | $\begin{gathered} \text { Run } \mathrm{ZC}, \\ E=0.9 \mathrm{~B}, \\ \text { Piston at } S=4 \end{gathered}$ | $\begin{gathered} \text { Run ZD, } \\ E=1.2 \mathrm{~B}, \\ \text { Piston at } S=4 \end{gathered}$ | $\begin{gathered} \text { Run ZE, } \\ E=1.5 \mathrm{~B}, \end{gathered}$ <br> Piston at $S=4$ | $\begin{gathered} \text { Run ZF, } \\ E=1.8 \mathrm{~B}, \\ \text { Piston at } S=4 \end{gathered}$ | $\begin{gathered} \text { Run ZG, } \\ E=2.4 \mathrm{~B}, \\ \text { Piston at } S=4 \end{gathered}$ | $\begin{gathered} \text { Run ZH, } \\ E=3.0 \mathrm{~B}, \\ \text { Piston at } S=4 \end{gathered}$ | $\begin{gathered} \text { Run ZI, } \\ E=5.0 \mathrm{~B}, \\ \text { Piston at } S=4 \end{gathered}$ | $\begin{gathered} \text { Run ZJ, } \\ E=10.0 \mathrm{~B}, \\ \text { Piston at } S=4 \end{gathered}$ | $\begin{gathered} \text { Run ZP, } \\ E=1.2 \mathrm{~B}, \end{gathered}$ <br> Piston at $Y_{e}$ Core | $\begin{gathered} \text { Run } \mathrm{ZV}, \\ E=10.0 \mathrm{~B}, \\ \text { Piston at } Y_{e} \text { Core } \end{gathered}$ |
| 16.4...... | 4.94 | 3.79 | 3.41 | 3.16 | 2.75 | 1.95 | 1.64 | 1.63 | 1.63 | 1.63 | 3.15 | 1.45 |
| 16.6...... | 5.08 | 3.99 | 3.57 | 3.24 | 2.49 | 1.78 | 1.63 | 1.63 | 1.63 | 1.63 | 3.23 | 1.44 |
| 16.8...... | 5.14 | 3.91 | 3.44 | 3.18 | 2.88 | 2.31 | 1.83 | 1.77 | 1.75 | 1.75 | 3.20 | 1.32 |
| 17.0...... | 5.55 | 4.15 | 3.68 | 3.41 | 3.13 | 2.51 | 1.83 | 1.77 | 1.76 | 1.76 | 3.46 | 1.35 |
| 17.1...... | 5.52 | 4.21 | 3.76 | 3.48 | 3.19 | 2.54 | 1.84 | 1.78 | 1.77 | 1.77 | 3.51 | 1.37 |
| 17.2...... | 5.51 | 4.19 | 3.72 | 3.46 | 3.16 | 2.47 | 1.78 | 1.75 | 1.74 | 1.74 | 3.49 | 1.34 |
| 17.3...... | 5.57 | 4.27 | 3.82 | 3.55 | 3.24 | 2.67 | 1.91 | 1.83 | 1.82 | 1.82 | 3.51 | 1.39 |
| 17.4...... | 5.49 | 4.08 | 3.60 | 3.25 | 2.17 | 1.52 | 1.50 | 1.50 | 1.50 | 1.50 | 3.22 | 1.37 |
| 17.5...... | 5.76 | 4.40 | 3.92 | 3.62 | 3.34 | 2.71 | 1.91 | 1.84 | 1.82 | 1.82 | 3.63 | 1.40 |
| 17.6...... | 6.04 | 4.66 | 4.19 | 3.77 | 3.28 | 2.34 | 1.92 | 1.88 | 1.87 | 1.87 | 3.78 | 1.46 |
| 17.7...... | 5.83 | 4.47 | 3.97 | 3.59 | 3.01 | 2.04 | 1.77 | 1.74 | 1.73 | 1.73 | 3.56 | 1.58 |
| 17.8...... | 6.05 | 4.62 | 4.14 | 3.84 | 3.46 | 2.79 | 1.91 | 1.84 | 1.83 | 1.83 | 3.86 | 1.40 |
| 17.9...... | 6.06 | 4.58 | 4.07 | 3.78 | 3.45 | 2.90 | 1.94 | 1.85 | 1.84 | 1.84 | 3.77 | 1.42 |
| 18.0...... | 5.71 | 4.30 | 3.69 | 2.09 | 1.52 | 1.50 | 1.49 | 1.49 | 1.49 | 1.49 | 3.02 | 1.38 |
| 18.1...... | 6.08 | 4.33 | 3.79 | 3.23 | 1.73 | 1.54 | 1.53 | 1.53 | 1.53 | 1.52 | 3.20 | 1.39 |
| 18.2...... | 6.59 | 4.77 | 4.13 | 3.77 | 3.23 | 2.67 | 1.61 | 1.56 | 1.54 | 1.54 | 3.82 | 1.41 |
| 18.3...... | 6.61 | 4.86 | 4.29 | 3.90 | 3.48 | 2.88 | 1.80 | 1.73 | 1.71 | 1.70 | 3.97 | 1.43 |
| 18.4...... | 5.85 | 4.25 | 1.56 | 1.51 | 1.51 | 1.51 | 1.51 | 1.51 | 1.51 | 1.51 | 1.91 | 1.40 |
| 18.5...... | 6.45 | 4.59 | 3.99 | 3.41 | 1.97 | 1.57 | 1.55 | 1.55 | 1.55 | 1.55 | 3.43 | 1.42 |
| 18.6...... | 6.25 | 4.57 | 3.93 | 2.54 | 1.55 | 1.52 | 1.51 | 1.51 | 1.51 | 1.51 | 3.24 | 1.41 |
| 18.7...... | 6.58 | 4.76 | 4.17 | 3.64 | 1.69 | 1.56 | 1.55 | 1.55 | 1.55 | 1.55 | 3.63 | 1.42 |
| 18.8...... | 6.66 | 4.71 | 4.06 | 3.45 | 2.10 | 1.59 | 1.57 | 1.57 | 1.57 | 1.57 | 3.49 | 1.42 |
| 18.9...... | 6.97 | 5.13 | 4.46 | 3.74 | 1.93 | 1.65 | 1.63 | 1.63 | 1.63 | 1.63 | 3.80 | 1.47 |
| 19.0...... | 6.99 | 5.16 | 4.43 | 3.38 | 1.84 | 1.65 | 1.63 | 1.63 | 1.63 | 1.63 | 3.58 | 1.44 |
| 19.2...... | 7.08 | 5.03 | 4.37 | 3.77 | 2.51 | 1.61 | 1.59 | 1.59 | 1.59 | 1.59 | 3.81 | 1.44 |
| 19.4...... | 7.25 | 5.09 | 4.38 | 3.79 | 2.73 | 1.61 | 1.57 | 1.56 | 1.56 | 1.56 | 3.84 | 1.44 |
| 19.6...... | 7.40 | 5.25 | 4.56 | 4.02 | 3.12 | 1.69 | 1.64 | 1.63 | 1.63 | 1.63 | 4.08 | 1.45 |
| 19.8...... | 7.66 | 5.49 | 4.72 | 3.79 | 1.99 | 1.63 | 1.61 | 1.61 | 1.61 | 1.61 | 3.97 | 1.43 |
| 20.0...... | 7.77 | 5.37 | 4.37 | 2.43 | 1.70 | 1.50 | 1.47 | 1.47 | 1.46 | 1.46 | 2.49 | 1.46 |
| 20.5...... | 7.75 | 5.47 | 4.67 | 3.57 | 1.83 | 1.67 | 1.65 | 1.65 | 1.64 | 1.64 | 3.80 | 1.46 |
| 21.0...... | 9.14 | 6.36 | 5.45 | 4.21 | 1.90 | 1.53 | 1.50 | 1.50 | 1.50 | 1.50 | 4.30 | 1.49 |
| 21.5...... | 7.88 | 5.92 | 5.05 | 3.30 | 1.66 | 1.63 | 1.61 | 1.61 | 1.61 | 1.61 | 3.61 | 1.45 |
| 22.0...... | 9.92 | 6.93 | 5.87 | 3.71 | 1.60 | 1.53 | 1.52 | 1.52 | 1.52 | 1.52 | 4.52 | 1.36 |
| 22.5...... | 9.81 | 6.96 | 5.68 | 2.82 | 1.55 | 1.50 | 1.50 | 1.49 | 1.49 | 1.49 | 3.32 | 1.43 |
| 23.0...... | 10.49 | 7.36 | 6.26 | 4.51 | 1.94 | 1.66 | 1.64 | 1.64 | 1.64 | 1.64 | 5.00 | 1.46 |
| 23.5...... | 11.42 | 8.10 | 6.86 | 5.78 | 3.11 | 2.18 | 1.95 | 1.93 | 1.92 | 1.92 | 6.22 | 1.59 |
| 24.0...... | 12.32 | 8.54 | 7.23 | 6.47 | 5.11 | 3.02 | 2.18 | 2.10 | 2.08 | 2.07 | 6.67 | 1.65 |
| 24.5...... | 12.64 | 8.91 | 7.47 | 6.66 | 4.70 | 2.60 | 2.30 | 2.23 | 2.21 | 2.20 | 6.87 | 1.68 |
| 25.0...... | 10.19 | 7.96 | 7.13 | 4.16 | 2.57 | 2.35 | 2.21 | 2.19 | 2.17 | 2.17 | 5.96 | 1.60 |
| 25.5...... | 13.48 | 9.41 | 7.68 | 2.01 | 1.90 | 1.88 | 1.87 | 1.87 | 1.87 | 1.87 | 3.00 | 1.62 |
| 26.0...... | 14.22 | 9.94 | 8.14 | 2.08 | 1.77 | 1.75 | 1.74 | 1.74 | 1.74 | 1.74 | 3.91 | 1.53 |

TABLE 3-Continued

|  | Remnant Mass ( $M_{\odot}$ ) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Initial <br> Mass <br> $\left(M_{\odot}\right)$ | $\begin{gathered} \text { Run ZA, } \\ E=0.3 \mathrm{~B}, \\ \text { Piston at } S=4 \end{gathered}$ | $\begin{gathered} \text { Run ZB, } \\ E=0.6 \mathrm{~B} \text {, } \\ \text { Piston at } S=4 \end{gathered}$ | $\begin{gathered} \text { Run ZC, } \\ E=0.9 \mathrm{~B}, \\ \text { Piston at } S=4 \end{gathered}$ | $\begin{gathered} \text { Run ZD, } \\ E=1.2 \mathrm{~B}, \\ \text { Piston at } S=4 \end{gathered}$ | $\begin{gathered} \text { Run ZE, } \\ E=1.5 \mathrm{~B} \text {, } \\ \text { Piston at } S=4 \end{gathered}$ | $\begin{gathered} \text { Run ZF, } \\ E=1.8 \mathrm{~B} \text {, } \\ \text { Piston at } S=4 \end{gathered}$ | $\begin{gathered} \text { Run } \mathrm{ZG} \text {, } \\ E=2.4 \mathrm{~B}, \end{gathered}$ <br> Piston at $S=4$ | $\begin{gathered} \text { Run ZH, } \\ E=3.0 \mathrm{~B} \text {, } \\ \text { Piston at } S=4 \end{gathered}$ | $\begin{gathered} \text { Run ZI, } \\ E=5.0 \mathrm{~B}, \\ \text { Piston at } S=4 \end{gathered}$ | $\begin{gathered} \text { Run ZJ, } \\ E=10.0 \mathrm{~B}, \\ \text { Piston at } S=4 \end{gathered}$ | $\begin{gathered} \text { Run ZP, } \\ E=1.2 \mathrm{~B}, \end{gathered}$ <br> Piston at $Y_{e}$ Core | $\begin{gathered} \text { Run ZV, } \\ E=10.0 \mathrm{~B}, \end{gathered}$ <br> Piston at $Y_{e}$ Core |
| 26.5...... | 14.41 | 9.97 | 8.29 | 6.41 | 1.88 | 1.82 | 1.81 | 1.81 | 1.80 | 1.80 | 7.23 | 1.55 |
| 27.0...... | 12.03 | 8.92 | 7.26 | 1.96 | 1.77 | 1.74 | 1.73 | 1.73 | 1.73 | 1.73 | 2.30 | 1.52 |
| 27.5...... | 15.71 | 11.13 | 9.15 | 3.16 | 1.63 | 1.61 | 1.60 | 1.59 | 1.59 | 1.59 | 6.89 | 1.46 |
| 28.0...... | 12.90 | 9.51 | 7.76 | 1.92 | 1.63 | 1.61 | 1.60 | 1.60 | 1.60 | 1.60 | 2.19 | 1.46 |
| 28.5...... | 16.36 | 11.72 | 9.42 | 2.54 | 1.68 | 1.64 | 1.63 | 1.63 | 1.63 | 1.62 | 7.50 | 1.43 |
| 29.0...... | 17.29 | 12.15 | 10.16 | 8.23 | 2.21 | 1.83 | 1.74 | 1.73 | 1.72 | 1.72 | 8.95 | 1.49 |
| 29.5...... | 17.77 | 12.75 | 10.25 | 7.56 | 1.99 | 1.76 | 1.71 | 1.71 | 1.70 | 1.70 | 8.83 | 1.46 |
| 30.0...... | 15.40 | 11.12 | 9.55 | 2.73 | 1.97 | 1.83 | 1.77 | 1.76 | 1.75 | 1.75 | 4.56 | 1.51 |
| 30.5...... | 18.91 | 13.70 | 11.16 | 9.74 | 3.15 | 1.98 | 1.79 | 1.78 | 1.77 | 1.77 | 9.96 | 1.52 |
| 31.0...... | 19.37 | 14.10 | 11.47 | 10.06 | 3.89 | 2.16 | 1.89 | 1.86 | 1.85 | 1.84 | 10.17 | 1.54 |
| 31.5...... | 19.53 | 14.48 | 12.04 | 10.29 | 2.62 | 2.14 | 1.98 | 1.95 | 1.94 | 1.94 | 10.74 | 1.59 |
| 32.0...... | 20.62 | 15.25 | 12.45 | 11.04 | 7.66 | 2.53 | 2.02 | 1.96 | 1.95 | 1.94 | 11.20 | 1.58 |
| 32.5...... | 21.01 | 15.41 | 12.73 | 11.32 | 5.49 | 2.42 | 2.05 | 2.01 | 1.99 | 1.98 | 11.48 | 1.61 |
| 33.0...... | 21.70 | 16.32 | 13.41 | 11.95 | 8.60 | 2.79 | 2.20 | 2.11 | 2.08 | 2.08 | 12.17 | 1.65 |
| 33.5...... | 21.17 | 16.19 | 13.43 | 11.82 | 3.59 | 2.53 | 2.22 | 2.15 | 2.13 | 2.12 | 11.96 | 1.66 |
| 34.0...... | 23.15 | 17.25 | 14.18 | 12.46 | 11.09 | 3.74 | 2.33 | 2.18 | 2.13 | 2.12 | 12.66 | 1.66 |
| 34.5...... | 23.41 | 17.73 | 14.65 | 12.88 | 11.29 | 3.28 | 2.38 | 2.25 | 2.21 | 2.20 | 13.06 | 1.67 |
| 35.0...... | 23.51 | 18.05 | 14.84 | 13.08 | 11.12 | 3.17 | 2.43 | 2.29 | 2.25 | 2.24 | 13.37 | 1.68 |
| 36.0...... | 26.27 | 19.60 | 16.27 | 14.12 | 12.95 | 10.04 | 2.86 | 2.47 | 2.35 | 2.33 | 14.43 | 1.82 |
| 37.0...... | 27.91 | 20.61 | 17.19 | 14.85 | 13.59 | 11.58 | 3.02 | 2.58 | 2.31 | 2.26 | 15.09 | 1.85 |
| 38.0...... | 20.96 | 16.24 | 14.08 | 11.43 | 3.99 | 3.16 | 2.54 | 2.32 | 2.24 | 2.23 | 11.95 | 1.68 |
| 39.0...... | 14.27 | 11.54 | 8.06 | 6.24 | 4.61 | 3.52 | 2.71 | 2.40 | 2.25 | 2.24 | 6.75 | 1.79 |
| 40.0...... | 32.12 | 24.05 | 20.64 | 18.16 | 16.48 | 15.29 | 6.15 | 3.38 | 2.40 | 2.19 | 18.32 | 1.92 |
| 41.0..... | 25.86 | 20.31 | 17.51 | 15.90 | 13.73 | 5.41 | 3.73 | 3.09 | 2.44 | 2.29 | 16.02 | 1.88 |
| 42.0...... | 31.18 | 23.52 | 20.18 | 18.14 | 16.53 | 15.01 | 4.04 | 3.35 | 2.48 | 2.27 | 18.15 | 1.96 |
| 43.0...... | 34.27 | 26.63 | 23.09 | 20.69 | 18.85 | 17.56 | 12.69 | 4.25 | 2.45 | 2.00 | 20.85 | 1.79 |
| 44.0...... | 35.94 | 28.69 | 24.78 | 22.23 | 20.40 | 18.98 | 16.07 | 5.23 | 2.60 | 1.66 | 22.22 | 1.66 |
| 45.0...... | 16.94 | 12.90 | 11.14 | 9.08 | 7.47 | 6.31 | 4.46 | 3.57 | 2.52 | 2.23 | 9.41 | 1.95 |
| 50.0...... | 15.46 | 13.94 | 12.69 | 11.67 | 10.66 | 9.20 | 5.85 | 3.64 | 2.47 | 2.36 | 11.89 | 1.86 |
| 55.0...... | 18.14 | 16.46 | 14.50 | 12.60 | 10.95 | 9.50 | 7.21 | 5.73 | 3.39 | 1.96 | 12.59 | 1.96 |
| 60.0..... | 43.32 | 34.58 | 29.61 | 27.46 | 25.88 | 24.62 | 11.75 | 9.35 | 4.56 | 1.93 | 27.45 | 1.93 |
| 65.0...... | 24.00 | 22.80 | 21.57 | 19.95 | 18.22 | 16.44 | 13.20 | 10.50 | 4.89 | 1.99 | 20.01 | 1.99 |
| 70.0...... | 52.95 | 45.53 | 38.23 | 35.35 | 33.35 | 31.71 | 29.03 | 14.53 | 6.57 | 2.21 | 35.21 | 2.08 |
| 75.0..... | 28.07 | 26.96 | 25.96 | 24.63 | 23.25 | 21.55 | 18.42 | 15.60 | 8.88 | 2.25 | 24.62 | 2.20 |
| 80.0...... | 29.61 | 29.41 | 27.99 | 27.09 | 25.99 | 24.49 | 21.39 | 18.52 | 11.14 | 2.40 | 27.06 | 2.32 |
| 85.0...... | 27.68 | 27.69 | 27.62 | 27.23 | 26.17 | 24.93 | 22.41 | 19.93 | 13.28 | 5.15 | 27.32 | 4.44 |
| 90.0...... | 26.83 | 26.86 | 26.77 | 26.83 | 26.77 | 26.25 | 24.41 | 21.92 | 15.26 | 7.02 | 27.41 | 6.90 |
| 95.0..... | 29.06 | 29.04 | 28.30 | 26.87 | 25.48 | 24.10 | 21.23 | 18.49 | 12.10 | 3.24 | 26.32 | 3.30 |
| 100.0.... | 40.01 | 38.34 | 36.95 | 35.70 | 34.12 | 31.79 | 25.08 | 13.35 | 2.12 | 2.03 | 35.78 | 1.53 |

TABLE 4
$Z=$ solar Baryonic Remnant Masses

| Initial Mass $\left(M_{\odot}\right)$ | Remnant Mass ( $M_{\odot}$ ) |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & \text { Run SA, } E=1.2 \mathrm{~B}, \\ & \text { Piston at } S=4 \end{aligned}$ | $\begin{gathered} \text { Run SB, } E=2.4 \mathrm{~B}, \\ \text { Piston at } S=4 \end{gathered}$ | $\text { Run } \mathrm{SC}, E=1.2 \mathrm{~B} \text {, }$ <br> Piston at Fe Core | $\operatorname{Run~} \mathrm{SD}, E=2.4 \mathrm{~B} \text {, }$ <br> Piston at Fe Core |
| 12.0..................... | 1.53 | 1.52 | 1.37 | 1.37 |
| 13.0.................. | 1.56 | 1.55 | 1.48 | 1.41 |
| 14.0..................... | 1.71 | 1.70 | 1.57 | 1.52 |
| 15.0..................... | 1.84 | 1.83 | 1.58 | 1.49 |
| 16.0..................... | 2.09 | 1.50 | 1.46 | 1.39 |
| 17.0..................... | 1.54 | 1.54 | 1.52 | 1.42 |
| 18.0.................. | 1.90 | 1.89 | 1.89 | 1.54 |
| 19.0.... | 1.66 | 1.64 | 1.71 | 1.49 |
| 20.0... | 1.86 | 1.82 | 1.96 | 1.62 |
| 21.0.... | 1.48 | 1.46 | 1.48 | 1.46 |
| 22.0.................... | 1.93 | 1.84 | 2.13 | 1.67 |
| 23.0.................... | 2.36 | 2.14 | 2.75 | 1.95 |
| 24.0..................... | 2.29 | 2.06 | 2.64 | 1.89 |
| 25.0.................... | 2.09 | 1.91 | 2.43 | 1.81 |
| 26.0.................... | 1.75 | 1.74 | 1.82 | 1.61 |
| 27.0..................... | 1.82 | 1.75 | 1.96 | 1.62 |
| 28.0..................... | 2.39 | 1.59 | 2.49 | 1.59 |
| 29.0..................... | 1.76 | 1.64 | 2.02 | 1.57 |
| 30.0..................... | 1.95 | 1.74 | 2.23 | 1.68 |
| 31.0..................... | 1.96 | 1.71 | 2.33 | 1.67 |
| 32.0..................... | 2.27 | 1.79 | 2.62 | 1.79 |
| 33.0..................... | 2.52 | 1.85 | 2.89 | 1.87 |
| 35.0..................... | 3.21 | 2.02 | 3.85 | 2.13 |
| 40.0.................... | 5.60 | 2.73 | 6.72 | 3.15 |
| 45.0.................... | 3.93 | 2.45 | 5.03 | 2.70 |
| 50.0.................... | 1.88 | 1.71 | 2.22 | 1.64 |
| 55.0.................... | 1.76 | 1.66 | 2.05 | 1.57 |
| 60.0.................... | 1.64 | 1.60 | 1.71 | 1.51 |
| 70.0.................... | 2.06 | 1.74 | 2.18 | 1.72 |
| 80.0..................... | 2.03 | 1.67 | 2.05 | 1.65 |
| 100.0................... | 2.08 | 1.85 | 2.16 | 1.75 |

possibility of primary nitrogen production in the star (A. Heger \& S. E. Woosley 2008, in preparation). For such massive stars, the entropy barrier separating the outer extent of the convective core during helium burning is not sufficient to prohibit mixing with the hydrogen envelope with its very weak burning shell (this phenomenon does not occur in nonrotating stars of solar metallicity). The mixing of hydrogen and hot carbon leads to the production of nitrogen, which is convected throughout most of the envelope. With the new large CNO abundance, nuclear energy generation is increased and the star eventually expands to red supergiant proportions. Stars that do not make nitrogen in this way stay compact. As Figure 3 shows, the result is two branches of remnant masses.

Figures 5, 6, and 7 show the distribution of remnant masses for primordial supernovae with explosion energies $0.6,1.2$, and 2.4 B for a piston located at the $S / N_{\mathrm{A}} k=4$ point. Figure 8 shows a similar remnant mass distribution for a piston located at the edge of the deleptonized core, for an explosion energy of 1.2 B . The systematics of these results is discussed in $\S 5$.

### 4.2. Fallback in Population I Supernovae

Massive Population I stars differ from Population III stars in that they always develop strong hydrogen-burning shells and become red supergiants. Their envelopes are thus, globally speaking, less tightly bound than in Population III stars and also have different profiles of $\rho r^{3}$ as a function of radius. Consequently, re-
verse shocks are weaker in red supergiants, as noted by Chevalier (1989) and Woosley \& Weaver (1995), and their remnant masses are smaller. Above about $35 M_{\odot}$ solar metallicity stars lose their envelopes to winds during the red giant stage and become WolfRayet stars. The Wolf-Rayet stars lose further mass so that, for example, a star with an initial mass of $100 M_{\odot}$ dies with a mass of only $6 M_{\odot}$. Such light stars obviously cannot leave behind very massive black holes and, in fact, tend to leave neutron stars.

Figure 9 shows the remnant masses expected for solar metallicity. These masses are influenced both by the decreased amount of fallback that happens in the reverse shock in red supergiants and by the mass loss before the explosion, especially above $40 M_{\odot}$.

Figure 10 shows the distribution of neutron star gravitational masses for the solar metallicity survey. The properties of these are sensitive to the placement of the piston, as well as its energy, and the figure is for a piston location at the $S / N_{\mathrm{A}} k=4$ point near the base of the oxygen shell and an explosion energy of 1.2 B . The inset shows the distribution of baryonic masses of black holes, on a logarithmic scale on the $x$-axis. The main figure and the inset are normalized to add up to $100 \%$ together (all remnants; see caption of Fig. 10 for details). Figure 11 shows the same diagram of remnant mass distribution for a piston located deeper in the star, at the edge of the iron core. Lower explosion energies than 1.2 B are not considered here but, like the Population III explosions, would give larger black hole masses,


Fig. 3.-Comparison of baryonic remnant masses for (a) ZB, (b) ZD, and (c) ZG models. The explosion energies are $0.6,1.2$, and 2.4 B for models ZB , ZD , and ZG , respectively. It is clear that there are two branches of remnant masses. The higher mass branch consists of compact stars with a radius less than $200 R_{\odot}$, whereas the lower mass branch consists of red supergiants with a radius greater than $200 R_{\odot}$. The positions of the He core (dotted lines) and CO core (dashed lines) in the initial models are also shown. Note that for the lower mass branch of ZB models the remnant mass is very close to the CO core mass.
up to approximately the mass of the helium core in the presupernova star (Woosley et al. 2002).

## 5. REMNANTS

### 5.1. Gravitational and Baryonic Masses

The fallback calculations described above and as summarized in Tables 3 and 4 give the baryonic remnant masses. For neutron stars especially, a significant fraction of this mass becomes binding energy and is radiated away in the form of neutrinos. This fraction can be estimated if the binding energy of the neutron star is known, but it is dependent on the nuclear equation of state employed. Here the estimate of Lattimer \& Prakash (2001) is adopted:

$$
\begin{equation*}
\mathrm{BE}=\frac{3}{5} \beta\left(1-\frac{1}{2} \beta\right)^{-1}, \quad \beta=\frac{G M_{\mathrm{remnant}}}{R_{\mathrm{remnant}} c^{2}} \tag{1}
\end{equation*}
$$

where $G$ is the gravitational constant, $M_{\text {remnant }}$ is the gravitational mass of the remnant, $R_{\text {remnant }}$ is the radius of the remnant, and $c$ is the speed of light. Lattimer \& Prakash (2001) recommend a radius of $\sim 12 \mathrm{~km}$. This equation can then be solved to give a remnant mass as a function of baryonic mass, $M_{\text {baryon }}$ :

$$
\begin{equation*}
M_{\mathrm{remnant}}=M_{\text {baryon }}\left(1+\frac{3}{5} \frac{G M_{\text {baryon }}}{R_{\mathrm{remnant}} c^{2}}\right)^{-1} \tag{2}
\end{equation*}
$$



Fig. 4.-Baryonic remnant masses for (a) ZB, (b) ZD, and (c) ZG models plotted on a finer scale for lower mass stars. The explosion energies are $0.6,1.2$, and 2.4 B for models ZB, ZD, and ZG, respectively. As we expected, ZG models make many neutron stars, whereas the lower energy ZB models make many black holes.

Here two choices of maximum neutron star mass are employed, 1.7 and $2.0 M_{\odot}$. The limiting baryonic mass for which such heavy neutron stars are made is then computed from

$$
\begin{equation*}
M_{\mathrm{baryon}}=M_{\mathrm{remnant}}\left(1-\frac{3}{5} \frac{G M_{\mathrm{remnant}}}{R_{\mathrm{remnant}} c^{2}}\right)^{-1} \tag{3}
\end{equation*}
$$

For example, a maximum gravitational mass of $2.0 M_{\odot}$ implies a maximum baryonic mass of $2.35 M_{\odot}$. For baryonic masses above that limit, a black hole forms. Here any effects due to rotation are neglected.

Remnants that collapse to black holes may also lose an appreciable fraction of their baryonic mass in the formation process, but unlike neutron stars, that fraction depends not just on the final state but on the formation process. If the black hole forms promptly from a big collapsing core, bypassing any neutron star stage, and if the fallback of matter contributing to its mass is small or essentially spherically symmetric, very little rest mass is radiated away in the form of neutrinos. The gravitational mass approximately equals the baryonic mass. On the other hand, one could first form a massive neutron star that cools, radiating away approximately $20 \%$ of its rest mass before it collapses. If the black hole is a rapidly rotating Kerr black hole, the binding energy of the last stable orbit is $42.3 \%$ of the rest mass. If the disk is hot enough and not advection dominated, this energy is radiated away. Depending on the size of the black hole, its rotation, and how much mass it accreted through a cooling disk and


FIg. 5.-Distribution of remnant masses for 0.6 B explosions of metal-free stars with pistons located at the $S / N_{\mathrm{A}} k=4.0$ point, for an initial mass range of $9.5-100 M_{\odot}$ and an assumed maximum neutron star mass of $2 M_{\odot}$. The main figure gives gravitational masses of neutron stars; the inset shows the baryonic masses of black holes. The color coding (cumulative) indicates the initial mass range of the progenitor stars. The curve is a Gaussian fit with the same average and variance as distribution for the neutron stars (mainfigure). For the inset the curve is a Gaussian fit to the logarithm of black hole masses (geometric fit). The normalization of the bins in the big plot is such that the sum over the bins times the bin width equals total fraction of neutron stars. For the inset the normalization is not "per solar mass" but "per dex;" i.e., the sum of bin height times bin width in dex equals the total fraction of black holes. The bin sizes are $0.025 M_{\odot}$ for the main figure and 0.05 dex for the inset. The spike at $1.18 M_{\odot}$ is for lower mass stars that make iron cores near the Chandrasekhar mass limit and have final mass cuts near the boundary of that core. Since iron cores have an appreciable neutron excess, the Chandrasekhar mass is appreciably reduced from the classical $1.39 M_{\odot}$ of baryons ( $1.26 M_{\odot}$ gravitational).


Fig. 6.-Distribution of remnant masses for 1.2 B explosions of metal-free stars with pistons located at the $S / N_{\mathrm{A}} k=4.0$ point, for an initial mass range of $9.5-100 M_{\odot}$ and an assumed maximum neutron star mass of $2 M_{\odot}$. See also the caption of Fig. 5.


FIg. 7.-Distribution of remnant masses for 2.4 B explosions of metal-free stars with pistons located at the $S / N_{\mathrm{A}} k=4.0$ point, for an initial mass range of $9.5-100 M_{\odot}$ and an assumed maximum neutron star mass of $2 M_{\odot}$. See also the caption of Fig. 5.


Fig. 8.-Distribution of remnant masses for 1.2 B explosions of metal-free stars with pistons located at the edge of the deleptonized core, for an initial mass range of $9.5-100 M_{\odot}$ and an assumed maximum neutron star mass of $2 M_{\odot}$. See also the caption of Fig. 5.


Fig. 9.-Comparison of baryonic remnant masses for SA series with Kepler and Pangu. The results from two different codes are similar. However, the final baryonic remnant masses calculated using Pangu (plus signs) are greater than those calculated using Kepler (diamonds), especially for the initial mass range of $30-50 M_{\odot}$.
at what rotation rate of the black hole that occurred, the gravitational mass could be some $20 \%-40 \%$ smaller than the baryonic mass.

For simplicity here, we assume that the gravitational mass of any black hole remnant equals the mass of the baryons that made
it with no correction for neutrino losses. It should be kept in mind, however, that this is actually an upper limit to the mass of the black hole. Perhaps more realistically, the binding energy of the heaviest stable neutron star, about $0.25 M_{\odot}$, should be subtracted from all our black hole remnant masses, assuming that, along the way, each black hole was formed from a proto-neutron star that reached its maximum mass, radiated its binding energy, and then collapsed. In the spirit of the rest of the paper, all effects due to rotation are neglected.

### 5.2. The Corrected Remnant Mass Distribution

The distribution of remnant masses is obtained by linear interpolation of the remnant masses among the different initial masses. The result is then integrated over a Salpeter initial mass function (IMF) with exponent -1.35 . The resulting mapping into bins is exact. A bin width of $0.025 M_{\odot}$ is used. The averages and standard deviations (Table 5) are computed from this distribution. For the black holes, the average logarithmic mass (geometric mean) is also given. The fourth column of Table 5 gives the fraction of remnants, from the mass range considered, that are black holes. The fraction of neutron stars is one minus that number.

To round out the table, remnant masses for main-sequence stars lighter than the $12 M_{\odot}$ considered by Woosley \& Heger (2007) and the $10 M_{\odot}$ considered by A. Heger \& S. E. Woosley (2008, in preparation) were estimated. Presupernova models resulting from 10 and $11 M_{\odot}$ solar metallicity stars were computed using the same physics and codes as described in the review. Because such stars result in a degenerate core surrounded by thin layers of heavy elements, it is reasonable to expect fallback to be negligible in the explosion. The (baryonic) remnant masses were just taken to


Fig. 10.-Distribution of remnant masses for 1.2 B explosions of solar metallicity stars with pistons located at the entropy $S / N_{\mathrm{A}} k=4$ point for an initial mass range of $9.1-100 M_{\odot}$. We assumed a maximum neutron star mass of $2 M_{\odot}$. See also the caption of Fig. 5.


Fig. 11.-Distribution of remnant masses for 1.2 B explosions of solar metallicity stars with pistons located at the edge of the deleptonized core, for an initial mass range of $9.1-100 M_{\odot}$ and an assumed maximum neutron star mass of $2 M_{\odot}$. See also the caption of Fig. 5.
be $S / N_{\mathrm{A}} k=4.0$ masses of the presupernova stars, $1.37 M_{\odot}$ for the $11 M_{\odot}$ star and $1.35 M_{\odot}$ for the $10 M_{\odot}$. The same $1.35 M_{\odot}$ value was taken to characterize all stars down to $9.1 M_{\odot}$, the assumed transition to superasymptotic giant branch (SAGB) stars (Poelarends et al. 2007). For the piston located at the Fe core, a baryonic remnant mass of $1.32 M_{\odot}$ was assumed for the $11 M_{\odot}$ star and lighter stars.

For the zero-metallicity stars, the remnant characteristics of the $10 M_{\odot}$ star were assumed to hold down to the SAGB limit for $Z=0$ stars, taken here to be $9.5 M_{\odot}$.

## 6. DISCUSSION AND CONCLUSIONS

Table 6 gives the statistical characteristics of sets of compact remnants extracted from an IMF-averaged distribution of supernovae of the two populations. Here a Salpeter IMF is assumed over the entire mass range examined, $9 \lesssim M / M_{\odot} \lesssim 100$. The error bars represent a $1 \sigma$ deviation in the distribution. Different choices for the IMF could be explored by others using the values in Tables 3 and 4. For the black hole masses, the logarithmic average, as well as the arithmetic average, might be of interest, and both are given. The statistical results depend not only on the physics of the explosion (piston mass and energy) but also on the assumed maximum mass of the neutron star. Obviously, the heavier that maximum mass, the fewer the number of black holes.

In general, the observed trends follow expectation. More energetic explosions eject more matter, experience less fallback, and make lighter compact remnants. Even the lowest energy explosions considered, 0.3 B , eject most of the hydrogen envelope of all Population III stars. Thus, a supernova-like display can be expected in all cases, although the event may be very faint if the
radius is small and no ${ }^{56} \mathrm{Ni}$ is ejected (A. Heger \& S. E. Woosley 2008, in preparation; Scannapieco et al. 2005). The mass of the black hole in these low-energy explosions approaches that of the helium core of the presupernova star (Fig. 3), e.g., $\sim 10 M_{\odot}$ in a $25 M_{\odot}$ supernova and $\sim 40 M_{\odot}$ in a $100 M_{\odot}$ star. The average black hole mass from a generation of such zero-metal stars ranges from about 6 to $10 M_{\odot}$ if one excludes hyperenergetic explosions ( 5 B and more) and very low energy ones. There is great variation about this mean, however, and hole masses up to $40 M_{\odot}$ are possible. The fraction of black hole remnants is also high, typically $20 \%-50 \%$ and possibly as great as $90 \%$. If modern supernovae can be taken as a guide, the results for the $S / N_{\mathrm{A}} k=4$, 1.2 B case (model SA) may be most realistic (Woosley \& Heger 2007).

The fraction of remnants that are black holes is clearly smaller for modern (i.e., solar metallicity) stars, and the average mass of those holes is smaller. The actual value is sensitive to the values adopted for the maximum neutron star mass and explosion energies, but percentages in the range $10 \%-25 \%$ are reasonable. Explosion energies as great as 2.4 B would probably give Type II supernova light curves that are too bright (Woosley \& Heger 2007). Typical black hole masses are around $3 M_{\odot}$ unless the explosion energy is very low.

Experimental estimates for the average black hole mass are hard to find, and it must be kept in mind that accurate values for the black hole mass can only come from binaries where the evolution might have been influenced by mass exchange. Rotation can also affect the relation between helium core mass and mainsequence mass and possibly lead to larger black holes. There is also a predisposition to find massive black holes since it is the

TABLE 5
Remnant Mass Averages and Distributions

| $Z$ | Piston | $E_{\text {exp }}$ <br> (B) | $\begin{aligned} & \mathrm{BH} \\ & (\%) \end{aligned}$ | $\log M_{\mathrm{BH}}$ $\left(M_{\odot}\right)$ | $\begin{aligned} & \text { BH Mass } \\ & \left(M_{\odot}\right) \end{aligned}$ | NS Mass $\left(M_{\odot}\right)$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Assume Maximum Neutron Star Gravitational Mass of 1.7 $M_{\odot}$ |  |  |  |  |  |  |
| Solar | $S=4$ | 1.2 | 23.96 | $0.41 \pm 0.14$ | $2.71 \pm 1.02$ | $1.41 \pm 0.15$ |
|  | $S=4$ | 2.4 | 10.63 | $0.35 \pm 0.05$ | $2.25 \pm 0.25$ | $1.40 \pm 0.13$ |
|  | Fe | 1.2 | 25.48 | $0.45 \pm 0.16$ | $3.06 \pm 1.33$ | $1.34 \pm 0.14$ |
|  | Fe | 2.4 | 7.15 | $0.41 \pm 0.07$ | $2.57 \pm 0.38$ | $1.33 \pm 0.12$ |
| 0......................... | $S=4$ | 0.3 | 75.09 | $0.86 \pm 0.38$ | $10.66 \pm 9.64$ | $1.39 \pm 0.15$ |
|  | $S=4$ | 0.6 | 70.39 | $0.79 \pm 0.36$ | $8.86 \pm 8.26$ | $1.32 \pm 0.14$ |
|  | $S=4$ | 0.9 | 60.25 | $0.80 \pm 0.33$ | $8.66 \pm 7.54$ | $1.33 \pm 0.14$ |
|  | $S=4$ | 1.2 | 52.63 | $0.75 \pm 0.35$ | $7.93 \pm 7.47$ | $1.33 \pm 0.14$ |
|  | $S=4$ | 1.5 | 34.85 | $0.76 \pm 0.38$ | $8.60 \pm 8.04$ | $1.36 \pm 0.15$ |
|  | $S=4$ | 1.8 | 26.31 | $0.76 \pm 0.40$ | $8.80 \pm 8.24$ | $1.35 \pm 0.13$ |
|  | $S=4$ | 2.4 | 19.59 | $0.72 \pm 0.38$ | $7.88 \pm 7.39$ | $1.35 \pm 0.13$ |
|  | $S=4$ | 3.0 | 19.36 | $0.63 \pm 0.33$ | $5.91 \pm 5.51$ | $1.35 \pm 0.12$ |
|  | $S=4$ | 5.0 | 18.89 | $0.50 \pm 0.24$ | $3.85 \pm 3.10$ | $1.35 \pm 0.12$ |
|  | $S=4$ | 10.0 | 17.55 | $0.36 \pm 0.10$ | $2.37 \pm 0.79$ | $1.36 \pm 0.13$ |
|  | Fe | 1.2 | 59.00 | $0.74 \pm 0.34$ | $7.63 \pm 7.18$ | $1.28 \pm 0.19$ |
|  | Fe | 10.0 | 5.23 | $0.39 \pm 0.16$ | $2.67 \pm 1.26$ | $1.27 \pm 0.15$ |
| Assume Maximum Neutron Star Gravitational Mass of 2.0 $M_{\odot}$ |  |  |  |  |  |  |
| Solar | $S=4$ | 1.2 | 8.59 | $0.56 \pm 0.12$ | $3.80 \pm 1.02$ | $1.47 \pm 0.21$ |
|  | $S=4$ | 2.4 | 3.72 | $0.41 \pm 0.02$ | $2.56 \pm 0.11$ | $1.43 \pm 0.17$ |
|  | Fe | 1.2 | 14.53 | $0.55 \pm 0.15$ | $3.76 \pm 1.40$ | $1.40 \pm 0.22$ |
|  | Fe | 2.4 | 4.77 | $0.45 \pm 0.04$ | $2.80 \pm 0.23$ | $1.34 \pm 0.15$ |
| 0......................... | $S=4$ | 0.3 | 70.44 | $0.90 \pm 0.36$ | $11.22 \pm 9.68$ | $1.45 \pm 0.20$ |
|  | $S=4$ | 0.6 | 60.26 | $0.87 \pm 0.33$ | $10.00 \pm 8.41$ | $1.45 \pm 0.25$ |
|  | $S=4$ | 0.9 | 56.26 | $0.83 \pm 0.32$ | $9.11 \pm 7.60$ | $1.38 \pm 0.22$ |
|  | $S=4$ | 1.2 | 47.74 | $0.79 \pm 0.33$ | $8.52 \pm 7.59$ | $1.37 \pm 0.20$ |
|  | $S=4$ | 1.5 | 30.18 | $0.83 \pm 0.36$ | $9.61 \pm 8.19$ | $1.39 \pm 0.18$ |
|  | $S=4$ | 1.8 | 21.93 | $0.84 \pm 0.38$ | $10.14 \pm 8.41$ | $1.38 \pm 0.17$ |
|  | $S=4$ | 2.4 | 14.16 | $0.88 \pm 0.34$ | $10.08 \pm 7.62$ | $1.39 \pm 0.17$ |
|  | $S=4$ | 3.0 | 13.15 | $0.77 \pm 0.31$ | $7.70 \pm 5.89$ | $1.39 \pm 0.17$ |
|  | $S=4$ | 5.0 | 10.85 | $0.62 \pm 0.26$ | $5.11 \pm 3.62$ | $1.40 \pm 0.19$ |
|  | $S=4$ | 10.0 | 1.79 | $0.59 \pm 0.16$ | $4.16 \pm 1.55$ | $1.44 \pm 0.22$ |
|  | Fe | $1.2$ | $51.83$ | $0.79 \pm 0.32$ | $8.39 \pm 7.35$ | $1.37 \pm 0.27$ |
|  | Fe | 10.0 | 1.38 | $0.62 \pm 0.14$ | $4.41 \pm 1.34$ | $1.29 \pm 0.18$ |

mass that is taken as an indicator that the object is not a neutron star. Still it is interesting that rather large values for black hole masses have been reported in systems that presumably were not particularly metal-poor (Remillard \& McClintock 2006; Harrison et al. 2007). Either such systems have experienced an atypical evolution (of either the black hole progenitor star or the black hole itself after it was born) or the explosion energies are substantially less than what one commonly takes for Type II supernovae.

Much better experimental calibrations are available for neutron star masses, although one still must be concerned about the favored selection of objects in close binary systems. The average neutron star masses for solar metallicity stars in Table 6 range from 1.33 to $1.47 M_{\odot}$. This is to be compared with, e.g., estimates by Thorsett \& Chakrabarty (1999) of $1.35 \pm 0.04 M_{\odot}$ for 21 radio pulsars. While the agreement of the averages is impressive, it is also noteworthy that many neutron stars in our calculated data set have masses outside this range. In fact, the lightest neutron star in our theoretical sample has a gravitational mass of $1.16 M_{\odot}$ for the $S=4$ set and $1.08 M_{\odot}$ for the iron core set. There are also numerous cases of neutron stars with gravitational masses around the maximum mass limit.

Two major deficiencies of the current study are that it does not include the effects of rotation or of binary interaction. The former will tend to increase the mass of the remnants for a given mainsequence star since it leads to a larger helium core mass. The latter may lead to reduced masses for remnants, especially if the parent star loses its envelope early on to a companion and loses a lot more mass as a Wolf-Rayet star. Both effects could be included in future studies. It would also be useful to explore a wider range of explosion energies for the solar metallicity stars. We plan such a survey, with mass and energy resolution more like the Population III survey presented here, in the very near future. For now we note that the maximum mass black hole expected, even for low-energy explosions, is approximately the mass of the heaviest helium core in a presupernova star, i.e., $15 M_{\odot}$ for solar metallicity stars and $40 M_{\odot}$ for zero metallicity stars (Woosley et al. 2002). Lowmetallicity stars above $260 M_{\odot}$ can make heavier black holes (Heger \& Woosley 2002), and that threshold could be reduced by rotation.
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TABLE 6
Remnant Mass Averages and Distributions by Origin

| Range <br> $\left(M_{\odot}\right)$ | $\begin{aligned} & \mathrm{BH} \\ & (\%) \end{aligned}$ | $\begin{aligned} & \text { NS } \\ & \text { (\%) } \end{aligned}$ | $\begin{gathered} \log M_{\mathrm{BH}} \\ \left(M_{\odot}\right) \end{gathered}$ | $\begin{gathered} \text { BH Mass } \\ \left(M_{\odot}\right) \end{gathered}$ | $\begin{aligned} & \text { NS Mass } \\ & \left(M_{\odot}\right) \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Case: $Z=$ solar, $E=1.2 \mathrm{~B}$, Piston at $S=4, M_{\mathrm{NS}}^{\max }=1.7 M_{\odot}$ |  |  |  |  |  |
| $<10$ |  | 12.44 | ... | ... | $1.24 \pm 0.00$ |
| 10-12. | $\ldots$ | 20.00 | $\ldots$ | ... | $1.27 \pm 0.04$ |
| 12-15.. | $\ldots$ | 18.64 | $\ldots$ | $\ldots$ | $1.46 \pm 0.08$ |
| 15-20................. | 3.52 | 13.54 | $0.30 \pm 0.01$ | $2.02 \pm 0.04$ | $1.56 \pm 0.08$ |
| 20-25................. | 4.93 | 4.42 | $0.35 \pm 0.02$ | $2.22 \pm 0.11$ | $1.50 \pm 0.10$ |
| 25-40................ | 8.98 | 3.52 | $0.44 \pm 0.14$ | $2.93 \pm 1.06$ | $1.61 \pm 0.04$ |
| >40 ..................... | 6.53 | 3.48 | $0.46 \pm 0.17$ | $3.14 \pm 1.25$ | $1.57 \pm 0.06$ |
| Total ................ | 23.96 | 76.04 | $0.41 \pm 0.14$ | $2.71 \pm 1.02$ | $1.41 \pm 0.15$ |
| Case: $Z=$ solar, $E=1.2 \mathrm{~B}$, Piston at $S=4, M_{\mathrm{NS}}^{\max }=2.0 M_{\odot}$ |  |  |  |  |  |
| <10 .................... | $\ldots$ | 12.44 | $\ldots$ | $\ldots$ | $1.24 \pm 0.00$ |
| 10-12................ | $\ldots$ | 20.00 | ... | $\ldots$ | $1.27 \pm 0.04$ |
| 12-15... | $\ldots$ | 18.64 | $\ldots$ | $\ldots$ | $1.46 \pm 0.08$ |
| 15-20.. | ... | 17.06 | $\ldots$ |  | $1.60 \pm 0.11$ |
| 20-25................. | 0.39 | 8.96 | $0.37 \pm 0.00$ | $2.36 \pm 0.01$ | $1.70 \pm 0.22$ |
| 25-40................. | 4.86 | 7.63 | $0.55 \pm 0.12$ | $3.64 \pm 0.98$ | $1.72 \pm 0.12$ |
| >40 ..................... | 3.34 | 6.67 | $0.61 \pm 0.10$ | $4.18 \pm 0.92$ | $1.67 \pm 0.12$ |
| Total ................ | 8.59 | 91.41 | $0.56 \pm 0.12$ | $3.80 \pm 1.02$ | $1.47 \pm 0.21$ |
| Case: $Z=0, E=1.2 \mathrm{~B}$, Piston at $S=4, M_{\mathrm{NS}}^{\max }=1.7 M_{\odot}$ |  |  |  |  |  |
| <10 .................... | $\ldots$ | 6.98 | ... |  | $1.16 \pm 0.00$ |
| 10-12............... | $\ldots$ | 21.24 | $\ldots$ |  | $1.26 \pm 0.05$ |
| 12-15................. | 3.20 | 16.60 | $0.34 \pm 0.03$ | $2.22 \pm 0.16$ | $1.44 \pm 0.13$ |
| 15-20................. | 15.62 | 2.50 | $0.50 \pm 0.07$ | $3.23 \pm 0.50$ | $1.56 \pm 0.05$ |
| 20-25................. | 9.94 | . | $0.62 \pm 0.12$ | $4.28 \pm 1.21$ | ... |
| 25-40................. | 13.24 | 0.04 | $0.81 \pm 0.30$ | $7.95 \pm 4.42$ | $1.69 \pm 0.00$ |
| >40 ...................... | 10.63 | .. | $1.27 \pm 0.17$ | $19.91 \pm 7.18$ | $\ldots$ |
| Total ................ | 52.63 | 47.37 | $0.75 \pm 0.35$ | $7.93 \pm 7.47$ | $1.33 \pm 0.14$ |

Case: $Z=0, E=1.2 \mathrm{~B}$, Piston at $S=4, M_{\mathrm{NS}}^{\max }=2.0 M_{\odot}$

| <10 .................... | $\ldots$ | 6.98 | ... | ... | $1.16 \pm 0.00$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 10-12................. | $\ldots$ | 21.24 | $\ldots$ | $\ldots$ | $1.26 \pm 0.05$ |
| 12-15................. | 1.19 | 18.61 | $0.38 \pm 0.00$ | $2.38 \pm 0.02$ | $1.48 \pm 0.17$ |
| 15-20................. | 14.43 | 3.70 | $0.52 \pm 0.05$ | $3.32 \pm 0.40$ | $1.65 \pm 0.15$ |
| 20-25................. | 9.94 | . . | $0.62 \pm 0.12$ | $4.28 \pm 1.21$ | ... |
| 25-40................. | 11.55 | 1.73 | $0.88 \pm 0.25$ | $8.81 \pm 4.08$ | $1.82 \pm 0.08$ |
| >40 ..................... | 10.63 | ... | $1.27 \pm 0.17$ | $19.91 \pm 7.18$ | $\ldots$ |
| Total ................ | 47.74 | 52.26 | $0.79 \pm 0.33$ | $8.52 \pm 7.59$ | $1.37 \pm 0.20$ |

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